

# OPTOELECTRONICS

Power Products Databook



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# HARRIS SEMICONDUCTOR OPTOELECTRONIC DEVICES

# Contents

Optoelectronics, based on semiconductor mass production technology, is strongly influencing the design of electronic control circuitry. Optoelectronic components sense the presence and intensity of light, the position of objects which break or reflect a light beam, and transmit electronic signals without electrical connections. This provides high speed and high reliability at low cost for a variety of useful functions, from automatic light level control in copy machines, or sensing the right instant to fire an automobile's spark plug, to allowing delicate computer circuitry to control high power machine tools by interfacing logic signals to the power line circuitry without allowing line voltages and noise to interfere with the logic.

Harris Semiconductor, a leader in both optoelectronics and semiconductor technology, has contributed significantly to optoelectronics starting from the invention of the light emitting diode and the first commercially successful light activated silicon controlled rectifier. Today Harris Semiconductor can offer the broadest line of optoelectronic circuit components in the industry. This Data Book is written to provide the circuit designer with a knowledge of the operation, interfacing, and detailed application of these components so he may successfully design practical, cost effective, and reliable circuitry. It also provides the data sheets, selection guides and cross-reference information needed to choose the optimum device for a specific task.

The data sheets provide definitive device ratings and characteristics data. The Data Book also includes dimensional outlines of the various packages used and application notes on Harris Semiconductor Optoelectronics.

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**Dimensional Outlines** 

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# **Quick-Reference Product Guide**

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# HARRIS OPTOELECTRONIC Devices

# Index to Types

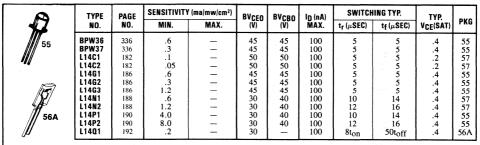
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CNY47 CNY47A CNY48 CNY51 CQX14 CQX15 CQX16 CQX17 CQY80 F5D1	370 370 372 374 340 340 340 340 342	H11B1 H11B2 H11B3 H11B255 H11C1 H11C2 H11C3 H11C4 H11C5 H11C6	234 234 324 236 238 238 238 242 242 242	H21L2 H22A1 H22A2 H22A3 H22A4 H22A5 H22A6 H22B1 H22B2 H22B3	312 314 314 316 316 316 318 318 318	MCT26 MCT210 MOC3009 MOC3011 MOC3011 MOC3012 MOC3020 MOC3021 MOC3022 MOC3023	398 400 288 288 288 288 290 290 290
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#### **INFRARED EMITTERS**

NO NO	TYPE NO.	PAGE NO.	MIN. Po @ If = 100mA	MAX. V <sub>F</sub> @ I <sub>F</sub> = 100mA	PEAK EMISSION Wavelength Typ. n Meters	RISE TIME TYP. µSEC	FALL TIME TYP. µSEC	MAX. PD mW	MAX. IF CONT. mA	PKG
<i>f</i> 54A	1N6264 1N6265 1N6266 CQX14 CQX15 CQX16	166 166 168 340 340 340	6.0mW 6.0mW 25mW/sr 5.4mW 5.4mW	1.7V 1.7V 1.7V 1.7V 1.7V	940 940 940 940 940 940	1.0 1.0 1.0 1.0 1.0	1.0 1.0 1.0 1.0 1.0	1300 1300 1300 1300 1300 1300	100 100 100 100 100	54A 54A 54A 54A 54
54	CQX17 F5D1 F5D2 F5D3 F5E1 F5E2 F5E3 F5F1	340 172 172 172 172 172 172 176	1.5mW 12mW 9mW 10.5mW 12mW 9mW 10.5mW	1.7V 1.7V 1.7V 1.7V 1.7V 1.7V 1.7V	940 880 880 880 880 880 880 940	1.0 1.5 1.5 1.5 1.5 1.5 1.5	1.0 1.5 1.5 1.5 1.5 1.5 1.5	1300 1300 1300 1300 1300 1300 1300 100	100 100 100 100 100 100 100 60	54 54A 54A 54A 54 54 54 54
56	F5G1 LED55C LED55B LED56 LED55CF LED55BF LED56F	178 180 180 180 180 180 180	.26ll W/Sr .6mW/sr 5.4mW 3.5mW 1.5mW 5.4mW 3.5mW	1.7V 1.85V 1.7V 1.7V 1.7V 1.7V 1.7V	940 880 940 940 940 940 940	1.0 1.5 1.0 1.0 1.0 1.0	1.0 1.5 1.0 1.0 1.0 1.0	100 100 1300 1300 1300 1300 1300	50 100 100 100 100 100	56 54A 54A 54A 54 54 54

### **DETECTORS**

#### **PHOTO TRANSISTORS**



#### **PHOTO DARLINGTONS**

	TYPE	PAGE	SENSITIVITY	(ma/mw/cm²)	BVCEO	BVCBO	In (nA)	SWITCH	IING TYP.	TYP.	
	NO.	NO.	MIN.	MAX.	(V)	. (V)	MAX.	t <sub>r</sub> (μSEC)	tf (μSEC)	VCE(SAT)	PKG
	BPW38	338	15.0	_	25	25	100	75	50	.8	55
4///	L14F1	184	15.0		25	25	100	75	50	.8	55
** 57	L14F2	184	5.0		25	25	100	75	50	.8	55
	L14R1	194	5.0	_	30	_	100	45ton	250toff	.9	56A

# **OPTOISOLATORS**

# PHOTO TRANSISTOR OUTPUT

	TYPE NO.	PAGE NO.	SURGE ISOLATION VOLTAGE RMS	CURRENT TRANSFER	BVCEO (VOLTS)	TYPI (μ8		VCE (SAT) MAX.	PKG.
	HU.	110.	MIN.	RATIO MIN.	MIN.	t,	t,		<u> </u>
295	CNX35	344	4000V	40-160%	. 30	2	2	.4	296
	CNX36	344	4000V	80%	30	2	2	.4	296
	CNY17I CNY17II	346 346	3000V 3000V	40-80% 63-125%	70 70	2 2	2 2	.3 .3	296 296
	CNY17III	346	3000V	100-200%	70	2	2	.3	296
	CNY17IV	346	3000V	160-320%	70	2	2	.3	296
1 11000 1711	CNY32	360	4000V	20%	30	3	3	.4	297
	CNY47	370	2500V	20-60%	30	2	2	.4	296
	CNY47A	370	2500V	40%	30	2	2	.4	296
	CNY51	374	4000V	100%	70	2	2	.4	296
	CQY80 GEPS2001	342 382	4000V 2500V	60% 30%	30	5	5	4	296 296
	GFH600I	384	2800V 2800V	63-125%	70	5	5	.3	296
	GFH600II	384	2800V 2800V	100-200%	70	5	5	.3	296
	GFH600III	384	2800V	160-320%	70	5	5	.3	296
	GFH601I	388	2800V	40-80%	70	5	.5	.4	296
	GFH601II	388	2800V	63-125%	70	5	- 5	.4	296
	GFH601III	388	2800V	100-200%	70	5	5	.4	296
	GFH601IV	388	2800V	160-320%	70	5	5	.4	296
296	HIIAI	210	2500V	50%	30	2	2	.4	296
	H11A2	210	2500V 2500V	20%	30	2 2	2 2	.4 .4	296 296
	H11A3 H11A4	210	2500V 2500V	20% 10%	30	2	2	.4	296
Tann	H11A5	210	2500V 2500V	30%	30	2	2	.4	296
I I DANN	H11A520	218	4000V	20%	30	2	2	.4	296
	H11A550	218	4000V	50%	30	2	2	.4	296
100	H11A5100	218	4000V	100%	30	2	2	.4	296
	H11AG1	226	4000V	300%	30	5	5	.4	296
	H11AG2	226	4000V	200%	30	5	5	.4	296
	H11AG3	226	2500V	100%	30	5	5 5	.4	296
İ	H11AV1 H11AV1A	230 230	4000V 4000V	100%	70	5 5	5	.4 .4	296 295
	H11AV2	230	4000V 4000V	50%	70	5	5	.4	296
	H11AV2A	230	4000V	50%	70	5	5	.4	295
297	H11AV3	230	4000V	20%	70	5	5	.4	296
	H11AV3A	230	4000V	20%	70	5	5	.4	295
	H24A1	332	4242V	100%	30	3	3	.4	297
	H24A2	332	4242V	20%	30	3	3	.4	297
	4N25	196	2500V	20%	30	3	3	.5	296
	4N25A	196	2500V	20%	30	3	3	.5	296 296
1 11 111	4N26 4N27	196 196	2500V 2500V	20% 10%	30	3 3	3	.5 .5	296
fo fo	4N28	196	2500V 2500V	10%	30	3	3	.5	296
	4N35	200	2500V	100%	30	5	5	.3	296
1	4N36	200	2500V	100%	30	5	5	.3	296
	4N37	200	2500V	100%	30	5	5	.3	296
-	H74A1	246	2500V		15	1			296
	MCT2	398	2500V	20%	30	5	5	.4	296
	MCT2E	398	2500V	20%	30 30	5 5	5 5	.4	296 296
	MCT26 MCT210	398 400	2500V 2500V	6% 150%	30	5	5	.4 .4	296
	SL5500	292	2500V 2500V	40-300%	30	20	50	.4	296
	SL5501	292	2500V	25-400%	30	20	50	.4	296
	SL5504	296	2500V	25-400%	80	50	150	.4	296
	SL5511	300	2500V	25%	30	20	50	.4	296
	нідн vc	LTAGE	E PHOTO TRA	ANSISTOR	OUTPU				
	TYPE NO.	PAGE No.	ISOLATION VOLTAGE V <sub>IO</sub> (RMS)	CURRENT Transfer Ratio Min.	BVCEO (VOLTS) Min.	TYP (μS		VCE (SAT) MAX.	PKG.
		250			+	+		<del>                                     </del>	+
	H1101 H1102	250 250	4000V 2500V	20%	300 300	5	5	.4	296 296
	H11D3	250	2500V 2500V	20% 20%	200	5	5	.4	296
	H1104	250	2500 V 2500 V	10%	200	5	5	.4	296
1	4N38	204	2500V	10%	80	5	5	1.0	296
i									
	4N38A CNY33	204	2500V	10%	80	5	5	1.0 .4	296 296

# **OPTO ISOLATORS (Continued)**

# PHOTO DARLINGTON OUTPUT

297

TYPE NO.	PAGE No.	SURGE ISOLATION VOLTAGE RMS	CURRENT TRANSFER	BVCEO (VOLTS)	(VOLTS) (USEC) VCE (SAT)			
		MIN.	RATIO MIN.	MIN.	t	t,	mnn.	
H11B1	234	4000V	500%	25	125	100	1.0	296
H11B2	234	4000V	200%	25	125	100	1.0	296
H11B3	234	4000V	100%	25	125	100	1.0	296
H11B255	236	2500V	100%	55	125	100	1.0	296
H24B1	334	4242V	1000%	30	125	100	1.4	297
H24B2	334	4242V	400%	30	125	100	1.4	297
4N29	198	2500V	100%	30	5	40	1.0	296
4N29A	198	2500V	100%	30	5	40	1.0	296
4N30	198	2500V	100%	30	5	40	1.0	296
4N31	198	2500V	50%	30	5	40	1.2	296
4N32	198	2500V	500%	30	5	100	1.0	296
4N32A	198	2500V	500%	30	5	100	1.0	296
4N33	198	2500V	500%	30	5	100	1.0	296
CNY31	358	4000V	400%	30	125	100	1.4	297
CNY48	372	2500V	600%	30	125	100	1.0	296
MCA230	392	2500V	100%	30	5	100	1.0	296
MCA231	392	2500V	200%	30	5	100	1.0	296
MCA255	392	2500V	100%	55	5	100	1.0	296

# HIGH VOLTAGE PHOTO DARLINGTON OUTPUT

296



TYPE NO.	PAGE NO.	SURGE ISOLATION VOLTAGE	CURRENT TRANSFER	BVCEO (VOLTS)	TYPI (µS		VCE (SAT) MAX.	PKG.	
NU.		VIO (RMS)	RATIO MIN.	MIN.	t, t				
H1161	256	4000V	1000%	100	5	100	1.0	296	
H11G2	256	4000V	1000%	80	5	100	1.0	296	
H1163	258	4000V	200%	55	5	100	1.0	296	
H11G45	260	4000V	250%	55	50	500	1.0	296	
H11G46	260	4000V	500%	55	50	500	1.0	296	

# TRIAC DRIVER OUTPUT

TYPE NO.	PAGE NO.	SURGE ISOLATION VOLTAGE V <sub>IO</sub> (RMS)	IF TRIGGER Max.	BLOCKING Voltage Min.	ON-STAGE Voltage 146 = 100 ma Max.	TYPICAL dv/dt V/µSEC STATIC	PKG.
					14.1		
H11J1	262	4000V	10mA	250V	3.0V	2.0	296
H11J2	262	4000V	15mA	250V	3.0V	2.0	296
H11J3	262	2500V	10mA	250V	3.0V	2.0	290
H11J4	262	2500V	15mA	250V	3.0V	2.0	290
H11J5	262	2500V	25mA	250V	3.0V	2.0	296
GE3009	378	4000V	30mA	250V	3.0V	6.0	29
GE3010	378	4000V	15mA	250V	3.0V	6.0	29
GE3011	378	4000V	10mA	250V	3.0V	6.0	29
GE3012	378	4000V	5mA	250V	3.0V	6.0	29
GE3020	380	4000V	30mA	400V	3.0V	6.0	29
GE3021	380	4000V	15mA	400V	3.0V	6.0	29
GE3022	380	4000V	10mA	400V	3.0V	6.0	29
GE3023	380	4000V	5mA	400V	3.0V	6.0	29
MOC3009	288	7500Vpk	30mA	250V	3.0V	6.0	29
MOC3010	288	7500Vpk	15mA	250V	3.0V	6.0	29
M0C3011	288	7500Vpk	10mA	250V	3.0V	6.0	29
MOC3012	288	7500Vpk	5mA	250V	3.0V	6.0	29
M0C3020	290	7500Vpk	30mA	400V	3.0V	6.0	29
M0C3021	290	7500Vpk	15mA	400V	3.0V	6.0	29
M0C3022	290	7500Vpk	10mA	400V	3.0V	6.0	29
M0C3023	290	7500Vpk	5mA	400V	3.0V	6.0	29

# **OPTOISOLATORS (Continued)**

#### PHOTO SCR OUTPUT

TYPE NO.	PAGE NO.	SURGE ISOLATION VOLTAGE V <sub>IO</sub> (RMS)	IF TRIGGER (MAX.	BLOCKING Voltage (Min.)	TYPICAL TON (µSEC)	V <sub>F</sub> (MAX.)	PKG.
HIICI	238	4000V	20mA	200	1	1.5	296
H11C2	238	2500V	20mA	200	1	1.5	296
H11C3	238	2500V	30mA	200	1 1	1.5	296
H11C4	242	4000V	20mA	400	1	1.5	296
H11C5	242	2500V	20mA	400	-1	1.5	296
H11C6	242	2500V	30mA	400	1	1.5	296
HIIMI	274	4000V	7mA	800	1	1.5	296
H11M2	274	4000V	15mA	800	1	1.5	296
H11M3	278	4000V	7mA	600	1	1.5	296
H11M4	278	4000V	15mA	600	1	1.5	296
4N39	206	2500V	14mA	200	1	1.5	296
4N40	206	2500V	I4mA	400	1 1	1.5	296
H74C1	248	2500V		200			296
H74C2	248	2500V		400		1	296
CNY30	354	2500V	20mA	200	1	1.5	296
CNY34	354	2500V	20mA	400	1	1.5	296
MCS2	394	2500V	14mA	200	1	1.5	296
MCS2400	394	2500V	14mA	400	1	1.5	296
MCS21	396	3000V	20mA	200	1	1.5	296
MCS2401	396	3000V	20mA	400	1	1.5	296

# PROGRAMMABLE THRESHOLD ISOLATOR

TYPE NO.	PAGE NO.	SURGE ISOLATION VOLTAGE	CURRENT TRANSFER	BV <sub>CEO</sub> (VOLTS)	TYPI (µS		V <sub>CE (SAT)</sub> MAX.	PKG.
NO.		VIO (RMS)	RATIO MIN.	MIN.	t	tı	minn.	
H11A10	214	2500	10%	30	2	2	.4	296

#### **AC INPUT ISOLATOR**

TYPE NO.	PAGE SURGE ISOLATIO NO. VOLTAGE		CURRENT TRANSFER	BV <sub>CEO</sub> (VOLTS)	TYPI (µ8		V <sub>CE (SAT)</sub>	PKG.
NU.		VIO (RMS)	RATIO MIN.	MIN.	t,	t,	max.	
H11AA1	222	1770V	20%	30	2	2	.4	296
H11AA2	222	1770V	10%	30	2	2	.4	296
H11AA3	222	1770V	50%	30	2	2	.4	296
H11AA4	222	1770V	100%	30	2	2	.4	296
CNY35	364	1060V	10%	30	2	2	.4	296

296

# BILATERAL OUTPUT Analog FET

TYPE NO.	PAGE NO.	SURGE ISOLATION VOLTAGE VIO (RMS)	ON-STATE RESISTANCE MAX. OHMS	OFF-STATE RESISTANCE MIN. OHMS	BREAKDOWN VOLTAGE	TURN-ON TIME (µSEC)	TURN-OFF TIME (µSEC)	PKG.
H11F1	252	2500	200	300M	30	15	15	296
H11F2	252	2500	330	300M	30	15	15	296
H11F3	252	2500	470	300M	15	15	15	296

# **Darlington**

TYPE NO.	TYPE PAGE ISOLATION NO. NO. VOLTAGE VIO (RMS)		CURRENT Transfer Ratio Min.	BV <sub>CEO</sub> (VOLTS) MIN.	TYP (µS	ICAL EC)	V <sub>CE (SAT)</sub> MAX.	PKG.
		V <sub>IO</sub> (RMS)	incrio min.	171114.	t.	t,		
H11K1 H11K2	266 266	2500V 2500V	1000% 500%	250 200	20 20	40 40	2.5 2.5	296 296

# **SCHMITT TRIGGER OUTPUT**

TYPE NO.	PAGE NO.	SURGE ISOLATION VOLTAGE	CURRENT IOFF/ION FON RATIO		IOFF/ION VOL (I		MAXIMUM Data Rate, NRZ	OPER/ VOL	TAGE	PKG.
		V <sub>IO</sub> (RMS)	MAX.	MIN.	MAX.	MAX.		MIN.	MAX.	
HIILI	270	2500V	1.6mA	0.3	0.9	0.4V	1.0MHz	3V	16V	296
H11L2	270	2500V	10mA	0.3	0.9	0.4V	1.0MHz	3V	16V	296
H11L3	270	2500V	5mA	0.3	0.9	0.4V	1.0MHz	3V	16V	296
HIINI	282	4000V	3.2mA	0.65	0.95	0.5V	5.0MHz	4V	15V	296
H11N2	282	4000V	5mA	0.65	0.95	0.5V	5.0MHz	4V	15V	296
H11N3	282	2500V	10mA	0.65	0.95	0.5V	5.0MHz	4V	15V	296

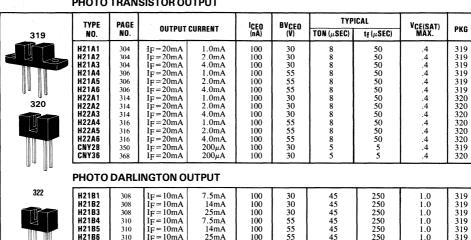
# **OPTO ISOLATORS (Continued)**

#### **VIDEO/WIDEBAND LINEAR ISOLATOR**

296	TYPE NO.	PAGE NO.	SURGE ISOLATION VOLTAGE RMS MIN.	OUT Voli @IF={	PUT FAGE	A OUT Vol: @I =1	PUT	-6db Bandwidth	OPER. VOL		PKG.
				MIN.	MAX.	MIN.	MAX.	TYPE.	MIN.	MAX.	
	H11V1 H11V2 H11V3	286 286 286	4000V 4000V 4000V	2.0 2.0 2.0	7.0 7.0 7.0	0.5 0.75 0.33	1.25	0-10 MHz 0-10 MHz 0-10 MHz	5V 5V 5V	15V 15V 15V	296 296 296

#### PHOTON COUPLED INTERRUPTER MODULE

#### PHOTO TRANSISTOR OUTPUT



14mA

25mA

7.5mA

14mA

25mA

7.5mA

14mA

25mA

2.5mA

100

100

100

100

100

100

100

100

55

30

30

45

45

45

45

45 45

150





H21B5

H21B6

H22B1

H22B2

H22B3

H22B4

H22R5

H22R6

CNY29



### **SCHMITT TRIGGER OUTPUT**

310

310

318

318

318

320

320

320

 $I_F = 10mA$ 

 $I_F = 10 \text{mA}$ 

 $I_F = 10 \text{mA}$ 

 $I_F = 10mA$ 

 $I_F = 20 \text{mA}$ 

TYPE NO.	PAGE NO.	TURN ON CURRENT (F(ON),	IOFF	ERESIS /I(ON) Tio	OUTPUT VOLTAGE VOL		ATING TAGE	PKG
		MAX.	MIN.	MAX.	MAX.	MIN.	MAX.	
H21L1 H21L2 H22L1 H22L2	312 312 322 322	30mA 15mA 30mA 15mA	.5 .5 .5	.9 .9 .9	.4V .4V .4V .4V	4V 4V 4V 4V	15V 15V 15V 15V	323 323 322 322

250

250

250

250

250

250

250 250

150

1.0

1.0

1.0

1.0

1.0

1.0

1.0

1.0

12

319

320

320

320

320

320

320

319

# MATCHED EMITTER DETECTOR PAIRS

	РНОТО	TRAN	ISISTOR O	UTPUT				at es		
	TYPE	PAGE NO.	OUTPUT C	UDDENT	ICEO	BVCEO	TYP	CAL	VCE (SAT) MAX.	PKG.
	NO.		UUIFUI	Unneni	nnen (na)		TON (µSEC)	T <sub>1</sub> (µSEC)	MAX.	FRU.
321	H23A1 H23A2	324 324	IF=30mA IF=30mA	1.5mA 1.0mA	100 100	30 30	8 8	50 50	.4 .4	321 321
	PHOTO DARLINGTON OUTPUT									
11 1	H23B1	326	IF=10mA	7.5mA	100	30	45	250	1.0	321
	SCHMI	TT TRI	GGER OUT	PUT						
	TYPE PAGE CURRENT IOFF/I(ON) OUTPUT VOLTAGE VOLTAGE  NO. NO. IF(ON). RATIO VOL									PKG
			MAX.	MIN.	MAX.		MAX.	MIN.	MAX.	
	H23L1	328	20mA	.5	.9		.4V	4V	15V	

# **Industry Replacement Guide**

equivalents for the products listed. Harris assumes no responsibility and does not guarantee that the replacements are exact, but replacements. only that the replacements will meet the terms of its applicable

The suggested replacements represent what is believed to be published product warranties. The pertinent product-specification sheets should always be used as the key tool for actual

COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER	COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER		COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER		COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER
1N6264	1N6264	CLI-840	H21B1		FCD825B	H11A1		H11B2	H11B2
1N6265	1N6265	CLI-841	H21B4		FCD825C	H11A550		H11B3	H11B3
1N6266	1N6266	CLI-850	H21B2		FCD825D	H11A550		H11B255	H11B255
4N25	4N25	CLI-851	H21B5		FCD830	H11A1		H11C1	H11C1
4N25A	4N25A	CLI-860	H21B3		FCD830A	H11A2		H11C2	H11C2
4N26	4N26	CLI-861	H21B6		FCD830B	H11A3		H11C3	H11C3
4N27	4N27	CLI-870	H21B1		FCD830C	H11A520		H11C4	H11C4
4N28	4N28	CLI-871	H21B4		FCD830D	H11A520		H11C5	H11C5
4N29	4N29	CLT2010	L14C2		FCD831	H11A3		H11C6	H11C6
4N29A	4N29A	CLT2020	L14C1		FCD831A	H11A3		H11D1	H11D1
					ka sa a sa			and the state of t	
4N30	4N30	CLT2130	L14G2		FCD831B	H11A3		H11D2	H11D2
4N31	4N31	CLT2140	L14G2		FCD831C	H11A520	١.,	H11D3	H11D3
4N32	4N32	CLT2150	L14G1		FCD831D	H11A520		H11D4	H11D4
4N32A 4N33	4N32A 4N33	CLT2160 CNY17I	L14G3 CNY17I		FCD836 FCD836C	H11A3 H11A520		H11F1 H11F2	H11F1 H11F2
4N35	4N35	CNY17II	CNY17II		FCD850	4N29		H11F3	H11F3
4N36	4N36	CNY17III	CNY17III		FCD860	H11B1		H11G1	H11G1
4N37	4N37	CNY17IV	CNY17IV		FCD865	H11B1		H11G2	H11G2
4N38	4N38	CNY28	CNY28		FPE500	LED56		H11G3	H11G3
4N38A	4N38A	CNY29	CNY29		FPE510	LED56F		H11G45	H11G45
		1			l de la decidada de la composição de la co				
4N39	4N39	CNY30	CNY30 CNY31		FPE520 FPE530	LED56		H11'G46 H11J1	H11G46 H11J1
4N40 BPW13A	4N40 L14C2	CNY31 CNY32	CNY32		GE3009	LED56F GE3009		H11J2	H11J2
BPW13B	L14C2	CNY33	CNY33		GE3010	GE3010		H11J3	H11J3
BPW13C	L14C2	CNY34	CNY34		GE3010	GE3010		H11J4	H11J4
BPW36	BPW36	CNY35	CNY35		GE3012	GE3011		H11J5	H11J5
BPW37	BPW37	CNY36	CNY36		GE3020	GE3020		H11L1	H11L1
BPW38	BPW38	CNY37	CNY28		GE3021	GE3021		H11L2	H11L2
BPX-38-1	L14C1	CNY47	CNY47		GE3022	GE3022		H11L3	H11L3
CL-100	LED56	CNY47A	CNY47A		GE3023	GE3023		H11N1	H11N1
CLI-2	H11A5	CNY48	CNY48		GFH600I	GFH600I		H11N2	H11N2
CLI-3	4N37	CNY51	CNY51		GFH600II	GFH600II		H11N3	H11N3
CLI-5	H11A3	CNY75A	GFH601II		GFH60III	GFH600III	1	H13A1	H21A1
CLI-6	H11A1	CNY75B	GFH601III		GFH6011	GFH601I		H13A2	H21A1
CLI-7	H11A3	CNY75C	GFH601IV		GFH601II	GFH601II		H13B1	H21B1
CLI-8	H11A3	CQX14	CQX14		GFH601III	GFH601III		H13B2	H21B1
CLI-9	H11A3	CQX15	CQX15		GFH601IV	GFH601IV		H15A1	H24A2
CLI-10	H11B1	CQX16	CQX16		H11A1	H11A1		H15A2	H24A2
CLI-11	H11B1	CQX17	CQX17		H11A2	H11A2		H15B1	H24B2
CLI-12	H11B2	CQY80	CQY80		H11A3	H11A3		H15B2	H24B2
CLI-13	H11G3	F5D1	F5D1		H11A4	H11A4		H17A1	H23A1
CLI-14	H11G3	F5D2	F5D2		H11A5	H11A5		H17B1	H23B1
CLI-20	H11A2	F5D3	F5D3		H11A10	H11A10		H20A1	H22A1
CLI-210	H22A1	F5E1	F5E1		H11A520	H11A520		H20A2	H22A1
CLI-220	H22B1	F5E2	F5E2		H11A550	H11A550		H20B1	H22B1
CLI-230	H22B1	F5E3	F5E3		H11A5100	H11A5100		H20B2	H22B1
CL1-506	H11A3	F5F1	F5F1		H11AA1	H11AA1		H21A1	H21A1
CLI-506A	H11A3	F5G1	F5G1		H11AA2	H11AA2		H21A2	H21A2
CLI-506B CLI-510	H11A3 4N37	FCD810 FCD810A	H11A3		H11AA3	H11AA3		H21A3 H21A4	H21A3 H21A4
			H11A5		H11AA4	H11AA4			
CLI-511	4N37	FCD810B	H11A3		H11AG1	H11AG1	1	H21A5	H21A5
CLI-800	H21A1	FCD810C	H11A520		H11AG2	H11AG2		H21A6	H21A6
CLI-810 CLI-811	H21A1 H21A4	FCD810D	H11A520		H11AG3	H11AG3	l	H21B1	H21B1
CLI-811 CLI-820	H21A4 H21A2	FCD820 FCD820A	H11A3 H11A2		H11AV1 H11AV1A	H11AV1		H21B2 H21B3	H21B2 H21B3
CLI-821	H21A5	FCD820A	H11A3		H11AV2	H11AV1A H11AV2		H21B3	H21B4
CLI-830	H21A3	FCD820B	H11A520		H11AV2A	H11AV2A		H21B5	H21B5
CLI-831	H21A6	FCD820D	H11A520		H11AV3	H11AV2A		H21B6	H21B6
CLI-835	H21A1	FCD825	H11A1		H11AV3A	H11AV3A	1	H21L1	H21L1
CLI-836	H21A4	FCD825A	H11A1		H11B1	H11B1		H21L2	H21L2
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# **Industry Replacement Guide**

COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER
H22A1	H22A1
H22A2	H22A2
H22A3	H22A3
H22A4	H22A4
H22A5	H22A5
H22A6	H22A6
H22B1	H22B1
H22B2	H22B2
H22B3	H22B3
H22B4	H22B3
H22B5	H22B5
H22B6	H22B6
H22L1	H22L1
H22L2	H22L2
H23A1	H23A1
H23A2	H23A2
H23B1	H23B1
H23L1	H23L1
H24A1	H24A1
H24A2	H24A1
H24B1	H24B1
H24B2	H24B2
H74A1	H74A1
H74C1	H74C1
H74C2	H74C2
IL1	H11A3
IL5	H11A1
IL12	H11A5
IL15	H11A5
IL16	H11A5
IL74	H11A5
IL201	CNY17II
IL202	CNY17III
IL203	CNY17IV
IL250	H11AA3
ILA30	H11B3
ILA55	H11B255
ILCA2-30	H11B3
ILCA2-55	H11B255
L14C1	L14C1
L14C2	L14C2
L14F1	L14F1
L14F2	L14F2
L14G1	L14G1
L14G2	L14G2
L14G3	L14G3
L14N1	L14N1
L14N2	L14N2
L14P1	L14P1
L14P2	L14P2
L14Q1 L14R1 LED55B LED55BF LED55C LED55CF LED56 MCA11G1 MCA11G2	L14Q1 L14R1 LED55B LED55BF LED55C LED55CF LED56 LED56F H11G1 H11G2
MCA8	H21B1
MCA81	H21B1
MCA230	MCA230
MCA231	MCA231
MCA255	MCA255
MCP3009	GE3009
MCP3010	GE3010
MCP3011	GE3011

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COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER
MCP3020	GE3020
MCP3021	GE3021
MCP3022	GE3022
MCS22	MCS2
MCS21	MCS21
MCS2400	MCS2400
MCS2401	MCS2401
MCT22	MCT2
MCT2E	MCT2E
MCT2E	H21A1
MCT26 MCT81 MCT210 MCT2200 MCT2201 MCT2202 MCT270 MCT271 MCT272 MCT273	MCT26 H21A1 MCT210 H11A520 H11A550 CNY17II CNY17II CNY17II CNY17III
MCT274	CNY17IV
MCT275	CNY17III
MCT277	H11A1
MCT5200	H11AG3
MCT5201	H11AG3
MCT5211	H11AG3
MCT5211	H11AG2
MCP3011A	GE3011
MCP3012	GE3012
MCP3022A	GE3022
MCP3023	GE3023
MEH520	F5D2
MEH580	F5E2
MES560	F5G1
MES760	F5F1
MFOD202F	GFOD1A1
MFOD302F	GFOD1B1
MFOE102F	GFOE1A1
MLED71	F5F1
MLED930	LED56
MOC1000 MOC1001 MOC1002 MOC1003 MOC1005 MOC1006 MOC119 MOC1200 MOC3000 MOC3001	4N26 4N25 4N27 4N28 H11A520 H11B2 4N30 H11C6 H11C5
MOC3002	H11C3
MOC3003	H11C2
MOC3007	H11C3
MOC3009	MOC3009
MOC3010	MOC3010
MOC3011	MOC3011
MOC3012	MOC3012
MOC3020	MOC3020
MOC3021	MOC3021
MOC3022	MOC3022
MOC3023	MOC3023
MOC5003	H11L2
MOC5004	H11L2
MOC5005	H11L2
MOC5006	H11L2
MOC5007	H11L1
MOC5008	H11L3
MOC5009	H11L2

COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER
MOC5010 MOC7811 MOC7812 MOC7813 MOC7821 MOC7822 MOC7823 MOC8020 MOC8020 MOC80021 MOC8030	* H21A1 H21A2 H21A3 H22A1 H22A2 H22A3 H11G2 H11G2 H11G2
MOC8050	H11G2
MOC8100	H11AG3
MRD300	L14G1
MRD310	L14G2
MRD3050	L14G2
MRD3051	L14G2
MRD3051	L14G2
MRD3053	L14G2
MRD3053	L14G2
MRD3054	L14G2
MRD3055	L14G2
MRD3056	L14G1
MRD360	L14F1
MRD370	L14F2
MRD701	L14Q1
MRD711	L14R1
MT1	L14C1
MT2	L14G1
MTH320	L14G3
MTH321	L14P2
MTH360	L14N1
MTH420	L14P1
MTS360	L14Q1
MTS361	L14Q1
MTS460	L14Q1
MTS461	L14Q1
MSA8	H21B1
MSA81	H21B1
MST8	H21A1
MST81	H21A1
OP130	LED56
OP130W OP131 OP131W OP132 OP132W OP133 OP133W OP135W OP136	LED56F LED55BF LED55CF LED55CF LED55CF LED55CF LED55BB LED55BF LED55BF LED55B
OP136W OP137 OP137W OP140 OP140SL OP140SLA OP140SLB OP140SLC OP140SLD OP230	LED55BF LED55C LED55CF F5F1 F5F1 F5F1 F5F1 F5F1 F5F1 F5F1
OP230W	F5E2
OP231	F5D2
OP231W	F5E2
OP232	F5D3
OP232W	F5E3
OP233	F5D1
OP233W	F5E1
OP240	F5E1

COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER
OP240SLA OP240SLB OP240SLC OP550 OP550SLA OP550SLB OP550SLC OP550SLD OP560 OP800	F5G1 F5G1 F5G1 L14Q1 L14Q1 L14Q1 L14Q1 L14Q1 L14Q1 L14R1 L14G2
OP800W OP801 OP801W OP802 OP802W OP803 OP804 OP805 OP811 OP811W	L14C2 L14G2 L14C1 L14C1 L14G1 L14G3 L14P1 L14P1 L14P1 L14G2 L14C1
OP812	L14G1
OP813	L14G3
OP814	L14G3
OP830	L14F1
OP841	L14G2
OP841W	L14C2
OP842	L14G1
OP842W	L14N1
OP843	L14G3
OP843W	L14N1
OP844 OP844W OP845 OP845W OPB120 OPB242 OPB243 OPB800 OPB800S OPB800S	L14P1 L14N1 L14P1 L14N1 H21A1 H21A1 H21B1 H21B1 H21A1 H21B1 H21B1
OPB804	H22A1
OPB806	H21A1
OPB813	H21A1
OPB814	H21A2
OPB815	H21A2
OPB816	H21A1
OPB817	H21A1
OPI2100	MCT210
OPI2150	H11A4
OPI2151	H11A4
OPI2152	H11A2
OPI2153	H11A1
OPI2154	H11AG3
OPI2155	H11AG3
OPI2250	H11A3
OPI2251	H11A3
OPI2252	H11A3
OPI2252	H11A1
OPI2254	H11AG3
OPI2255	H11AG3
OPI2500	H11AA2
OPI3009	GE3009
OPI3010	GE3010
OPI3011	GE3011
OPI3012	GE3012
OPI3020	GE3020
OPI3021	GE3021

# **Industry Replacement Guide**

COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER	COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER
OPI3022	GE3022	SD5440-3	L14G2
OPI3023	GE3023	SD5440-4	L14G1
OPI3150	H11B2	SD5440-5	L14G1
OPI3151	H11B2	SD5443-1	L14G2
OPI3152	H11B3	SD5443-2	L14G3
OPI3153	H11B1	SD5443-3	L14G3
OPI3250	H11B1	SE3450-1	LED56F
OPI3251	H11B1	SE3450-2	LED56F
OPI3252	H11B1	SE3450-3	LED56F
OPI3253	H11B1	SE3451-1	LED56F
OPI4201	H11C1	SE3451-2	LED55BF
OPI4202	H11C3	SE3451-3	LED55CF
OPI4401	H11C4	SE3453-1	LED56F
OPI5000 OPI5010 OPI6000	H11C6 H11A520 H11A520 H11D1	SE3453-2 SE3453-3 SE3453-4 SE3455-1	LED56F LED55BF LED55BF
OPI6100	H11D3	SE3455-2	LED55CF
OP17002	H24A2	SE5450-1	LED56
OPI7010	H24A1	SE5450-2	LED56
OPI7320	H24B2	SE5451-1	LED56
OPI7340	H24B2	SE5451-2	LED55B
OPS690	H23A2	SE5451-3	LED55B
OPS691	H23A2	SE5453-1	LED56
OPS692	H23A1	SE5453-2	LED55B
OPS693	H23A1	SE5453-3	LED55B
PC900	H11L3	SE5453-4	LED55B
S22MD1	H11M3	SE5455-1	LED55B
S22MD2	H11M3	SE5455-2	LED55C
SCS11C1 SCS11C3 SCS11C4 SCS11C6 SD3443-1 SD5410-1 SD5410-2 SD5410-3 SD5440-1	H11C1 H11C3 H11C4 H11C6 L14C1 L14F1 L14F1 L14F1 L14F1 L14G2	SE5455-3 SE5455-4 SFH600-1 SFH600-2 SFH600-3 SFH601-1 SFH601-2 SFH601-3 SFH601-4	LED55C GFH600I GFH600II GFH601II GFH601III GFH601IV
SD5440-2	L14G2	SG1009	LED55B

COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER
SG1009A SPX2 SPX2E SPX4 SPX5 SPX6 SPX26 SPX28 SPX33 SPX35 SPX35 SPX35	LED55C H11A550 H11A550 H11A550 H11A550 H11A5100 H11A520 H11A520 H11A520 H11A5100 H11A5100
SPX37 SPX53 SPX103 SPX1872-1 SPX1872-2 SPX1872-3 SPX1872-4 SPX1873-1 SPX1873-2 SPX1873-2 SPX1873-3	H11A5100 H11A550 4N35 H22A1 H22A1 H22B1 H22B1 H22B1 H21A1 H21A1 H21A1 H21B1
SPX1873-4 SPX1876-1 SPX1876-2 SPX1876-3 SPX2762-4 SPX7271 SPX7272 SPX7273 SPX7910 SPX7911	H21B1 H21A1 H2!A1 H2!B1 H22A2 CNY17II CNY17III H11L1 H11L3
TIL31A TIL31B TIL33A TIL33B TIL34A TIL34B TIL40 TIL81	LED55B LED55B LED55BF LED55BF LED56 LED56 F5F1 L14G1

COMPETITIVE TYPE NUMBER	NEAREST HARRIS PART NUMBER
TIL99 TIL111 TIL112 TIL113 TIL114 TIL115 TIL116 TIL117 TIL117 TIL118 TIL119	L14C2 H11A4 H11A5 H11B2 H11A3 H11A3 H11A3 H11A3 H11A5 H11A5
TIL124 TIL125 TIL126 TIL138 TIL143 TIL144 TIL145 TIL146 TIL146 TIL147 TIL148	H11A520 H11A520 H11A520 H21A1 H21A1 H21A1 H21B1 H21B1 H22B1 H22A3 H22A1
TIL153 TIL154 TIL155 TIL156 TIL157 TIL411 TIL412 TIL903-1 TIL903-2 TIL904-1	H11A520 H11A520 H11A520 H11G2 H11G2 L14Q1 L14R1 F5D2 F5D2 F5E2
TIL904-2 XC88FA XC88FB XC88FC XC88FD XC88PA XC88PB XC88PB XC88PC XC88PD	F5E2 F5E2 F5E2 F5E3 F5E1 F5D2 F5D2 F5D3 F5D1

# **Optoelectronics Theory**

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# **OPTOELECTRONICS THEORY**

#### **OPTOELECTRONIC DEVICES**

This section describes the basic semiconductor devices utilized in optoelectronics, their principles of operation and their circuit functions in order to give the circuit designer an understanding of the device characteristics of interest in optoelectronic applications.

#### Light Sources

Many different light sources need to be considered, such as light emitting diodes, tungsten lamps (evacuated and gas filled), neon lamps, fluorescent lamps and Xenon tubes. Because most light emitters are designed to work as visible light sources, the information on the specification sheets is mainly concerned with the visible part of the spectrum. The information is given in photometric rather than radiometric terms. Many references contain excellent discussions of terms and definitions used in 'light' measurement; a brief coverage of the quantitative aspects of light in optoelectronics is covered in a later section of this manual. Since the characteristics and operation of the conventional light sources (i.e., lamps, flash tubes, sunlight) are familiar, the only light sources to be detailed are the semiconductor diode sources, laser diodes and light emitting diodes.

Junction luminescence, or junction electroluminescence, occurs as a result of the application of direct current at a low voltage to a suitably doped crystal containing a pn junction. This is the basis of the Light Emitting Diode (herafter referred to as LED), a pn junction diode that emits light when biased in a forward direction. The light emitted can be either invisible (infrared), or can be light in the visible spectrum. Semiconducting light sources can be made in a wide range of wavelengths, extending from the near-ultraviolet region of the electromagnetic spectrum to the far-infrared region, although practical production devices are presently limited to wavelengths longer than ≈ 500nm. LED's for electronic applications (due to the spectral response of silicon and efficiency considerations) are normally infrared emitting diodes (hereafter referred to as IRED). The IRED is an LED that emits invisible light in the near-infrared region. Forward bias current flow in the pn junction causes holes to be injected into the N-type material and electrons to be injected into the P-type material, i.e., minority carrier injection. When these miniority carriers recombine, energy proportional to the band gap energy of the semiconductor material is released. Some of this energy is released as light, while the remainder is released as heat, with the proportions determined by the mixture of recombination processes taking place. The energy contained in a photon of light is proportional to its frequency (i.e., color) and the higher the band gap energy of the semiconductor material forming the LED, the higher the frequency of the light emitted.

Harris Semiconductor offers two types of IRED's, both using a relatively low band gap, silicon doped, liquid phase epitaxially grown material. Gallium Arsenide (GaAs) is used to make an efficient and extremely reliable IRED, with a peak wavelength  $(\lambda) \approx 940$ nm. A different process is used to increase

the frequency. It is done by replacing some of the gallium with aluminum. This increases the band gap energy, yielding an IRED which emits at  $\lambda \approx 880$ nm. Due to decreased absorption in the bulk material, this gallium aluminum arsenide (GaA1As) emitter is much more efficient than the GaAs emitters. Also, the 880nm wavelength is better matched to the silicon detectors, increasing detector sensitivity. The combination of these factors leads to greatly increased overall system response. For the newer, faster couplers, such as the H11N and H11V, a GaAlAs emitter of 730nm wavelength is used. Although the GaAlAs wavelength can be widely varied by Al/Ga ratio, each change is a separate challenge in performance, cost and reliability.

It is also possible to increase the wavelength by decreasing the band gap energy. This can be done by using an element such as indium instead of aluminum to change the band gap energy, yielding a wavelength longer than 1000nm. Unfortunately, this process tends to be more challenging than GaA1As. However, the long wavelength emitters are useful in fiber optic communications, where glass fibers may be optimized for low absorption loss and high bandwidth at these infrared wavelengths.

The diode laser is a special form of LED or IRED with tightly controlled physical dimensions and optical properties in the junction-light producing region. This produces an optical resonant cavity at the wavelength of operation such that optical-electrical feedback assures highly efficient, directional and monochromatic light production. The small, intense, virtually monochromatic beam and high frequency of operation made possible with the diode laser can be of great advantage in applications such as fiber optics, interferometry, precise alignment systems and scanning systems. The precision optical cavity is difficult to manufacture and can build stress into the crystal structure of the laser that will cause rapid degradation of light output power. Although laser diodes offer high performance, they can be uneconomical and reliability must be assessed for each application.

The electrical characteristics of the LED, laser diode and IRED are similar to other pn junction diodes in that they have a slightly higher forward voltage drop than silicon diodes because of the higher band gap energy, and a fairly low reverse breakdown voltage because of the doping levels required for efficient light production.

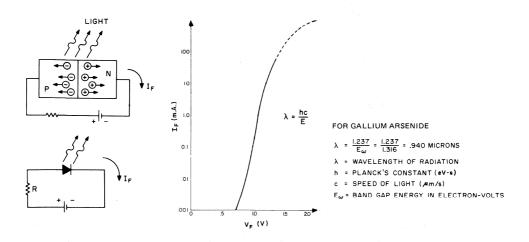


Fig. 1 - The forward biased light emitting diode pn junction.

#### Light Detecting Devices

A light source energized by electricity is only part of the semiconductor optoelectronics picture. Light detectors, devices based on mass produced silicon semiconductor technology and which convert light signals into electrical signals, are another significant part of the modern semiconductor optoelectronics picture.

**a. Photodiode** — Basic to understanding silicon photosensitive devices is the reverse biased pn junction, photodiode. When light of the proper wavelength is directed toward the junction, hole electron pairs are created and swept across the junction by the field developed across the depletion region. The result is a current flow, photocurrent, in the external circuit, proportional to the effective irradiance on the device. It behaves basically as a constant current generator up to its avalanche voltage, shown in Figure 2. It has a low temperature coefficient and the response times are in the submicrosecond range. Spectral response and speed can be tailored by geometry and doping of the junction. Increasing the junction area increases the sensitivity (photocurrent per unit irradiance) of the photodiode by collecting more photons, but also increases junction capacitance, which can increase the response time.

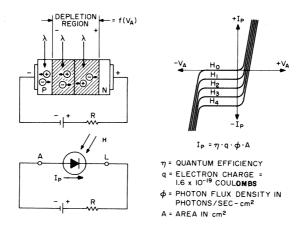


Fig. 2 - Light sensitive reverse biased pn junction photodiode.

The absorption coefficient of light in silicon decreases with increasing radiation wavelength. Therefore, as the radiation wavelength decreases, a larger percentage of the hole-electron pairs are created closer to the silicon surface. This results in the photodiode exhibiting a peak response point at some radiation wavelength. At this wavelength a maximum number of hole-electron pairs are created near the junction. The maximum of the spectral response curve of the L14G phototransistor is approximately 850nm. For wavelengths longer than this, more hole-electron pairs are created deeper in

the transistor beyond the photodiode (collector-base) junction. For shorter wavelengths, more of the incident radiation is absorbed closer to the device surface, and does not penetrate to the junction. In this manner, spectral response characteristics of the silicon photodiode are modified by the junction depth.

All common silicon light detectors consist of a photodiode junction and an amplifier. The photodiodes are usually made on a single chip of silicon from the same doping processes that form the amplifier section. In most commercial devices, the photodiode current is in the submicroampere to tens of microamperes range, and an amplifier can be added to the chip at minimal cost. Total device response to bias, temperature and switching waveforms becomes a combination of photodiode and amplifier system response.

All semiconductor junction diodes are photosensitive to some degree over some range of wavelengths of light. The response of a diode to a particular wavelength depends on the semiconductor material used and the junction depth of the diode. In some cases, light emitting diodes can be used to detect their own wavelength of light. Whether or not a particular device is photosensitive to its emission wavelength depends upon how well the bulk material absorbs this wavelength to create hole electron pairs. GaA1As, which has high output efficiency due to decreased bulk absorption at 880nm, exhibits virtually no photosensitivity at 880nm for the same reason. The GaAs emitters, however, tend to be reasonable detectors of light generated at the 940nm GaAs emission wavelength. This phenomenon can be very useful in some applications, such as half-duplex communication links.

**b.** Avalanche Photodiode — One type of amplifier system in common use can be incorporated as part of the photodiode itself. An avalanche photodiode uses avalanche multiplication to amplify the photocurrent created by hole-electron pairs. This provides high sensitivity and speed. However, the balance between noise and gain is difficult, therefore costs are high. Also temperature stability is poor and a tightly controlled, high value of bias voltage (100-300V) is required. For these reasons, the APD is used in limited applications.

**c. Phototransistor** — The light sensitive transistor is one of the simplest photodiode-amplifier combinations. By directing light toward the reverse biased pn junction (collector-base), base current is generated and amplified by the current gain of the transistor. External biasing of the base is possible, if that contact is accessible, so that the formula for emitter current is:

$$I_E = (I_P \pm I_B)(h_{FE} + 1)$$

where  $I_p$  = Photon generated base current

I<sub>E</sub> = Emitter current

 $I_B$  = Base current

h<sub>FF</sub> = Transistor DC current gain

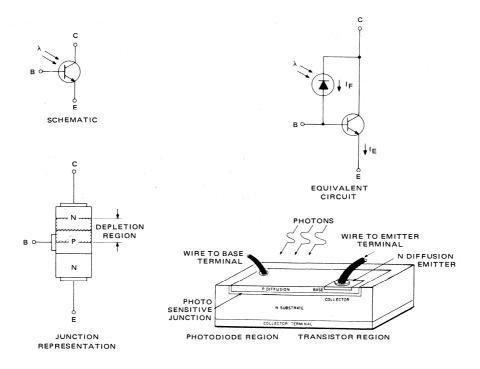


Fig. 3 - Light generated current in phototransistor.

The formula shows that the sensitivity of this transistor can be influenced by different bias levels at the base. It also indicates that response of the phototransistor will vary as the  $h_{FE}$  varies with current, bias voltage, and temperature. Speed of response is affected by a greater factor than the speed of the transistor. The switching time of the combination is usually governed by the RC time constant of the base circuit, i.e., the input time constant of the amplifier. This is due to the capacitance of the photodiode, combined with the low base currents and normally unterminated base contact causing high input impedance, and multiplied by the voltage gain  $(A_V)$  of the amplifier. This fact leads to a generalization of photodetectors: "higher gain, slower response." This generalization does not of course, cover all cases, for example, where the voltage across the phototransistor is constant  $(\Delta V_{CB} = O)$ , i.e.,  $A_V = O$ .

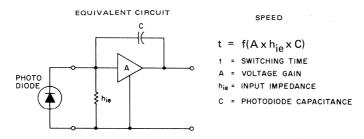


Fig. 4 - Phototransistor switching speed.

The high value of  $h_{FE}$  and large collector-base junction area required for high phototransistor sensitivity can also cause high dark current levels when the collector-base junction is reverse biased. The phototransistor dark current is given by

$$I_{CEO(DARK)} = h_{FE} I_{CBO}$$

where  $I_{CBO}$  is the collector-base junction leakage current. This leakage is proportional to junction area and periphery at the surface. Careful processing of the transistor chip is required to minimize the phototransistor dark current and maintain high light sensitivity. Typical phototransistor dark currents at 10V reverse are on the order of 1nA at room temperature and increase by a factor of two for every 10°C rise in temperature. Phototransistor specifications normally guarantee much higher dark current limits, i.e., 50 to 100 nA, due to the limitations of automated test equipment.

Dark current effects may be minimized for low light level applications by keeping the base-collector junction from being reverse biased, i.e., having a  $V_{\rm CEO}$  of less than a silicon diode forward bias voltage drop. This technique allows light currents in the nanoampere range to be detected.

A circuit illustrating this mode of operation is shown in Figure 5. The band gap effect of the highly doped BE junction of  $Q_1$  dominates the open base potential, forcing  $V_{BE(Q1)}$  to equal one diode drop. Since  $V_{BE(Q1)}$  closely approximates  $V_{BE(Q2)}$  (one diode drop each),  $V_{BC(Q1)} \approx 0$ . This creates a minimum leakage current condition.

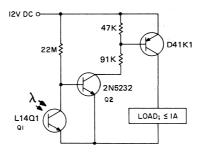


Fig. 5 - Use of phototransistor at very low light levels.

This circuit will turn the load on when illumination to  $Q_1$  drops below approximately 0.5 foot-candle.

**d. Photodarlington** — Basically, this is the same as the light sensitive transistor, except for its much higher gain from two stages of transistor amplification cascaded on a single chip.

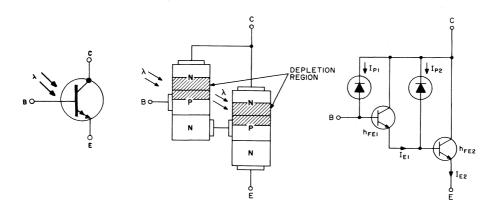


Fig. 6 - Photodarlington amplifier illustrating the effects of photon current generation.

With different bias levels at the base:

$$I_{E2} = [I_{P2} + (I_{P1} \pm I_B)(h_{FE1} + 1)](h_{FE2} + 1)$$

Since  $h_{FE} >> 1$ , a close approximation to this equation is:

$$I_{E2} \approx (I_{P1} \pm I_B)(h_{FE1})(h_{FE2})$$

To maximize sensitivity,  $I_{pl}$  should contain as large a portion of the photon produced current as possible. To accomplish this, an "expanded base" design is used, in which a large area photodiode is included in the first stage collector-base junction. This photodiode dominates the pellet topography in much the same way as shown in Figure 3 for the phototransistors.

The darlington connection is popular for applications where the light to be detected is low level, since the  $h_{FE}$  product normally ranges from  $10^3$  to  $10^5$ , assuring high electrical signal levels. As with phototransistors, speed of response suffers, since the voltage amplification can never be brought to zero due to internal parasitic impedances which cannot be eliminated from the pellet. Thus, photodarlington speed will always be less than the phototransistor. Dark current effects, as with phototransistors, are also amplified by the increased gain of the darlington connection, and can limit usefulness at high voltage, high temperature and/or high power. A base emitter resistor can minimize these effects.

**e. PhotoSCR (Silicon Controlled Rectifier)** — The two transistor equivalent circuit of the silicon controlled rectifier illustrates the switching mechanism of this device.

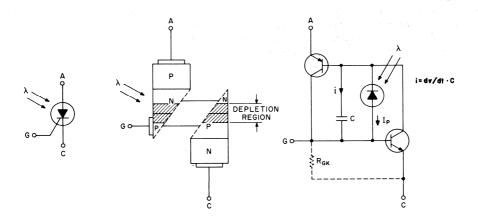


Fig. 7 - Photo SCR and two transistor equivalent circuits illustrating the effects of photon current generation and junction capacitance.

Photon current generated in the reverse biased pn junction reaches the gate region to forward bias the npn transistor and initiate switching. Part of this current,  $I_p$ , can be channeled around the gate-cathode terminal to decrease sensitivity. This is also expressed in the formula for anode current,  $I_A$ , by the expression  $(I_P \pm I_G)$ .

$$\begin{split} I_A &= \frac{\alpha_2 \{(I_P \pm I_G) + I_{CBO(1)} + I_{CBO(2)}\}}{I - \alpha_1 - \alpha_2} \\ \text{when } \alpha_1 + \alpha_2 = 1 \text{ then } I_A = \infty & I_{CBO(1)} \& I_{CBO(2)} - \text{Leakage Currents} \\ I_A &= \text{Anode Current} & \alpha = \text{Current Gain} \\ I_P &= \text{Photon Current} & \alpha_1 - \text{Varies with } I_A \text{ and } I_P \\ I_G &= \text{Gate Current} & \alpha_2 - \text{Varies with } I_A \text{ and } I_P \pm I_G \end{split}$$

In discrete device literature, photoSCR is often abbreviated LASCR, Light Activated SCR. Since the photodiode current is of a very low level, a LASCR must be constructed so that it can be triggered with a very low gate current. The high sensitivity of the LASCR causes it to be sensitive also to any effect that will produce an internal current. As a result, the LASCR has a high sensitivity to temperature, applied voltage, or rate of change of applied voltage, and has a longer turn-off time than normally expected of a SCR.

All other parameters of the LASCR are similar to an ordinary SCR, so that the LASCR can be triggered with a positive gate signal of conventional circuit current, as well as being compatible with the common techniques of suppressing unwanted sensitivity. All commercially available LASCR types of devices are of comparatively low current rating (<2A) and can thereby be desensitized to extraneous signals with small, low-cost, reactive components.

Figure 8 shows that the LASCR contains a high voltage phototransistor pnp beetween the anode (A) and gate (G) terminals. Due to physical construction details, this 'transistor' is of low gain and behaves as a symmetrical transistor, i.e., emitter and collector regions are interchangeable. Due to the low gain, photo response is quite stable in this configuration. In fact, this connection has been used with calibrated units for measurement of irradiance.

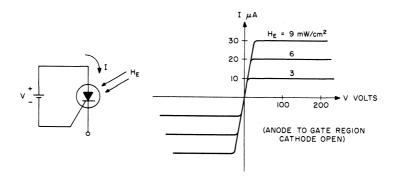


Fig. 8 - Typical pnp phototransistor action of LASCR.

Because of its high voltage junction parameters, the LASCR has unique spectral and dark current characteristics compared to the devices mentioned previously.

f. Other Photodetector Amplifiers — There are many other photodetector-amplifier combinations which are based on the previously discussed principles. The use of integrated circuit technology allows many combinations of photosensitive devices with active and passive devices on a single silicon chip. Specific examples of these are the photodarlington with integral base emitter resistor, the bilateral analog FET photodetector, the triac trigger devices and the optical input Schmitt trigger. These will be examined in detail as part of the optoisolator system.

#### OPTOELECTRONIC COMPONENTS

Detailing the basic device characteristics and operation provides an understanding of what can be expected from the semiconductor, but leaves undefined the actual component characteristics that will be affected by both device and package parameters. The basic optoelectronic devices can be packaged to provide:

- discrete detectors and emitters, which emit or detect light;
- interrupter/reflector modules, which detect objects modifying the light path;
- isolators/couplers, which transmit electrical signals without electrical connections.

The following descriptions will provide an insight into the various package characteristics and how they modify the basic devices already described.

#### Optoelectronic Detectors and Emitters

These optoelectronic components require packaging that protects the chip, and allows light to pass through the package to the chip, i.e., a semiconductor package with a window. The window can be modified to provide lens action, which gives higher response on the optical axis of the lens, greater directional sensitivity and a large aperture with less resolution. In most commercial components, the lens is also an integral part of the package, for economic reasons, so the tight control of optical tolerances is compromised somewhat to optimize chip protection via the hermetic seal. This causes lensed components to exhibit wider variations, unit to unit, than simple window components, as the optical gain variations and the basic device response variations are multiplied. Due to these factors, when high gain, highly directional optical systems are required, it is normal procedure to recommend that components without integral lenses be used in conjunction with external optics of the required quality.

The other major factor in detector/emitter packaging is the choice of a plastic or hermetic package. These may be with or without lens, although the plastic devices have the optical axis perpendicular to the leads, while the hermetic package optical axis is parallel to the leads. The hermetic package will operate at higher power, over a wider temperature range and is more tolerant of severe environments, but it is also more expensive than the plastic package. Although some components are limited to a single package type, on most the user must weigh the application's technical and economical constraints in order to optimize both the device and package of the optoelectronic component used.

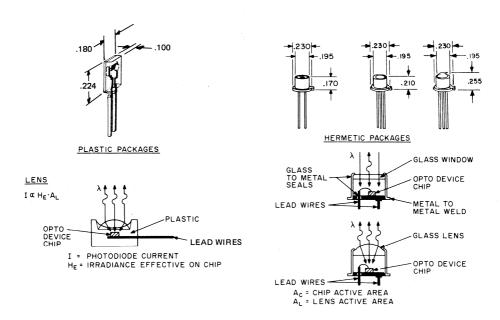
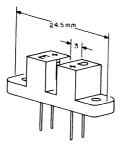
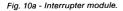


Fig. 9 - Discrete optoelectronic component package concepts.

#### Interrupter/Reflector Modules

The use of interrupter or reflector modules eliminates most of the optical calculations and geometric and conversion problems in mechanical position sensing applications. These modules are specified electrically at the input and output simultaneously — i.e., as a coupled pair — and have defined constraints on the mechanical input. All the designer need do is provide the input current and mechanical input (i.e., pass an infrared-opaque object through the interrupter gap) and monitor the electrical output. Other than normal tolerance, resolution, and power constraints, the only new knowledge required is the ability of the sensed object to block or reflect infrared light and an estimate of the effects of ambient light conditions providing false signals. This is true of both "off the shelf" commercial modules and limited volume custom modules, as the mechanical and optical parameters of any given module are fixed. Once the module is characterized for minimum and maximum characteristics, it is a defined electrical and mechanical component and does not require optical design work for each new application. This puts these sensor modules in the same design category as mechanical precision limit switches, except that the activating mechanism blocks or reflects light instead of applying a force. Thus mechanical wear and deformation effects are eliminated.





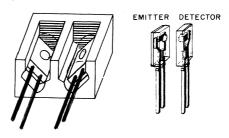
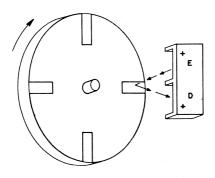


Fig. 10b - Reflector module built from H23.

Most commercially available interrupter modules are built around plastic packaged emitters and detectors. Reflective modules and other custom modules are built around both plastic and hermetic parts, depending on the required cost/performance trade-offs. It should be noted that due to the longer, angle critical, and generally less efficient light transmission path in a reflector module, lensed devices are dominant in these applications. This also explains the lack of standard reflective modules, because tight spacing between the module and the mechanical actuator must be maintained to provide adequate optical coupling, which leads to different mechanical mounting requirements for each mechanical system which is sensed.



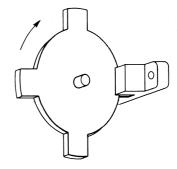


Fig. 11a - Reflector module.

Fig. 11b - Interrupter module.

### Optocouplers

Optocouplers, also known as optoisolators, are purely electronic components. The light path, IRED to photodetector, is totally enclosed in the component and cannot be modified externally. This provides one way transfer of electrical signals from the IRED to the photodetector, without electrical connection between the circuitry containing the devices. The degree of electrical isolation between the two devices is controlled by the materials in the light path and by the physical distance between the emitter and detector. (i.e., the greater the distance, the better the isolation.) Unfortunately, the current transfer ratio (CTR), which is defined as the ratio of detector current to emitter current (i.e., the effectiveness of electrical signal transfer) is inversely proportional to this separation and some type of compromise has to be made to achieve the most optimum effects. In the case of the dual in-line package, the use of optical glass has proven to be a most efficient dielectric. It allows maximum CTR and a minimum separation distance for a given isolation voltage withstand capability. Minimum (H11A5100) CTR's of 100% in combination with isolation voltages of 5000V in phototransistor couplers result. Also, because of the glass dielectric design, yields are much more predictable, due to positive alignment of IRED and detector combined with common side wire bonding, versus other methods of manufacture.

The reflector design, illustrated in Figure 12d, represents a sixth generation optoisolator, designed utilizing the knowledge and experience of 20 years of optoelectronic manufacturing by Harris Semiconductor, world leader in optoisolator technology and production. It represents the most advanced features in optoisolator design, with reliable, stable glass dielectric, eutectic mountdown die attach, large gold bond wires, and flexible protective coating over the liquid epitaxial IRED die. The reflector design has the additional advantages of:

- -highly automated assembly for enhanced quality;
- -eliminates one wire bond for improved reliability;
- -reflects IRED side light for more efficient coupling;
- —has triple layer dielectric (silicone-glass-silicone) for better isolation (higher isolation voltage, lower isolation capacitance).

It is expected that the reflector design will prove a new standard for optoisolator performance, reliability and quality as production quality and reliability experience provides the necessary data base. Large scale, controlled, reliability testing has provided indications that lead to the premise of improved reliability. Parametric data comparing production devices built with different constructions proves the improved electrical performance.

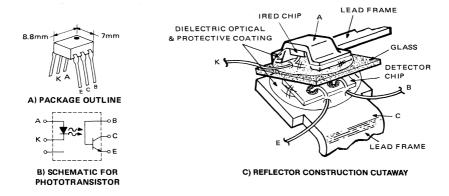


Fig. 12 - Glass dielectric construction techniques for Harris 6 pin DIP.

An invaluable modification of the glass dielectric system is the H11AV construction, which utilizes the glass as a long (>2mm) light pipe. This allows a DIP package to meet VDE isolation requirements as well as providing ultimate isolation in the six pin DIP. Isolation capacitance of this design is under 0.5pF. Note that a modification of this design, with different physical dimensions, is used to produce the AC input optoisolator with antiparallel IREDS.

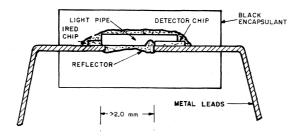


Fig. 13 - Cutaway view of Harris H11AV: 6 pin DIP optoisolator approved to VDE Safety Standard 0883/6.80, with testing to 0730/6.76 and 0860/11.76.

Although the DIP package is the most common one used for couplers, other packages are commercially available to provide higher isolation voltage and other special requirements. For very high isolation voltage requirements (10 to 50 kV) the H22 interrupter module can be modified by the user

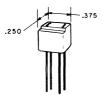


Fig. 14 - H24 optocoupler, 4000V isolation voltage.

at very low cost by putting a suitable dielectric (glass, acrylic, silicone, etc.) in the air gap and insulating and encapsulating the lead wires. For higher isolation voltages the use of the H23 matched pair with glass dielectric or the fiber optics can provide a low cost isolator. This approach utilizes a coupler system already characterized and is easily handled from a design standpoint.



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# SYSTEMS DESIGN CONSIDERATIONS

#### **EMITTER AND DETECTOR SYSTEMS**

#### Light, Irradiance and Effectiveness

When the word "light" is used in this discussion instead of "electromagnetic radiation," it does not refer to just the visible part of the spectrum, but to that part of the spectrum where silicon light sensitive devices respond to irradiance. "Light" is a misnomer for the infrared component, but it has become accepted usage.

The normalized response of silicon light sensitive devices and output sources is illustrated below. Peak spectral response is found at approximately 0.85 microns or 8500 Angstroms (Å) (1 Å= $10^{-10}$  meters) for the light activated transistors but shifts down toward 1.0 micron for the LASCR. Individual device spectral response curves are modified by photosensitive junction depth, minority carrier lifetime and surface waveplate and reflection effects. The response of the eye is shown for comparison, but it can be treated just as any other light sensitive device. When the silicon detector response and sources are compared, it is observed that the IRED GaA1As and GaAs (Si) are capable of most efficient coupling.

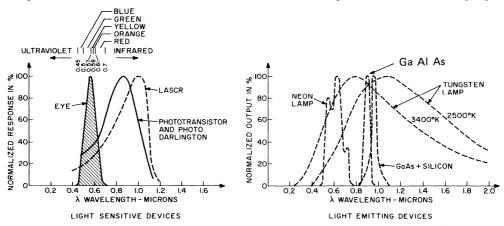


Fig. 15 - Normalized spectral characteristics of light sensitive and light emitting diodes.

Since the spectral characteristics of most sources and detectors do not match, a rigorous determination of the response of the photodetector to a given incident light level (Irradiance, H) would require: a) determining the irradiance and spectral content of the light, b) the spectral response and sensitivity of the detector, c) integrating the spectral response and spectral content to determine effectiveness, d) multiplying by the irradiance to determine the effective irradiance ( $H_E$ ) and e) multiply by the sensitivity to determine the response. If the irradiance is not easily measurable (the normal case), it is determined by: a) analyzing the power into the source ( $P_{in}$ ), b) determining the conversion efficiency of the source in producing light ( $\eta$ ) and c) defining the spacial distribution of the output and the transmissivity of the light path.

$$\text{EFFECTIVENESS} = \frac{\text{AREA UNDER CURVE C}}{\text{AREA UNDER CURVE A}} = \frac{\int_{-\infty}^{\lambda} f(A) \cdot f(B)}{\int_{-\infty}^{\lambda} f(A)}$$

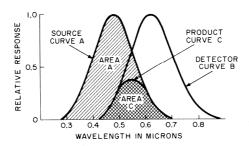


Fig. 16 - Effectiveness of Source A on Detector B.

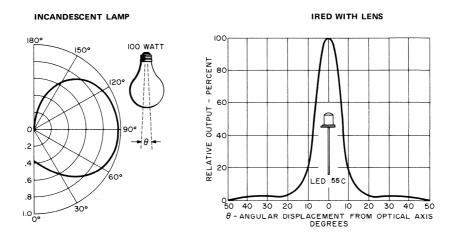


Fig. 17 - Spacial distribution of light sources.

In practice, all these parameters vary. For feasibility studies, approximations are used, then, in the prototype stage, effective irradiance is measured using calibrated detectors and "worst case" (or a distribution of) sources to analyze worst case and tolerance effects.

It is often difficult to obtain worst case samples for system evaluation purposes. In many cases, sufficient accuracy to evaluate detector irradiance levels can be obtained by using the collector base photodiode response of an unlensed phototransistor or photodarlington. The accuracy of this method rests on the conversion efficiency of silicon, a basic physical property, which peaks at about 0.6 A/W in the 800 to 900nm spectral region. For the L14C phototransistor which has an active area of 0.25mm square and peak response around 850nm, this corresponds to approximately  $1.4\mu$ A per mW/cm² with the 880nm GaA1As IRED,  $1.2\mu$ A per mW/cm² for the 940nm GaAs (si) IRED and  $0.4\mu$ A per mW/cm² using 2870°K tungsten light. The L14N phototransistor, with 1mm² active area, will provide 4 times these output currents for uniform irradiance. The inconsistency of integral lenses makes this method impractical for lensed detectors.

RADIATORS	DETECTORS	HUMAN EYE	SILICON PHOTOTRANSISTORS
Tungsten Lamp	2000°K	.003	.16
	2200° K	.007	.19
	2400° K	.013	.22
	2600° K	.021	.24
	2800°K	.030	.27
	3000° K	.044	.30
Neon Lamp		.35	.7
GaAs IRED 940nm		0	.8
GaA1As IRED 880nm		0	.98
Fluorescent Lamp		.1	.4
Xenon Flash		.13	.5
Sun		.16	.5
			1

TABLE 1: APPROXIMATE EFFECTIVENESS OF VARIOUS SOURCES

To illustrate a feasibility study using approximation, consider a 10W tungsten lamp source and a silicon phototransistor of  $1mA/mW/cm^2$  (H<sub>E</sub>)\* sensitivity, 0.1 meter (4 inches) apart:

$$P_{out} = \eta \cdot P_{in} \approx .85(10) = 8.5W$$

Conversion efficiency of tungsten lamps is 80% for gas filled and 90% for evacuated lamps.

Assuming a spherical distribution of light from the lamp —

$$H_T = \frac{P_{out}}{4 \cdot \pi \cdot d^2} \text{ mW/cm}^2 \approx \frac{8500}{12.56 (10)^2} = 6.8 \text{ mW/cm}^2$$
  
 $H_E = 0.25 \cdot H_T \text{ mW/cm}^2 = 1.7 \text{ mW/cm}^2$ 

Assuming that there are no transmission losses in the path, the phototransistor collector current is  $I_C = 1 mA/mW/cm^2 \times 1.7 mW/cm^2 = 1.7 mA$ ,

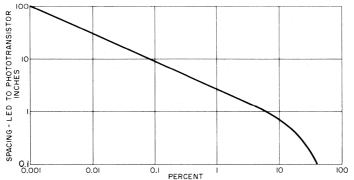
 $\begin{array}{lll} where: & P_{in} & - \ Power \ input \ (mW) \\ & P_{out} & - \ Power \ output \ (mW) \\ & d & - \ Distance \ (cm) \\ & \eta & - \ Conversion \ efficiency \ of \ light \ source \\ & H_T & - \ Total \ irradiance \ (mW/cm^2) \\ & H_E & - \ Effective \ irradiance \ (mW/cm^2) \\ & I_c & - \ Transistor \ collector \ current \end{array}$ 

For the IRED, or any lensed device, the spacial distribution of energy is determined by the lens characteristics, and no simple relationship exists for general cases. For the case of the lensed TO-18 IRED's (LED55, F5D families), with a TO-18 detector on the optical axis, analysis of the beam pattern in a piece-wise linear integration indicates:

$$H \cong 2.6 \text{ Po/(d+1.1)}^2 \text{ for } d \ge 1 \text{ cm}, \text{ as illustrated in Fig. 18}.$$

Experimental data indicates this is a conservative model, although it should be noted that the lenses exhibit a wide variation in optical characteristics.

<sup>\*</sup> $H_E=H_T$  x effectiveness (Table 1), where  $H_T$  is total irradiance.



% lensed TO -18 IRED output incident on TO -18 phototransistor lens  $(0.1 \text{cm}^2)$  of L14C, F, G, N, P axis, clear path transmission: To find Hequiv. @  $2870^\circ \text{K}$  (spec. condition) multiply Po of LED by 30 times this percentage.

Fig. 18 - Lensed LED to phototransistor coupling chart.

A F5D series GaA1As IRED will have efficiencies of 5% to 10%, and on a steady-state basis is limited to about 150mW power dissipation in a normal range of ambients. For the same 10cm spacing, using the IRED at 150mW and 8% efficiency, the transistor collector current is:

$$I_c = 2.6 (150 \text{mW}) (.08) (.98/.27) (1 \text{mA/mW/cm}^2)/(11.1 \text{cm})^2 = .95 \text{mA}$$

where the  $.98 \div .27$  factor is the spectral response correction from Table 1.

The transistor collector current is about 56 percent of the current the lamp generates, but with an input power of only 1.5% of the lamp power, the efficiency of the total system has increased approximately by a factor of 40 due to the lens and the effectiveness of the light. If the IRED is operated in a pulsed mode,  $P_0$  can be raised to 50 times the steady-state value for short times ( $\approx 1\mu \rm sec$ ) and low repetition rates (200pps), although efficiency suffers above the 500mA ( $\approx 1 \rm W$ ) bias point. The effects of lens misalignment, temperature, tolerances, and aging all must be evaluated before "worst case" or "Gaussian" expected performance can be determined, but these steps should follow initial breadboard verification of the assumptions made above. In critical applications, the LED output and transistor photodiode and gain characteristics must now be analyzed to determine response.

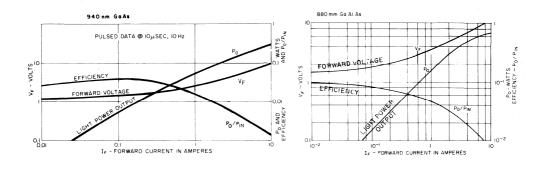


Fig. 19 - Typical power out, forward voltage and efficiency of IREDs.

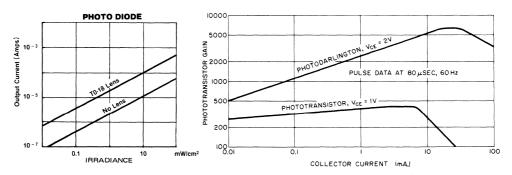


Fig. 20 - Typical photodetector current and gain.

TABLE 2: CHECK LIST OF REQUIRED SOURCE/DETECTOR INFORMATION

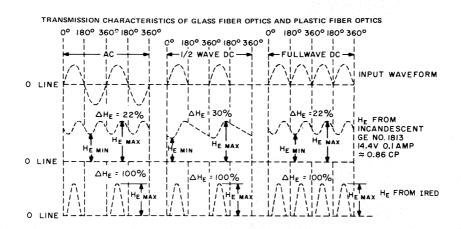
CHECK LIST	SOURCE
Relationship between the radiator's input electrical power and peak axial intensity of radiation	Specification Sheet
2. The radiator's relative radiation pattern	Specification Sheet
3. The radiator's relative output as a function of wavelength*	Specification Sheet
4. Distance between radiator and receiver	Design Requirements
5. Angular relationship between axis of radiator and receiver	Design Requirements
6. Relative acceptance pattern of receiver	Specification Sheet
7. Relative sensitivity of receiver as a function of wavelength*	Specification Sheet
8. Sensitivity of receiver	Specification Sheet
9. Light transmission efficiency	Path Material Properties

<sup>\*</sup>Numbers 3 and 7 are not needed if the effectiveness is known.

The transmission of the light from source to detector is normally not a problem and can often be checked visually. Most organic materials, e.g., plastics, have strong attenuation of near infrared wavelengths such that (although they look transparent and will work with incandescent light) they may not work with IRED's. This problem is noted on transmission paths exceeding 1 foot. The strongest common attenuations are found around 890nm in organics and 950nm in materials containing the OH radical. This problem commonly occurs in fiber optics systems because of their long path lengths. Fiber optics systems are discussed in a later section.

Another criteria for selecting the proper light source is the speed at which the system must work. As can be seen in Figure 21, applying ac or unfiltered dc to light emitting devices may change their effective irradiance by as much as 30% for tungsten lamps, or as much as 100% for IRED's. Only filtered dc will yield constant effective irradiance for all light emitting devices. For high speed data transmission, the high efficiency GaAs and GaA1As are capable of operation at frequencies greater than 1mHz when optimized. Faster diodes are difficult to build with high efficiency and long life.

In some applications it is advantageous to have an optoelectronic transceiver, a unit that can both transmit and receive via light. Although most LED's and IRED's are light sensitive, they usually are relatively insensitive at the wavelength they produce. This is true of the 880nm high efficiency GaA1As IRED, but not as pronounced on the 940nm GaAs (Si) IRED. The 940nm units also will detect 940nm radiation. The sensitivity is less than that of a silicon photodiode: typically  $0.15\mu$ A per mW/cm² on an unlensed device such as the LED55BF. Leakage current is typically under 10nA at 2V and 25°C, doubling with every 25°C temperature rise. This would provide a 20db noise margin at 15uw/cm² and 50°C in an all GaAs (Si), 940nm, transmission system without lenses on the detector. Lensed units improve sensitivity at the expense of resolution and alignment requirements.



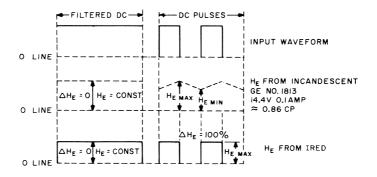


Fig. 21: Time dependance of irradiance for various power supplies.

# Lenses and Reflectors

Simple converging lenses are commonly used to extend the range and improve the directionality of optical systems. Improved directionality minimizes pick up or "stray" ambient light, as well as defining the volume in which an object can be sensed. In emitter-detector systems (as opposed to light level sensing) range is increased by focusing the light from the emitter into a beam and/or by focusing the received light on the detector. Focusing reflectors may be used to perform the same functions and are normally analyzed using the same techniques. Reflectors can offer better optical performance, and must be evaluated for cost, mechanical properties, and tolerances if considered. Optimum mechanical performance and optical efficiency is obtained when opto-electronic components without built-in lenses are used with component optics, as both range and directivity are improved over using integrally lensed devices. This is due to the better optical parameters of component lenses, compared to those integral to the semiconductor device package, which are not compromised by packaging requirements of the semiconductor material.

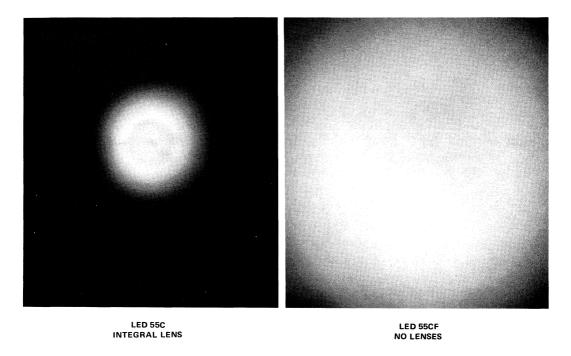


Fig. 22 - Typical infrared irradiation pattern of IRED on surface 5 cm. away (actual size).

Lenses are normally specified by the f number, i.e., focal length divided by effective diameter, and either the effective diameter or the focal length.

$$f # = \frac{Focal Length}{Effective Diameter}$$

Normally, the effect on irradiance (H), of adding a lens to the detector end of a system can be approximated by determining the ratio of the area of lens to the area illuminated in the plane of the base of the phototransistor and multiplying it by the irradiance incident on the lens. This approximation is only valid for irradiance that approximates a point source, i.e., the diameter of the light source is less than 0.1 times its distance from the lens. The lens will reflect and attenuate the result by about 10%.

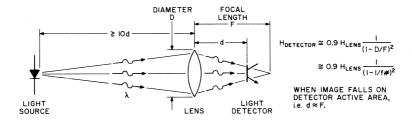
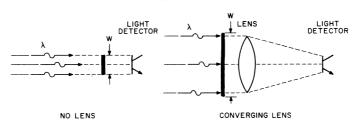


Fig. 23 - Detection with a converging lens.

Although the use of lenses narrows the field of view of the detector and alleviates some ambient light problems, it can also widen the path of light that must be blocked to turn the detector off. Resolution is always less when focusing lens systems are used on the detector without light masking.



 $\boldsymbol{w}$  is the width an object must have to block the detector from light, i.e. full on to full off.

Fig. 24 - Effect of lens on resolution.

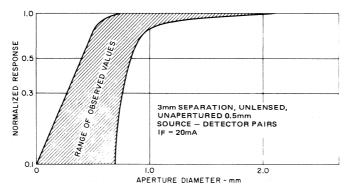


Fig. 25 - Effect of aperture size on response transparent aperture on opaque field.

With an unlensed L14C phototransistor detector, the light sensitive area is about 0.5mm (0.02 in.) square. Diffraction, tolerance and edge effects will add approximately 0.3mm (0.012 in.) to the path width which must be blocked to darken the detector. When a converging lens is added in front of the detector, the field of view is lessened, and the light path is widened by the lens system's magnification. Adding a converging lens to the light source increases the irradiance on the detector but has insignificant effect on the light path width. Converging lenses on either device makes detector/source alignment more critical as the light path and view of the devices are now "beams." The combination of lenses and apertures can tailor field of view and resolution in many applications. For high resolution applications the consistency of the lenses becomes significant. Various masking and coding techniques are used to minimize these interactions, with sensitivity or transmission efficiency usually being the parameters traded off with alignment and cost of materials.

### Ambient Light

The effect of ambient light on optoelectronics is generally difficult to estimate, since the ambient light varies in terms of level, direction, spectral content and modulation. If the detector is not highly directional, it will normally be found that all reflecting surfaces near the system must be coated with a non-reflecting material or shielded from both ambient light and reflections of light from the light source. Note that back-lighting of the detector can cause trouble by reflecting off the object that normally blocks the light path. As a final solution, a pulse encoded and decoded light system can be used to give very high ambient light immunity, as well as greatly extend the distance over which the system will operate.

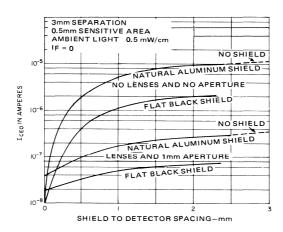


Fig. 26 - Effect of ambient light and shield finish on optoelectronic object detector.

#### Pulsed Systems

High levels of light output can be obtained by pulsing the IRED. High signal to noise ratios at the detector are obtained by AC signal processing and simple pulse decoding techniques. Such a system is illustrated in the section on Optoelectronic Circuits.

Pulsed light systems can provide significant performance improvements in detector-emitter pair applications at the expense of more complex circuit design. The cost of a pulsed system may actually be lower than that of the high power light source and sensitive detector required to do a similar job, since low cost commodity components are easily designed into a pulsed system. Performance of the pulsed system will almost always be better than a steady-state system.

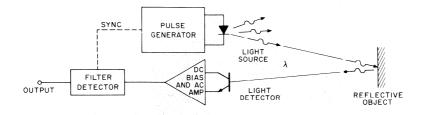


Fig. 27 - Typical pulsed reflective object sensor.

Generally, low cost systems use unijunction transistor (UJT) derived current pulses of from 1 to 10µsec at a 0.1 to 1% duty cycle, into an IRED, since shorter times do not provide corresponding increases in light output and require more sophisticated (and costly) circuits to develop the pulse. The detector is normally a phototransistor cascode biased\* by an ac amplifier of one to three transistors (low cost I.C. amplifiers are too slow). Synchronous rectification of the ac amplifier output (sychronized by the pulse generator), allows a significant increase in performance at low cost. Xenon flash tubes and laser light sources provide highest output but cost and complexity limit these to extremely high performance systems. Normal cost/performance progressions are: dc operations, no external optics; pulsed operation, no external optics; pulsed operations with external optics and exotic (laser, etc.) source systems. Occasionally, commodity plastic lenses may be found that will provide lower cost than the pulse electronics, but alignment and mechanical sytems cost must be compared against possible electronics savings.

#### Precision Position Sensing

Precision position sensing can be done using various techniques, depending on the application. Some techniques require multiple emitter detector pairs to provide the desired resolution and accuracy. Normal design practice in multiple path sensing applications is to design the light shield mechanism to provide a "gray code" output, i.e., each sequence is only one bit different from the preceding one. One advantage to such systems is that they are not affected by transients, power loss, etc. They also require one optical path per bit, with path coding hardware and initial alignment. These can prove economically impractical in many applications.

However, the availability of powerful, low-cost logic in a system requiring the position sensing function allows cost optimization by using logic to minimize the number of scanning points. Clever mechanical design of the scanning area provides the key to optimization.

To illustrate this, a rotary encoder (see Figure 28) requires only two sensors to scan the rotating disc to provide position, speed, and direction of rotation. This information is coded in the T triangle wave — the slope providing speed, the ratio of instantaneous amplitude to peak amplitude provides position within 15° increments and the phase relationship to the S-wave indicates direction of rotation. The S-wave output transitions are counted to provide the position to 15° increments.

<sup>\*</sup>Biased in this manner, the phototransistor can respond in less than a microsecond. LED current, pulse width and repetition rates can then be determined strictly from response time, distance covered, LED thermal resistance and cost constraints.

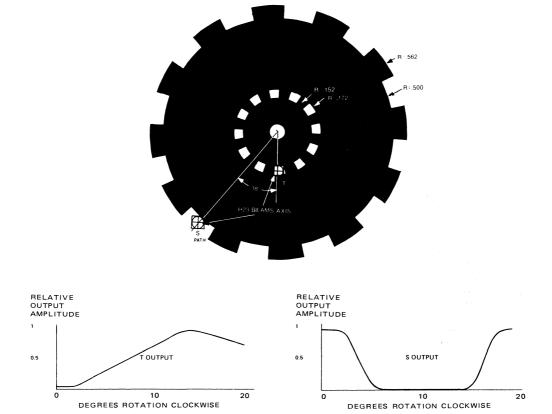


Fig. 28 - Cost optimized shaft encoder.

Linear position information can also come from two sensors. Accuracy and high resolution result from the use of Moiré fringes shown in Figure 29. The scale difference is obtained using two grating scales, as illustrated, or by using two identical scales held at an angle. The two sensors are placed within 1/2 period of each other.

As one scale is moved in relationship to the other fixed scale, each sensor output goes through a complete period for a motion of one gradient. The phase relationship between sensors outputs contains direction of motion, the slope of the waveform provides speed, and the ratio of instantaneous amplitude to peak amplitude provides distance within a grid. The number of cycles is counted for absolute position.

Additional advantages of the Moiré fringe technique are the use of large area sensor emitter-detector pairs and the non-critical initial placement of the pairs. Using the H21 module for the sensors requires that the individual masks of the grids be less than  $0.25 \, \text{mm}$  wide, cover a height of over  $1.5 \, \text{mm}$ , and the static period of the fringe pattern (dark area to dark area) be over 6mm for interrupters mounted side by side. Spacing the sensors between n and n + 1/2 periods apart eliminates the last criteria, at the expense of a more rigid, precise mechanical design.

For extremely fine gratings, note that the sensor light path can cover up to 15% of the static period with a loss of only about 10% in peak amplitude for 40% transmission gratings. The static period of the gratings is the reciprocal of one minus the ratio of grids per unit length, in units of grid length. Example, with a scale factor difference of 1.5%, the static period is  $1\div0.015=66.7$  grids. This can be verified by counting grids in Figure 29. Note that both the space between the gratings and reflectivity of the gratings can affect the observed phase difference.

Practical production units must be designed to account for those effects, as well as amplitude differences of signals in the two channels, ambient light and mechanical parameters. Fiber optics can often be used to advantage in position sensing applications. The small fiber can fit many places discrete devices would not, and the fiber is not sensitive to the electromagnetic fields found in many sensing environments.

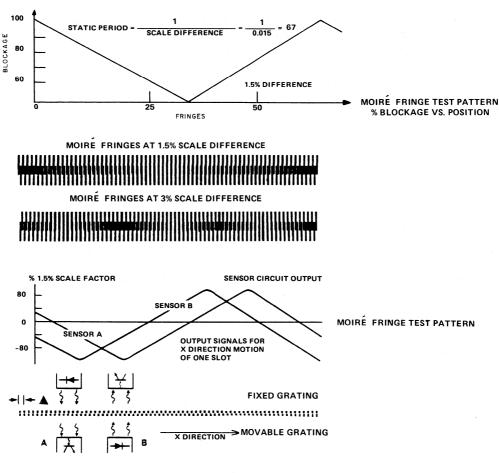


Fig. 29 - Moiré fringe test pattern.

#### **OPTOCOUPLER SYSTEMS**

The optocoupler, also known as an optoisolator, consists of an IRED, a transparent dielectric material and a detector in a common package. It has been defined previously in terms of construction and the various semiconductors which can be used in it. To utilize these devices in a circuit, the characteristics of the combined component, as well as its parts must be known. Characteristics such as coupling efficiency (the effect of IRED current on the output device), speed of response, voltage drops, current capability and characteristic V-I curves, are defined by the devices used to build the coupler and the optical efficiency. The detailed coupler specification defines these parameters such that circuit design can be done in the same manner as with other semiconductors with input, output, and transfer characteristics — except that the input is dielectrically isolated. This is the critical difference, the definition of the isolation parameters and what they mean to the design of a circuit.

#### Isolation

Three critical isolation parameters are isolation resistance, isolation capacitance, and dielectric withstand capability. Note that all three are specified with input terminals short circuited and output terminals short circuited. This prevents damage to the emitter and detector due to the capacitive charging currents that flow at the relatively high test voltages.

- a. Isolation Resistance is the dc resistance from the input to output of the coupler. All Harris couplers are specified to have a minimum of 10<sup>11</sup> ohms isolation resistance, which is higher than the resistance that can be expected to be maintained between the mounting pads on many of the printed circuit boards the coupler is to be mounted on. Note that at high dielectric stress voltages, with printed circuit board leakage added, currents in the tens of nanoamps may flow. This is the same magnitude as photodiode currents, generated at IRED currents of up to 0.5mA in a typical dual in-line darlington coupler, and could be a problem in applications where low levels are critical. Normally, care in selection and processing of the printed circuit board will minimize any isolation resistance problems.
- **b.** Isolation Capacitance is the parasitic capacitance, through the dielectric, from input to output. Typical values range between 0.3pF and 2.5pF. This can lead to noticeable effects in circuits which have the dielectric stressed by transients exceeding 500V per microsecond. This would occur in circuits sensitive to low level currents, biased to respond rapidly and subjected to the fast transients. Common circuitry that meets these criteria is found in machine tool automation, interfacing with long electrical or communication lines and in areas where large amounts of power are rapidly switched. The majority of capacitive isolation problems are solved through one or a combination of the following:
  - clean up circuit board layout especially base (gate) lead positioning;
  - use base emitter shunt resistance and/or capacitance;
  - design for immunity to noise levels expected;
  - electrostatically shield highly sensitive circuit portions;
  - use snubber capacitors coupling the commons on both sides of the dielectric.

This will lower the rate-of-rise of transient voltages and, lower currents into sensitive portions of the circuit. In applications where these techniques do not solve the noise problem a lower isolation capacitance is required. Several alternatives exist. In the standard six pin DIP package the H11AV series (which contains a > 2mm glass light pipe dielectric) provides the lowest isolation capacitance (0.5pF max.) available in this package. Where base lead pickup is indicated, the H24 series optoisolators eliminate the base lead.

c. Isolation Voltage is the maximum voltage which the dielectric can be expected to withstand. Table 3 illustrates the parameters that must be defined to qualify isolation voltage capability, which depends on time, dv/dt, and waveshape. The dependence is a function of the method by which the coupler is constructed. To illustrate the effect the voltage waveform can have on the isolation capability of a coupler, a series of tests were run to quantify these effects on both a glass dielectric and a competitive dual lead frame DIP coupler.

The results of the tests were analyzed to determine the percent difference in surge isolation voltage capability that was exhibited by the couplers for the various waveforms applied, as compared to the specified test method. These percentages were then applied to a hypothetical device that just met a 1000V peak specification. The results were tabulated to determine the "real" surge voltage capability of this device for each waveform. This was done to allow the circuit designer to determine a realistic surge voltage derating for each coupler type. Dual lead frame couplers with other dielectric materials and/or dielectric form factors may show different changes in capability with waveform. The glass dielectric is very consistent in both electrical properties and form factor and performed consistently from device to device.

TABLE 3: SURGE ISOLATION VOLTAGE CAPABILITY OF HYPOTHETICAL 1000V COUPLER

COUPLER WAVE FORM	AC ZERO Φ	DC RAMP	AC RAMP	AC STEP	DC STEP
Glass	707 V*	1025 V	650 V	580 V	919 V
Dual Lead Frame	540 V	1000 V*	540 V	510 V	780 V

<sup>\*</sup>Specification sheet test method.

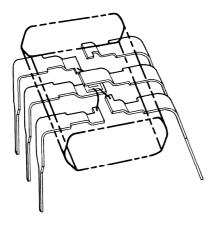


Fig. 30 - Competitive construction, dual lead frame.

# The tests performed were:

- 1. AC rms surge rating per Harris definition
- \*2. DC Ramp Value at failure when potential gradually increased from zero definition used on competitive device.
- \*3. AC Ramp rms value at failure of gradually increased potential.
- AC Step rms value at failure of instantaneously applied voltage. Application of voltage synchronized to peak voltage.
- 5. DC Step Value at failure of instantaneously applied potential.

<sup>\*</sup>ramp slope 1000V/sec

#### TABLE 4: HARRIS SEMICONDUCTOR OPTOCOUPLER ISOLATION VOLTAGE SPECIFICATION METHOD

# I. Surge Isolation Voltage

#### a. Definition:

This rating is used to protect against transient over-voltages generated from switching and lightning-induced surges. Device shall be capable of withstanding this stress a minimum of 100 times during its useful life. Ratings shall apply over entire device operating temperature range.

#### b. Specification Format:

Specification, in terms of peak and/or rms, 60 Hz voltage, for a one minute duration.

#### c. Test Conditions:

Application of full rated 60 Hz sinusoidal voltage for one second, with initial application restricted to zero voltage (i.e., zero phase), from a supply capable of sourcing 5 mA at rated voltage.

# II. Steady-State Isolation Voltage

#### a. Definition:

This rating is used to protect against a steady-state voltage which will appear across the device isolation from an electrical power source during its useful life. Ratings shall apply over the entire device operating temperature range and shall be verified by a 1000 hour life test.

# b. Specification Format:

Specified in terms of peak and/or rms 60Hz sinusoidal waveform.

#### c. Test Conditions:

Application of the full rated 60 Hz sinusoidal voltage, with initial application restricted to zero voltage (i.e., zero phase), from a supply capable of sourcing 5 mA at rated voltage, for the duration of the test.

Steady-state isolation voltage ratings are usually less than surge ratings and must be verified by life test. The Harris steady-state rating confirmation tests were performed on devices segmented by surge isolation voltage capabilities into groups of the lowest voltages that could be supplied to the specification tested. A destructive surge isolation voltage test was performed at a specified surge rating to confirm the selection process, and then the couplers were placed on rated 60 Hz steady-state isolation stress. No failures were observed on the 160 couplers tested for 1000 hours. This consisted of 32 units, H11A types, each group tested at a voltage ratio of 800/1060, 1500/2500, 1500/1770, 2200/2500 and 2500/4000 (life test to surge test voltage ratio). Note that some of the tests are beyond the rated steady-state condition for a given test voltage, again confirming the inherent properties of glass dielectric.

The failure mode of a coupler stressed beyond its dielectric capability is of interest in many applications. Ideally, the coupler would heal and still provide isolation, if not coupling, after breaking down. Unfortunately, no DIP coupler does this. The results of a dielectric breakdown can range from the resistive path, caused by the carbonized molding compound along the surface of the glass observed on glass dielectric couplers, to a metallic short, caused by molten lead wires bridging lead frame to lead frame, noted on some dual lead frame products. In critical designs, the effects of dielectric breakdown should be considered and, if catastrophic, protection of the circuit via current limiting, fusing, Harris MOV® Varistor, spark gap, etc., is indicated. Some techniques for protection are illustrated below. Note that film resistors can fuse under fault currents, providing combined protection. Breakover protection, if feasible, is probably the best choice when a coupler with adequate breakover capability cannot be obtained.

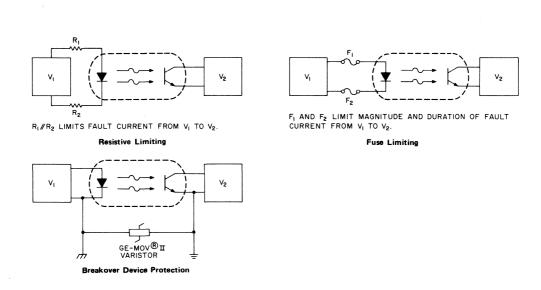


Fig. 31 - Methods of limiting or eliminating dielectric breakover problems.

Another phenomenon that has been observed in some photocouplers when subjected to de dielectric stress is a rise in the leakage current of the detector device. This phenomenon is known as "dielectric channelling" or as "ionic drift." This rise in leakage is usually observed at high levels of dielectric voltage stress and elevated temperature, although field reports indicate the phenomena has been observed at dielectric stresses as low as 50Vdc in some brands of couplers. The phenomenon seems independent of normal HTRB channelling, since it appears only under dielectric stress and not under detector blocking voltage stress. The cause is hypothesized to be mobile ions in the dielectric material that move to the detector surface under the influence of the voltage field generated by the dielectric stress. At the detector surface, the field produced by these ions would cause an inversion layer (similar to that formed in a MOS field effect transistor) to form in the collector or base region of the detector and carry the leakage current. The Harris coupler glass dielectric has been designed to be as ion free as possible and the detector devices (which are optimized for minimum susceptability to the formation of inversion layers) have proven to provide a stable, reliable and highly reproducible coupler design. Tests performed on these devices at stresses up to 1500V and 100°C produced no significant change in detector leakage.

## Input, Output and Transfer Characteristics

The complete optocoupler has the electrical characteristics of the IRED and the detector at the input and output, respectively. Since the individual devices and the dielectric characteristics are known, emphasis will be on the transfer characteristics of the coupler. Some specific device characteristics are also detailed to provide the information required for a complete analytical circuit design.

a. Input The input characteristics of the coupler are the characteristics of an IRED — usually a single diode, although the H11AA has an anti-parallel connected, two IRED input. The forward voltage drop,  $V_F$ , is slightly different than that of the discrete IRED previously discussed, due to differences in wiring and contact details. Figure 32 illustrates this for all Harris coupler types. In pulsed operation

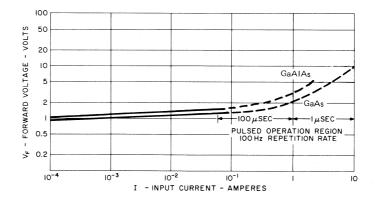


Fig. 32 - Typical optocoupler input characteristics — V<sub>F</sub> vs. I<sub>F</sub> at 25° C.

significantly higher currents can be tolerated, but close control of pulse width and duty cycle are required to keep both chip and lead bond wire from bias conditions which will cause failure. The temperature coefficient of forward voltage is related to the forward current and is of small magnitude as it changes  $V_F$  by only about  $\pm~10\%$  over the temperature range.

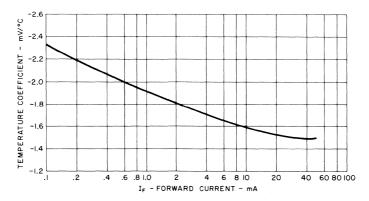


Fig. 33 - IRED forward voltage temperature coefficient.

The GaAlAs IRED of the new H11AG is quite similar to the GaAs IRED used in previous introductions, in terms of input characteristics. It exhibits a slightly higher forward voltage drop (typically 0.1V more from about 1 to 100 mA bias) with a similar temperature coefficient of forward voltage. The input capacitance, speed and reverse characteristics are quite similar to GaAs types. The outstanding advantage of the GaA1As IRED is the 3 or 4 to 1 improvement in transfer efficiency due to better radiation efficiency and detector responsivity. This improvement allows specification and application of the optoisolator down to input bias currents of  $200\mu$ A and simultaneously provides current transfer ratios exceeding 100% over the 0 to  $70^{\circ}$ C temperature range.

The stability and predictability of the IRED forward voltage drop lends itself to various threshold (like H11A10) and time delay applications. Threshold operation is accomplished by shunting the IRED with a resistor such that  $V_F$  isn't reached until the input current reaches the desired threshold value for turn-on. This type of application is documented in the specification of the H11A10.

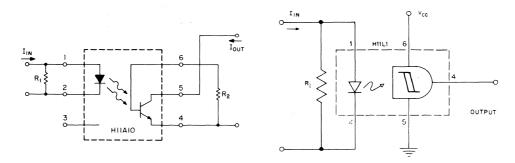


Fig. 34 - Current threshold operation of optocoupler.

The H11L1 Schmitt trigger output optoisolator gives a more precise current threshold than the H11A10, with fast rise and fall times on the output waveform. This is due to the low turn-on threshold current, the IRED current and voltage, and the hysterisis — all of which have 0° to 70°C specification minimum/maximum limits. Time delay turn-on can be accomplished by shunting the LED with a capacitor in applications where a slow turn-on and turn-off can be tolerated. In speed sensitive, time delay applications, the trade-off between time delay at the input with a Schmitt trigger output vs. incorporation of the time delay in a discrete Schmitt trigger circuit must be evaluated for cost and performance.

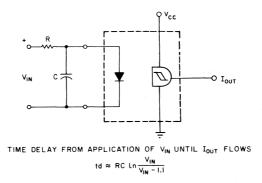


Fig. 35 - Time delay operation of optocoupler.

The input capacitance of the optoisolator is IRED junction capacitance. It is a function of bias voltage and, although normally ignored, has an effect on the turn-on time of the IRED. As the IRED is forward biased, its capacitance rises. The charging of this increasing capacitance delays the availability of current to generate light and causes a slower response than expected. In the liquid epitaxial-processed gallium aluminum arsenide and silicon-doped gallium arsenide devices, this effect is noticeable only at low drive currents, while rise time effects due to minority carrier lifetime dominates turn-on time at currents over a few milliamperes.

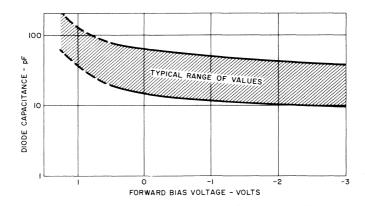


Fig. 36 - IRED capacitance as a function of bias voltage.

To minimize both effects when optimum rise time is required, the current waveform to the coupler input should have a leading edge spike, such as that provided by a capacitive discharge circuit.

b. Signal Transfer Characteristics The heart of the transfer characteristics of an optocoupler is the photodiode response to the light generated by the input current. In all isolators, the output is the combination of the photodiode response and the gain characteristics of the detector amplifier. With the transistor and darlington couplers, the photodiode characteristics are available in the collector-base connection and can be measured and utilized. Note that to use the photo-darlington as a photodiode, the

emitter of the output section must be open-circuited and not shorted to the base as can be done with a single phototransistor in this mode. This is because the base of the output transistor is not electrically accessible, so when the darlington is connected with a base emitter short, it acts not as a photodiode, but as a photodiode in parallel with a low-current-transfer ratio (ratio of output current to input current) phototransistor.

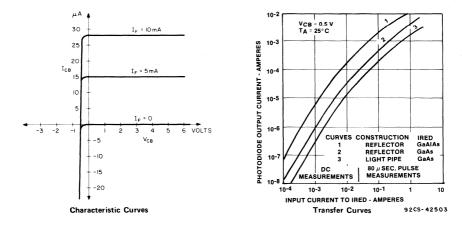


Fig. 37 - Typical optocoupler transfer characteristics — photodiode response of phototransistor and photodarlington couplers.

The photodiode response plot of Fig. 37 also illustrates the efficiency of various construction alternatives. The most efficient coupling is provided by utilizing the superior efficiency of the GaA1As IRED combined with the improved optical path of the reflector package. The least efficient illustrates the relative disadvantage of the wide spacing of the light pipe construction using the proven GaAs IRED. It also illustrates the more efficient coupling provided by the reflector design, which takes advantage of the fact that about 3/4 of the energy emitted by the IRED pellet comes from the sides of the die, which reflects side light down through the dielectric onto the detector die.

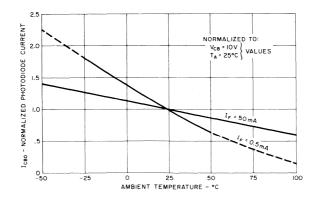


Fig. 38 - Photodiode transfer characteristics temperature variation.

More complex output devices do not normally have the photodiode output available. The bilateral analog FET has photodiode action from either of the output terminals to the substrate, but provides lower output current than the phototransistor. The photoSCR exhibits phototransistor action from anode to gate. The triac trigger devices have phototransistor action from substrate to either output terminal. The Schmitt trigger detector has no external linear output due to photodiode action because the photodiode is part of a complex circuit.

In the SCR coupler, the pnp portion of the device from anode to gate activated by the photodiode can be monitored and utilized in both forward and reverse directions as a symmetrical switch for low currents at voltages up to rated voltage. High power dissipation is possible in this configuration, so care must be exercised to avoid exceeding the dissipation ratings of the device.

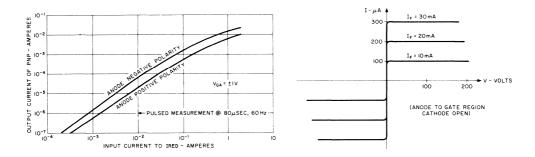


Fig. 39 - Characteristic curves — pnp phototransistor action of H11C SCR optocoupler.

Using a unijunction transistor to pulse the IRED allows the SCR coupler biased in this mode to trigger triacs and anti-parallel SCR's without a bridge of rectifiers and its problems associated with commutating dv/dt. It is also useful for switching and sampling low level dc and ac signals since offset voltage (the prime cause of distortion) is practically zero. Temperature coefficients of both the photodiode response and the pnp response will be negative, as both primarily indicate the incident light and illustrate the decrease in IRED efficiency as temperature rises.

 $\underline{c.\ Phototransistor}$  The phototransistor response is the product of the photodiode current and the current gain (h<sub>FE</sub>;  $\beta$ ) of the npn transistor. The photodiode current is very slightly affected by temperature, voltage and current level, while the transistor gain is affected by all of these factors. In the case of temperature, the gain variation offsets the temperature effects on IRED efficiency, giving a low temperature coefficient of IRED-transistor current transfer ratio (CTR). Due to voltage and current effects, this temperature coefficient will vary with bias level as illustrated in Figure 40. As different manufacturers use different processes in IRED, phototransistor and coupler manufacturing, considerable variation in the CTR temperature coefficients is found from manufacturer to manufacturer.

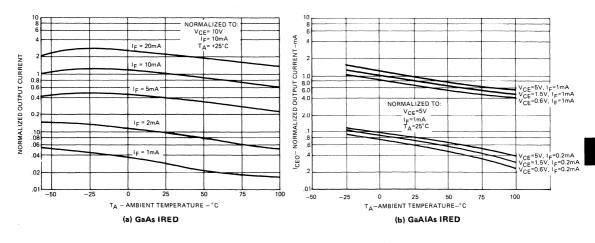


Fig. 40 - Bias effects on CTR temperature coefficient.

Dynamic response of the phototransistor is dominated by the capacitance of the relatively large photodiode, the input resistance of the transistor base-emitter junction, and the voltage gain of the transistor in the bias circuit. Through Miller Effect, the R-C time constant of the phototransistor becomes: input resistance × capacitance × voltage gain. The penalty for a high gain photo-transistor is doubled. High gain raises both voltage gain and the input resistance by lowering the base currrent. The same dual penalty is extracted when a lower operating current and higher load resistor are chosen. These effects can trap an unwary circuit designer, since competitive pressures have driven specification sheet values of switching times to uncommon bias conditions. These uncommon bias conditions include very low values of load resistors with fractions of a volt signal level changes. While this provides an idea of ultimate capability, it also forces the designer to carefully evaluate each situation.

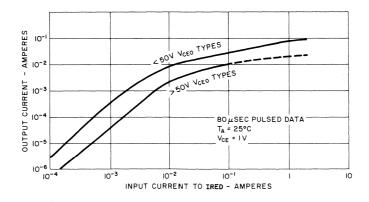
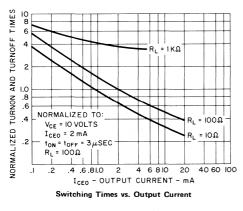


Fig. 41 - Typical phototransistor optocoupler transfer characteristics.



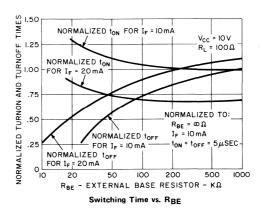


Fig. 42 - Bias effects on phototransistor switching speed.

Some applications will require speed-up techniques, such as base emitter shunt impedance, linear or cascode biasing of the phototransistor, capacitor discharge pulsing of the IRED, etc. Highest speed is obtained from the photodiode alone, biased from a stiff voltage source, with the IRED pulsed at as high a current as practical. In this mode of operation, response is dominated by the IRED and photodiode intrinsic properties and can be under 0.2 $\mu$ sec. The newer IRED used in the H11N and H11V Series has response times of less than 70 ns. Use of a load resistor in the photodiode requires charging the photodiodes capacitance (25pF at OV, typically) with the associated R-C time constant.

Leakage current of the phototransistor must also be considered (especially if the base is open-circuited) when high temperature operation and/or low current operation is desired. The photodiode leakage current (typically 200pA at 10V, 25°C) will be about 200 times this at 100°C. In the open base bias mode, this current is multiplied by beta, which also increases with temperature. This combination of effects raises a typical 2nA  $I_{CEO}$  at 10V, 25°C to  $4\mu A$  (2000 times) at 10V, 100°C. Consider the effect on a circuit, which operates at a  $100\mu A$  phototransistor current, with a device having the specified maximum leakage limit, 100nA at 25°C, when the ambient temperature rises. The use of a 10 megohm base emitter resistor would allow the worst case unit to operate normally without appreciable effect on the CTR. Leakage and switching speed effects must be considered before opting for operating open base. Higher operating voltages and/or a time varying dielectric stress (which provides capacitive base current drive) are additional factors which can cause undesired leakage effects.

The availability of the H11AG series phototransistor coupler with GaA1As emitter minimizes the problems encountered of low input currents and high temperatures. Due to the high efficiency of this series, photocurrents in the photodiode detector are increased by about 4 times. As leakage currents are not affected by the more efficient design, this directly translates to an improvement in capability. This improvement is illustrated by the specification guarantees of  $200\mu$ A input current operation over the 0 to  $70^{\circ}$ C temperature range.

d. Photodarlington The photodarlington adds the effects of an additional stage of transistor gain to the phototransistor coupler. The changes in CTR, its temperature coefficient, leakage currents and switching speed are extended from the photodiode-phototransistor relationships, and will not be detailed. Instead, the two major application areas where the photodarlington optocoupler is attractive, low input currents or at very high output currents, will be examined for device characteristics and their interaction with application performance.

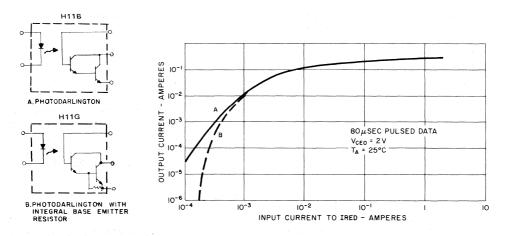


Fig. 43 - Typical photodarlington optocoupler transfer characteristics.

The high gain of the darlington permits useful output currents with input currents down to 0.5 mA. Both current gain and IRED efficiency drop very rapidly with increasing current, as illustrated in the emitter and detector systems section. These effects indicate that for very low input currents, i.e., below  $100 \text{ to } 500 \mu\text{A}$ , better performance in output current to leakage current ratio, can be obtained with the phototransistor coupler (although effort is required to get even fair performance at such low input currents, regardless of the output device). This defines the low input current operation region as roughly between 0.3 mA and 3 mA input current, and the high current output region at above 3 mA input current, i.e., where the output current is in the tens and hundreds of mA.

Operation in the low input current region with a photodarlington output optocoupler provides minimum output currents in the 0.1 mA to 10 mA range at  $25 \,^{\circ}\text{C}$ . High temperature leakage currents ( $I_{\text{CEO}}$ ) can also be in this range and the rise in output current with temperature does not approach the rise in leakage current. This effect indicates the need for a base emitter resistor in circuits which must

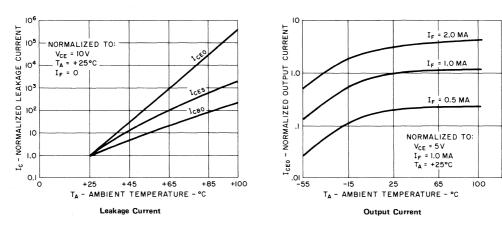


Fig. 44 - Typical temperature effects on photodarlington output.

operate at high temperature. The resistor can be external and/or integral to the darlington structure. With external resistors, the value selected for the resistor becomes a trade-off between minmizing the effect on output current, maximizing the effect on leakage current, and choosing a commonly available resistor. Usually, the result of the trade-off is the use of a 22 megohm resistor with the circuit designer providing more drive for the IRED, an alternative preferable to using a non-standard or series combination of resistors. Observing the photodiode response, and noting that V<sub>BE</sub> can be 1.3V, the 22 megohm resistor eliminates response on a typical unit for input currents less than 1/4mA, which, in worst-case analysis, makes the reason for providing more input current obvious. It also illustrates another reason for using a transistor output coupler in some of the lowest input current applications. At low temperatures, these phenomena make the darlington more attractive: leakage current has decreased, making a base emitter resistor unnecessary; IRED efficiency has increased and darlington gain has dropped, producing an output which is more a function of the input than the output device characteristics.

The integral base emitter resistor, as found in the H11G series, shunts the output stage base emitter of the photodarlington. It provides most of the advantages of an external resistor without the need for an additional component. Also, since the semiconductor design engineer can quantify maximum leakage levels, this resistor allows the photodarlington voltage and current capability to be simultaneously increased without danger of thermal runaway due to leakage currents. The H11G45 and H11G46 specifications illustrate the improvement of low current performance provided by the internal base emitter resistor. These devices are specified for operation at 1/2 mA input current, and maintain both high current transfer ratio ( $\geq 350\%$ ) and low leakage ( $\leq 100\mu$ A) over the 0 to 70°C temperature range. At higher current and voltage bias conditions, a comparison of the H11G1 with the H11B1, a photodarlington without integral resistor, illustrates the advantage. The H11G1 has 50% more current capability (150mA) and four times the  $V_{CEO}$  capability (100V). The integral resistor also provides an antiparallel diode between collector to emitter. This can be used to advantage for ac current switching using two detectors in inverse polarity series connection. The diode is of relatively low current capability, and its power dissipation must not be exceeded when operating in this mode.

Switching speeds in the low input current bias region are quite slow, and are decreased further by the large load resistors common for these biases. Some bias conditions have been reported where the photodarlington would not switch (full on to full off) at a 60Hz rate. The major point to note is that dynamic effects as illustrated in Figure 45, exist and must be allowed for in the early stages of circuit design and development.

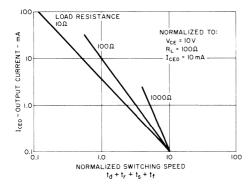


Fig. 45 - Photodarlington switching speed as a function of bias.

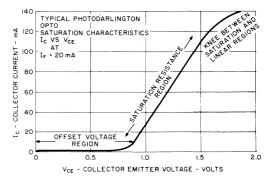


Fig. 46 - Typical photodarlington optocoupler saturation characteristics.

Operation of the photodarlington optocoupler at high output currents from low supply voltages has few pitfalls. Leakage, temperature, and dynamic effects are less critical due to normal bias levels. Current levels can be sufficiently high such that power dissipation can become a concern when driving low impedance loads, such as solenoids and small lamps. Saturation resistance and offset voltage are the prime factors which govern the power dissipation in these applications. Typical values for saturation resistance, up to  $I_C = 100 \text{mA}$ , are in the 4 to 8 ohm range. Typical offset voltage can be approximated by the 10mA collector current saturation voltage, which ranges from 0.8V to 1.1V. Power dissipation in the saturated photodarlington can now be approximated by:

$$P_d \approx I_c (V_{OFFSET} + I_c R_{SATURATION}).$$

For steady-state loads this corresponds to a maximum collector current limited by the 150mW maximum rating. In pulse applications, the decrease in photodarlington gain with increasing current, limits usefulness at high collector current. Since saturation resistance and gain rise with temperature, while offset voltage decreases, the dominant effect will depend on the collector current, the input current magnitude, and the transistor junction temperature. In high current pulsed operation, self-heating effects (in the IRED by reducing its efficiency, and in the darlington by raising the saturation resistance) can cause the observed saturation voltage to rise throughout the duration of the pulse. In higher supply voltage applications, above 25V, power dissipation due to leakage currents must be analyzed for thermal runaway.

e. PhotoSCR The photoSCR optocoupler differs from other SCR's due to the very low level gate drive available from the detector. This low level gate drives requires a very sensitive gate structure, while application constraints demand a SCR capable of operation on 120 and 240V ac lines, biased from a full wave rectifier bridge. These needs conflict and require the SCR chip design, processing and application to be carefully controlled. The success of the H11C series is a tribute to Harris' superior technology in SCR's, IRED's, and optocoupler assembly being successfully combined. The SCR optocoupler requires the circuit designer to consider the trade-off between optical sensitivity and sensitivity to dv/dt, temperature, and other undesirable effects. It also presents the circuit designer with a new effect, coupled dv/dt, where the rapid rise of voltage across the dielectric isolation capacitively supplies gate trigger current to the SCR. Due to the physical construction of the coupler, this could occur in either stress polarity, although highest sensitivity is with the IRED biased positive. These effects are not as formidable as might be anticipated, since the low currents at which the SCR is operated make the protection techniques identical in both method and typical values, to those required in most common low current SCR applications. Pulse current capability of the SCR is superb, making it ideal for capacitor discharge and triggering applications. Complete isolation of input and output enables anti-parallel and series connections without complicated additional circuitry. This facilitiates full wave ac control, high voltage SCR series string triggering, three-phase circuitry and isolated power supply design. The H74C series coupler is specified to drive 120/220Vac loads with input signals directly from TTL logic.

A knowledge of the SCR turn-on parameters eases analytical circuit design. The current into the IRED ( $I_{FT}$ ) required to trigger (turn-on) the SCR, is the principle parameter and approximates the current required to increase detector current enough to provide a diode drop of voltage across the gate-to-cathode resistor ( $R_{GK}$ ). From this the relationship of  $I_{FT}$  to  $R_{GK}$  is inferred, i.e., higher  $R_{GK}$ , lower  $I_{FT}$ . As  $R_{GK}$  also shunts currents generated by leakage, rapidly rising voltages across the junction

or isolation capacitance and stored charge during turn-off, it becomes obvious that a trade-off exists between optical trigger sensitivity and suspectibility to undesired triggering and ability to turn off. Turn-off is related to the holding current,  $I_H$ , the minimum anode current that will maintain the SCR in conduction. Because it is normally desirable to have the SCR turn-on with minimum IRED current, while being completely immune to dv/dt and other extraneous effects, and preserve dependable, rapid turnoff, the choice of a fixed value of  $R_{GK}$  becomes a compromise. Use of active devices in the place of, or in addition to,  $R_{GK}$  can provide the best solution, but at the price of additional circuit complexity.

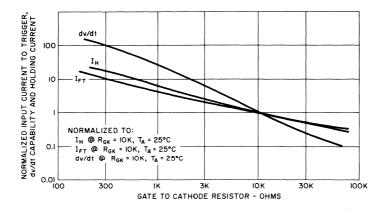


Fig. 47 - Typical effect of R<sub>GK</sub> on I<sub>FT</sub>, dv/dt, and I<sub>H</sub> of H11C SCR optocoupler.

Circuit component cost could be decreased through the techniques shown in Figure 48 by using a less costly coupler and less elaborate drive and snubber circuitry. Three examples of this type of gate bias are illustrated. The gate capacitor is simplest, but only affects dynamic response and is of limited use on dc

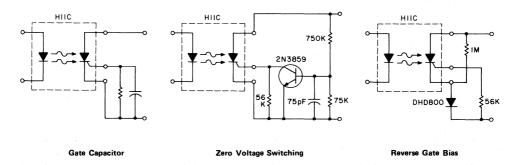


Fig. 48 - Methods used to optimize R<sub>GK</sub> effect.

or full wave rectified power. The zero voltage switching is the most effective, since it places a virtual short circuit from gate-to-cathode when the anode voltage exceeds approximately 7 volts. At low voltages, the SCR is quite immune to most of the effects mentioned, and yet optical triggering sensitivity is relatively unaffected. This circuit is limited to applications where zero voltage switching is compatible with performance requirements, of course. The reverse gate bias method is generally

applicable to a wider range of circuit applications and provides somewhat better than a 2:1 performance advantage over a simple resistor. It also improves turn-off time and is of particular advantage when the SCR is used on full wave rectified power sources. When gate-to-cathode resistors of over 10K are used, the high temperature operating capability of the SCR will be compromised without the use of some circuit which will perform similar to these. High junction temperatures are associated with either high ambient temperature or power dissipation caused by current flow, leading back to the compromise between input current magnitude and circuit simplicity. The ultimate in performance combines both techniques in one circuit—but also again limits application to zero voltage switching.

If very low drive currents are available for the IRED, and precise phase control is not required, the input current can be stored in a capacitor which is then discharged through the IRED periodically. A programmable unijunction circuit, using a  $0.2\mu F$  capacitor charged to 8V and discharged at 1msec. intervals draws less than 2mA average current and will turn-on a H11C1 with a 1K ohm  $R_{GK}$ . Other methods of overcoming the sensitivity compromise will undoubtedly suggest themselves to the circuit designer, and may prove to be higher performance, less costly, or both. To aid in the analysis of dynamic effects, typical capacitance values of 25pf anode-to-gate and 350pf cathode-to-gate are noted on the H11C photocoupler and the typical gate-to-cathode diode voltage drop is approximately 0.5V with a negative temperature coefficient of approximately  $2mv/^{\circ}C$ .

Use of the photoSCR coupler on dc circuits presents no new problems. DC stability of the Harris glassivated SCR pellet is excellent and has been proven in both the lab and field at voltages up to 400V. Commutation or other turn-off circuitry is identical to that detailed in the GE SCR Manual and a maximum turn-off time of  $100\mu$ sec is used to calculate the commutation circuit values. Pulse current capability of the H11C photoSCR coupler output is rated at 10A for  $100\mu$ sec. In conjunction with the  $50A/\mu$ sec, di/dt capability (di/dt indicates the maximum rate of increase of current through the SCR to allow complete turn-on and, thus, avoid damaging the device due to current crowding effects) of the H11C, it is capable of excellent capacitor discharge service.

For general pulse applications, the power dissipation may be calculated and used in conjunction with the pulse width, transient thermal resistance, and ambient temperature to determine maximum junction temperature, since the junction temperature is the ultimate limit on both pulse and steady-state current capability. A more complete explanation of this method of determining capability may be found in the GE SCR Manual and its reference material.

**f. Bilateral Analog FET Optoisolator** The bilateral analog FET optocoupler consists of a symmetrical, bidirectional silicon detector chip, which provides the characteristics of a bidirectional FET when illuminated, closely coupled to an infrared emitting GaAs diode source. The resulting photocoupled isolator provides an output conductance that is linear at low signal levels. The value of conductance is electrically controlled by the magnitude of IRED current over a range of from a few nanomhos to a few millimhos ( $10^{8}\Omega$  to  $10\Omega$ ). The stability of conductance is excellent, as expected from a silicon device. At higher bias voltages the output device current saturates at a value roughly proportional to the IRED current and remains relatively constant out to the breakdown voltage of about 30V. As the shunt capacitance of the detector is low ( $\approx 10$ pf) and the VI characteristics exhibit a very small offset voltage at zero current, the detector can be viewed as a remotely variable current controlled resistor for low level signals.

In circuits, the bilateral analog FET optocoupler can act as a nearly ideal analog switch or as the foundation for compression or expansion amplifiers with superb performance. The bilateral, low and high voltage characteristics are best understood by examining the detector V-I curves at appropriate voltage levels as a function of IRED drive. These can then be related to curves that define the maximum signal level for which output conductance is linear and the effects of IRED current on both output conductance and output current at high bias voltage. Note that these plots are based on pulse measurements, and the effects of IRED self heating due to power dissipation must be considered in steady-state operation. The region of linear output conductance can be illustrated in several ways,

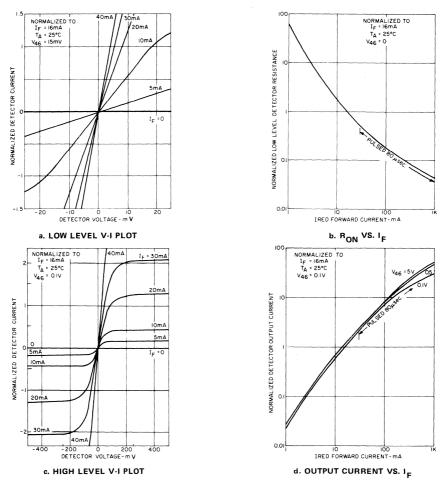


Fig. 49 - Bilateral analog FET characteristics.

although for circuit design, the most useful is defining maximum signal voltage or current and maximum Thevinen equivalent source voltage and resistance. Linear operation limits are determined utilizing a balanced bridge technique in which signal level is increased until detector nonlinearity unbalances the bridge and causes a proportionate output signal—usually 0.1%. Offstate impedance of the detector is determined by junction leakage currents and capacitance. Leakage current is typically 100pA at 15V and 25°C, or equivalent to 150g $\Omega$ , and rises an order of magnitude for each 22°C temperature rise. Junction capacitance is typically 10pf, at zero volts, and decreases with increasing detector voltage bias.

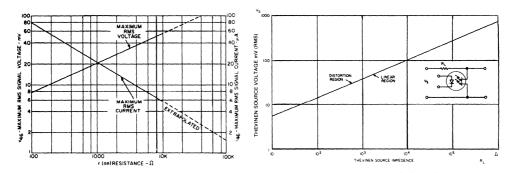


Fig. 50 - H11F bias limits for linear conduction.

The switching speed of the device is determined by detector junction capacitance, the availability of photon generated charges, and the time constant of the output impedance with its shunt capacitance and the equivalent Miller effect gain. Non-saturated switching times plot exponential waveforms that are better described by time constants, and in saturated switching the turn-on exponential is truncated by saturation. In most circuits, these effects combine to make turn-on appear faster than turn-off. The corresponding equations for nonsaturating switching show the ratio of voltage across the device during switching to its final value to be:

$$\begin{array}{lll} \mbox{for turn-on} & V_{7}/V_{\infty} \,=\, 1 \,-\, e^{-[\tau\,\times\,10^{9}/(5\,R_{L}\,+\,1500)]} \\ \mbox{for turn-off} & V_{7}/V_{\infty} \,=\, 1 \,-\, e^{-[\tau\,\times\,10^{9}/(6\,R_{L}\,+\,1500)]} \end{array}$$

for load resistor values over  $10K\Omega$ . Both rise time and fall time approach  $3\mu$ sec with lower values of load resistors. The rise time waveform is truncated when the device current becomes circuit limited, while the turn-off waveform is relatively unaffected by saturation. Delay time at turn-on is governed by the IRED, varying from 1 to  $10\mu$ sec as IRED current is reduced from 50mA to 2mA.

Offset voltage of the H11F (i.e., the detector voltage at zero detector current) is small, but may have an effect in some circuits. Typically, it is less than 0.5mV at all bias levels. The magnitude is affected by both IRED bias current and temperature, and is greatest at very low IRED currents. The magnitude of offset voltage of the H11F is comparable to that of most operational amplifiers it will be used with, so it can be ignored in many circuits.

g. Triac Driver Optoisolators The recognition that a large portion of the optoisolator applications functionally allow digital logic circuits to control ac line operated equipment led to the design of new detector device family. These detectors were not designed to act as ac load current switches, but to be pilot devices for triggering power triacs. These devices make possible significant reductions in components and circuit size when compared to circuits using phototransistor or photoSCR optoisolators.

Triac driver detector design combines high voltage signal transistor processing techniques with nonisolated, small scale I.C. circuits, providing a relatively low cost detector pellet, with bilateral symmetrical V-I characteristics. This is accomplished with a combination of lateral pnp-vertical npn transistor structures and diffused base bypass resistors. The npn and pnp transistors are connected to form two antiparallel pnpn's on a silicon pellet. The npn structure is designed to be photosensitive. Planar passivation on the pellet surface is necessary in this type of design, which places an effective upper limit on breakdown voltage capability. The device structures are constrained such that slow turn-off and low dV/dt capability are inherent, and they combine to severely limit commutating dV/dt capability. Additionally, the lateral pnp structure insures a high on-state voltage drop. Due to these characteristics, the circuit designer using a triac driver will utilize different design details, when compared to the rugged, traditional power semiconductors, to ensure reliable, dependable operation.

The planar construction allows pellet design flexibility that has not been available in traditional power semiconductors. Most impressive is the ability to form a gate resistor that can change value as a function of the device's voltage. This can be designed to improve static dV/dt capability, to increase light sensitivity, or to approximate the zero voltage switching function, again providing the opportunity for circuit simplification and the possibility of cost reduction. The cutaway construction drawing of Figure 51 illustrates the simple construction. Note the n-type silicon substrate on these devices is connected to a package terminal. With ac bias on the detector, the substrate will be biased one diode drop below the most positive terminal. In ac applications, any connection to this terminal can cause circuit malfunction or device damage.

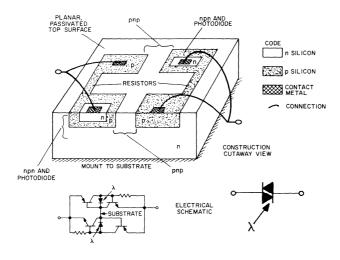


Fig. 51 - Simple triac driver concept

The application of the triac driver provides simple, flexible ac power control. The device characteristics demand some design effort to compensate for certain characteristics and to assure dependable, reliable, circuit operation. In general, more protection is required as peak power, line voltage and frequency increase. The triac drivers must be protected against voltage breakover. Planar devices are more susceptible to breakover damage than other power devices, and power line transient voltages commonly exceed 1000V.

False firing (detector turn-on without IRED turn-on) due to dV/dt can be prevented by using a snubber network. A proper snubber will eliminate false firing due to dV/dt associated with power line switch on, inductive loads, and high frequency "hash" on the line. The dV/dt withstand capability of the triac driver decreases rapidly with increased detector voltage and temperature. The dV/dt capability is appreciably lower than that of typical power triacs and will usually require use of more snubber capacitance than the power triac needs. In some cases, a two-stage RC filter is required to eliminate dV/dt problems, and can often be implemented by using the power triac snubber as the first stage. Breakover damage is easily prevented with a Harris MOV® Varistor. Surge current protection is recommended for loads which can provide over 2A peak current, since this current can flow through the triac driver while the power triac is turning on. This protection is provided by use of a series resistor. These protection techniques are illustrated in Figure 52.

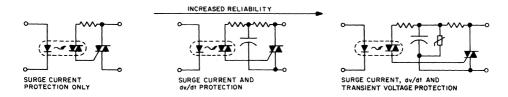
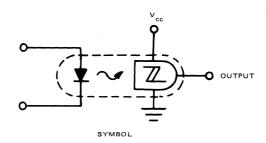


Fig. 52 - Elimination of triac driver malfunction and failure.

For some low voltage, low current applications, the triac driver can be used as a power switch, i.e., without a power triac. The major factor governing these applications is the commutating dV/dt capability of the triac driver. This represents the susceptibility of the triac driver to dV/dt triggering in one polarity immediately after conduction in the opposite polarity. Self-heating due to power dissipation, the negative temperature and voltage coefficients of dV/dt(c) and the wiring and source inductance of the circuit limit the range of application. Prudent circuit design dictates 60Hz, noninductive loads, be limited to under 0.5W.

h. Schmitt Trigger Output Optoisolator The H11L, optically isolated Schmitt trigger, has a medium speed, digital output integrated circuit detector. This unique detector provides the Schmitt trigger with functions of gain, fast switching and accurate threshold and hysteresis operating from an integral photo diode. As an optoisolator, it performs as a nearly ideal current input Schmitt trigger, furnishing electrical isolation between input and output to prevent undesired feedback. The circuit design provides almost foolproof operation, free from latch-up, oscillation, and providing relatively stable turn-on and turn-off threshold currents over a wide range of operating temperatures and voltages. The open collector output transistor on the detector chip is specified to sink over 16mA at 0.4V from an input current threshold of 1.6mA. All static parameters are specified over a 0 to 70°C. temperature range.

The equivalent circuit of the H11L illustrates the design features. The photo diode dominates the chip topography and provides efficient light collection. The preamplifier has a low input impedance to preserve speed, and features a clamp to prevent IRED overdrive of the photodiode from increasing switching times or causing other undesirable effects. The amplifier output current is added to a reference current and both produce (across a resistor) the Schmitt trigger input signal. This method of reference allows compensation for voltage and temperature coefficients throughout the operating range.



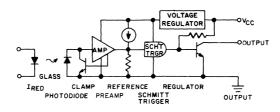


Fig. 53 - H11L equivalent circuit diagram.

The open collector output stage can sink up to 50mA, although saturation resistance and gain factors combine, such that up to 1.5V drop has been observed at 5V supply voltage. The base of the output transistor is driven resistively from an unregulated supply voltage, causing the saturation voltage to decrease at higher supply voltages. Saturation resistance of the output transistor is typically between 8 and 16 Ohms. The internal voltage regulator assures power supply rejection in the amplifier section and threshold stability in the Schmitt trigger portion.

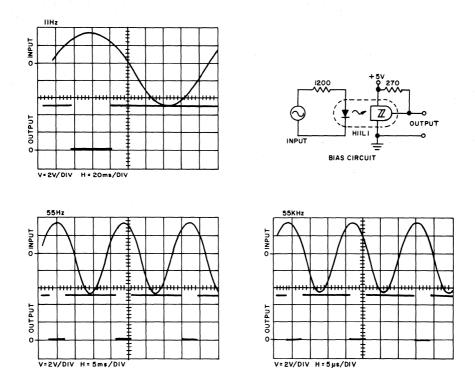


Fig. 54 - Schmitt trigger optoisolator operation illustrated at various frequencies.

Application of this opto isolator is straightforward in most applications. The function is simple, and the specification provides detailed data for worst case design. Switching characteristics are the only parameters complex enough to require further explanation. The switching times of the H11L are governed by the IRED switching speed, the photodiode response times, R-C time constants through the amplifier circuit and the switching time of the Schmitt trigger stage. The Schmitt trigger switching time, which translates to output rise and fall time, is usually under 100ns. This is approximately 10% of the

total switching time. The limiting factor in a simple circuit (i.e., resistive IRED bias) is IRED turn-off and turn-on time, which can be shortened by injecting charge into the IRED at turn-on and removing the charge at turn-off. Normally accomplished with a speed-up capacitor shunting the IRED current limiting resistor, this will reduce propagation delay times by one-third. Although further reductions in turn-on or turn-off delay can be obtained by IRED bias, maximum toggle frequency will decrease. Investigation shows turn-on times decreasing with higher IRED drive, while turn-off times increase.

At low repetition rates, fastest times will be obtained with resistive limiting of IRED current to slightly over turn-on threshold and capacitive charge injection-removal of about 0.8nC per mA IRED current. At high repetition rates or for short pulses, the overdrive supplied at turn-on fills both emitter and detector with charge which must be removed at turn-off, since the pulse time is too short for it to dissipate. Because of this, fastest square wave and short pulse response is obtained with resistive limiting of IRED current to about twice turn-on threshold and capacitive charge injection-removal of about 0.4nC per mA. This approximates specification sheet test conditions, where most H11L1 devices will operate at 500kHz (i.e., a 1MHz NRZ data rate).

Due to the higher threshold current and wider range of threshold currents found in the H11L2, compared to the H11L1, its maximum frequency capability, in a worst case bias circuit design, will be less. Switching time is also a function of detector supply voltage. Although turn-on time increases slightly with decreased supply voltage, turn-off time decreases more. Therefore, highest frequency operation will be obtained at a 3V supply voltage, using an H11L1 with speed-up capacitor.

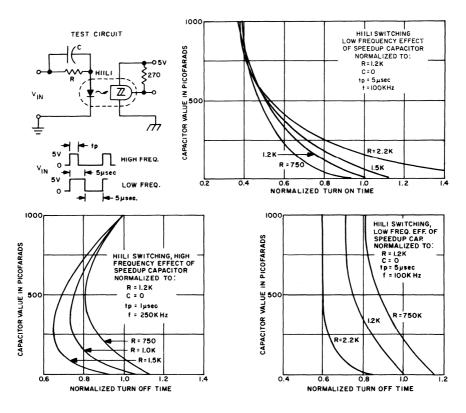


Fig. 55 - H11L switching.

The isolated Schmitt trigger action, with well-defined input threshold limits, provides a nearly ideal link to input information to logic systems. It can be used to monitor ac power line voltage, telephone lines for ring voltage and/or line current, inter-system data lines, and other currents and/or voltages. The fast transition times and wide supply range are compatible with most IC logic families. To minimize design time for these circuits, a bias resistor chart is provided in Figure 56. The input circuit

LOGIC FAMILY	V <sub>cc</sub>	R1	R2
TTL —			
-74, 74H, 74S	5V	390	0
-74L, 74LS, MSI, LSI	5V	3.3K	0
HNIL	15V	1.8K	0
CMOS —			
-3V Supply	3V	1.2K	0
-12V Supply	12V	5.6K	0
12L	5V	7.5K	27

BIAS CIRCUIT
FOR TTL, HNIL, CMOS,
12L, NMOS AND PMOS

NMOS and PMOS Biases per Manufacturer's Instructions.

Fig. 56 - H11L input for logic circuits, suggested bias resistors.

is designed to provide threshold current to the IRED from the specific monitor function. Fairly accurate ( $\pm 20\%$ ) current and voltage turn-on/turn-off limits can be set using the programmable current sensing circuit previously described (H11L specification), an advantage when line noise is of a significant amplitude compared to the signal level.

Logic circuit drive requirements for the H11L are straightforward from logic circuits capable of providing the 1.6mA or 10mA current to drive the IRED. Buffer circuits are required for lower output current capability devices. Logic drive of IRED's and buffer circuits are illustrated later in optoelectronics circuits.

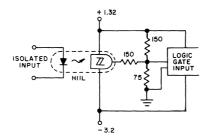


Fig. 57 - H11L input for ECL logic.

# Quality and Reliability of Optoelectronic Components

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Reliability Prediction in Application		
Reliability Enhancement of Optoisolators		

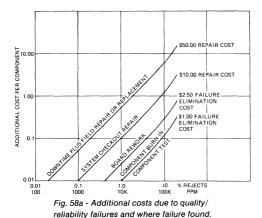
# QUALITY AND RELIABILITY OF OPTOELECTRONIC COMPONENTS

#### **QUALITY AND RELIABILITY COSTS**

The circuit designer must be aware of the expected reliability of the many different components used. This allows control of life cycle costs, such as warranty costs, repair costs and downtime costs, through proper application of these components. Also, component quality can significantly affect a project's economic viability. Quality costs are those associated with the percentage of components received that fail to meet some portion of their specified performance levels. Reliability costs are those associated with the percentage of components that change so that a circuit malfunction occurs.

Some reliability failures can result from inadequate circuit design allowances for parameter changes with temperature, bias, etc. In this discussion, these failures are considered unreliable design malfunctions and will not impact the component reliability considered here.

The costs associated with mediocre quality and/or reliability may prove very significant. A convenient method of visualizing these costs is to calculate the added cost-above purchase price — that is required to have a working component in the field. Cost impact comes from the combination of repair



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Fig. 58b - Subsystem complexity and rework rate.

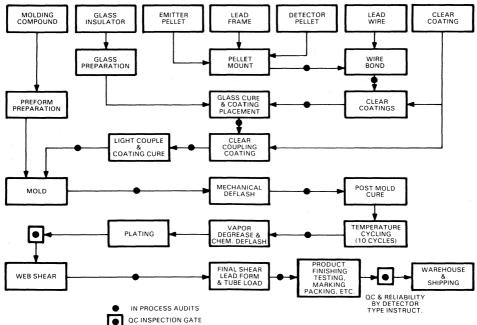
cost, downtime cost, and failure rate and will rise to a major factor if any are high.

Considerable emphasis is placed on the quality and reliability of Harris optoelectronic devices, from design, manufacturing, specification, testing, and the support literature provided to users. Both outgoing quality level (the AQL or LTPD shipped to) and, more importantly, process defect average are closely monitored, recorded, and used as tools to improve future performance. As an example of the effectiveness of this procedure, in 1981 phototransistor optoisolators were normally shipped to a 0.4% AQL. During that year, the observed electrical parameter defect level was approximately 0.1 percent, 4 times better than required to consistently pass.

A more appropriate indicator of quality is reflected in the 1983 quarterly reliability summaries. These reports summarize, by product line, each month's outgoing process average — the estimated average defect level in the outgoing product based on the appropriate MIL-STD quality control sample plan data generated in normal quality control monitoring of outgoing product. For the year of 1983 the monthly OPA for optoelectronic product electrical parameters ranged from a low of 1.7 parts per million (in March) to a high of 49 parts per million (in December). This impressive record includes all manufacturing sites and all optoelectronic devices, although it is dominated by optoisolators in sheer numbers. This record is the result of a recognition that quality and reliability are prime considerations in the selection of optoelectronics devices, due to the critical functions of sensing and isolation performed by them, and a commitment by all at Harris Semiconductor involved in optoelectronics to provide the best devices possible — without sacrificing competitive prices.

To meet the goals of higher quality, higher reliability in a competitive market requires an aggressive product improvement program. The most noticeable result of this program recently has been the introduction of the reflector construction technique in optoisolators. This construction technique provides higher performance, in coupling efficiency and isolation, follows more reliable design criteria (25% fewer wire bonds, lower IRED thermal resistance for cooler operation, longer internal creep path for isolation) and is more consistent, due to the unique mechanical design and the high degree of automation this design allows, providing the basis for even higher quality. Although this world leading design has not yet built up the historical data base associated with the present champion, the sandwich construction present, testing to date indicates equivalence today, with the promise that the knowledge and data gained will assure new records in the future. Table 5 illustrates the assembly process flow of the reflector design DIP coupler. Note the eutectic die bonds on both die, the flexible IRED antireflection coating, the glass dielectric, the 100% temperature cycle of ten cycles, and that the testing includes high temperature wire bond continuity on all devices in addition to parametric tests.

TABLE 5: DIP OPTOISOLATOR FLOW DIAGRAM—REFLECTOR CONSTRUCTION



Optoelectronic components reliability is also monitored. A manufacturer assesses the performance of his components by performing accelerated test sequences on periodic samples of the manufacturing line output. Most of these tests are run at, or beyond, maximum ratings to allow an accelerated reliability assessment of the product. These tests can provide the information required by the circuit designer, but the severity of the test conditions compared to use conditions must be considered. The extrapolated results of these severe tests to normal use levels is still a challenge for the circuit designer, but the challenge is lessened by the availibility of information that provides estimates of acceleration factors, i.e., the increase in rate-of-failure, caused by increasing stress levels, such as voltage, current and temperature. Application of these acceleration factors to the data can allow worse case circuit design techniques to be applied over the design life of electronic equipment. Several sources document estimates of these acceleration factors. One of the most widely used is MIL-HDBK-217 D although recent bibliographies and surveys indicate a vast quantity of relevant data on plastic encapsulated semiconductor devices exists. Such information sources should be consulted when estimates of equipment reliability are attempted from these, or any other, summaries of reliability test data.

## SUMMARY OF TEST RESULTS

Tables 6 through 9 summarize the periodic reports issued by Harris — SPD Quality Control on the optoelectronic products. As new products, processes and test procedures evolve, the application of past data to reliability prediction changes. Thus, data presented here represents a "snapshot in time" of data believed applicable to the product made now and in the immediately anticipated future. A separate section will cover the decrease in light output of the IRED with time of operation, a phenomenon noted in all light emitting diodes, both from the viewpoint of summarizing the observed data and of predicting the response of the majority of devices to expected stress.

Each stress condition monitors a different capability of the component. For the emitters and detectors, the operating life test stresses current, voltage and power activated mechanisms. The only tests which have been found to activate the output decrease of the IRED are tests in which current flows through the IRED. Storage life at elevated temperature tests stability and resistance to thermally activated mechanisms, such as corrosion caused by contamination. Humidity life tests the capability of the package to keep contaminants out, as well as the ability of the package to resist moisture acitvated corrosion, deterioration and surface leakage problems. Temperature cycle causes mechanical stress on components made of materials with different coefficients of expansion, and can break or thermally fatigue parts which are thermally mismatched. This is presently a problem with optoelectronic components packaged in clear epoxies when subjected to wide, repeated temperature changes, due to the large coefficient of expansion of the clear, unfilled epoxy. Since the object of the test program is to gain the most information in the shortest time, and since thermal fatigue has a very strong temperature acceleration, these tests are run to the limits defined by activation of non-valid failure mechanisms or beyond common test equipment capability, without regard for maximum ratings. All high efficiency IRED's have an anti-reflective coating that, unless carefully selected and controlled, can have a detrimental effect on extended temperature cycle performance. Illustrated here are temperature cycle results of the standard 100 cycle test and extended stress results to 200 and 500 cycles, without evidence of thermal fatigue. This is a tribute to the mechanical design of the Harris hermetic IRED. Mechanical sequence stress was not performed on the hemetic IRED, since it contains only two, redundant lead bonds and should exhibit one quarter the failure rate of transistors requiring two independent lead bonds.

TABLE 6: RELIABILITY TEST SUMMARY — EMITTERS AND DETECTORS

DEVICE TYPE	STRESS CONDITION	QUANTITY TESTED	TOTAL DEVICE HOURS	BEST ESTIMATE FAILURE RATE*	
Hermetic IRED • LED55 Series	Operating Life I <sub>F</sub> = 100mA @ 25°C	267	267,000	0.26%/10 <sup>3</sup> hrs. 0.26%/10 <sup>3</sup> hrs.+	
• LED56 Series • 1N6264 - 1N6266	Pulsed Life @ $38^{\circ}$ C $I_F = 1A$ for $80\mu$ sec @ $60$ Hz	200	600,000	0.12%/10 <sup>3</sup> hrs. 0.12%/10 <sup>3</sup> hrs. +	
	Storage Life* T = 200°C	80	80,000	2.2%/10 <sup>3</sup> hrs.	
	Temperature Cycle* -65°C to +200°C	414	86,100∿	0.42%/100~	
Hermetic Detectors  • L14F Series	Operating Life Pd = 300mW	75	75,000	0.95%/10 <sup>3</sup> hrs.	
• L14G Series	Storage Life T = 200°C	75	75,000	0.95%/10 <sup>3</sup> hrs.	
	Temperature Cycle -65°C to +200°C	75	7,500~	0.95%/100~	
	Mechanical Sequence 1.5 KG Drop Shock 20 KG Centrifuge 20 G Vibration	75	N.A.	No Failures	

<sup>★</sup> Catastrophic failure rate to best estimate 50% upper confidence level.

TABLE 7: RELIABILITY TEST SUMMARY — H23 PAIR FAMILY

(ALL HOUSINGS COMBINED - ALL DETECTORS COMBINED)

STRESS CONDITION	PAIRS TESTED	TOTAL PAIR DEVICE HOURS	BEST ESTIMATE FAILURE RATE†
Operating Life @ $25^{\circ}$ C $I_F = 60\text{mA}$ , $I_C = 20\text{mA}$ *	625	496,000	0.14%/10³ hrs.
100°C Storage	450	329,300	0.51%/10³ hrs.
Humidity Stress @ 85°C, 85% R.H.*	450	329,300	0.51%/10³ hrs.
Temperature Cycle - 65°C to +100°C	831	223,100~	0.021%/10~

<sup>†</sup>Catastrophic failure rate to best estimate 50% upper confidence limit.

<sup>+</sup> Combined catastrophic and degradation, to  $\triangle P_{OUT} \ge 50\%$ , est. failure rate to 50% UCL. \*Stress conditions exceed device specified maximum ratings.

<sup>\*</sup>Stress conditions exceed pairs specified maximum ratings in some or all housings.

The basic H23 matched pairs of emitters and detectors are also used in the H21 and H22 interrupter modules, the H24 optoisolator and as discrete devices. A significant effort was expended in the design of these devices to ensure their reliability. The most evident to the eye are the recessed lens, which is thereby protected from mechanical damage during automatic handling, and the serpentine path the mountdown lead follows within the package, to provide a moisture proof path seal in the transfer-molded epoxy. Additional features include the long-lived GaAs IRED with its protection and contact system, the extra large diameter bond wires to withstand extended temperature cycle and the conservative maximum ratings. Additionally, all units are submitted to temperature cycle and high temperature continuity testing prior to electrical parameter screening. No significant difference in reliability has been observed between the various housing alternatives, therefore the test data on all types has been lumped together by pairs, which conserves space and provides a larger, more statistically significant sample. The operating and humidity stresses are beyond specified maximum ratings, and 500 temperature cycles were tested on a portion of the samples. The observed change in IRED output with operation is the same low rate documented on all Harris Semiconductor GaAs IRED's in the next section.

The six pin DIP optoisolator differs from familiar solid state components in that it contains two chips and a light transmission medium, providing a higher potential for failure than simpler components. Due to these construction differences, it would be expected to have different dominant failure modes than either discrete or integrated circuit semiconductors. Each output device type also has some unique characteristics that require unique stress testing. Since the IRED is identical in each type of coupler, most IRED evaluation work is done on the transistor coupler due to the minimal variation of CTR with temperature and bias which provides an accurate monitor of IRED performance. Darlington test monitoring is done at extremely low IRED currents and, therefore, shows the highest rate of decrease when stressed at identical levels. (See next section for details.) The SCR output coupler is subject to the possibility of inversion layer formation (channelling) as are all high blocking voltage semiconductors. Stressing at high blocking voltage at high temperature (HTRB) will accelerate possible inversion layer formation. Test results of all detectors are combined for high temperature storage life, temperature cycle, humidity and salt atmosphere stress, all of which are relatively free of effects dependent on the output device. The results of these tests illustrate the superiority of the GE patented glass dielectric isolation, silicon doped liquid phase epitaxially grown IRED chip and total electrical and mechanical design. This is a premium optoisolator from a reliability and a performance standpoint. From a manufacturing standpoint, it enjoys high yields and ease of assembly, providing this quality at competitive costs.

In the evaluation reliability tables with the acceleration factors given in the next section, both the IRED heating from power dissipated in the output device and the standard readout bias must be known. This heating can require from  $5.5 \text{mW/}^{\circ}\text{C}$  for the H11A to  $11.5 \text{mW/}^{\circ}\text{C}$  for the H11AV construction. Standard CTR readout conditions for phototransistors are  $I_F = 10 \text{mA}$ , and for photodarlingtons at  $I_F = 1 \text{mA}$ .

For convenience, the reliability test summaries are separated into operating and non-operating stresses. All DIP package and detector types are combined in non-operating test results since no significant difference has been observed between types. Operating tests are separated by detector type into significant subgroups. Due to the combined effects of sample size and experience on best estimate failure rate, it is expected that the newer detector type failure rates are not representative. These failure rates are anticipated to decrease, as production increases, to approximate the level of the more mature types. The data base on combined phototransistor and photodarlington detectors is large enough to allow valid failure age analysis. This analysis indicates the failure rate decreases significantly with time on test, which signifies both long life capability and the possibility of reliability enhancement screening. A further analysis of lumped test data by date for failure age reinforces the decreasing failure rate and proves the consistent long-term reliability of the Harris Semiconductor DIP optoisolator.

## TABLE 8: RELIABILITY TEST SUMMARY — HARRIS DIP OPTOISOLATOR

#### (OPERATING STRESS TESTS)

DETECTOR TYPE	STRESS CONDITION	QUANTITY TESTED	TOTAL DEVICE HOURS	BEST ESTIMATE FAILURE RATE
Combined Phototransistor and Photodarlington	Operating Life, $T_A = 25$ °C $I_F = 60$ mA, $I_E = 20$ mA, $V_{CE} = 15$ V*	2499	1.8×10 <sup>6</sup>	0.64%/10³ hrs.
Phototransistor	Humidity Blocking Life, $T_A = 85$ °C RH = $85$ %, $V_{CB} = 24$ V, $V_{EB} = 4$ V, $V_{ISO} = 100$ V	120	6.0×10 <sup>4</sup>	1.2%/10³ hrs.
PhotoSCR	DC Blocking Life, $V_{AK} = 400V, I_F = 0, T_A = 100$ °C	579	3.1×10 <sup>5</sup>	0.55%/10³ hrs.
Triac Driver	AC Blocking Life, $V_{46} = 141V \text{ RMS}, I_F = 0, T_A = 100^{\circ}\text{C}$	180	1.2×10 <sup>5</sup>	2.2%/10³ hrs.
Photo Schmitt Trigger	DC Blocking Life, $V_{65} = V_{45} = 20V, I_F = 0, T_A = 100$ °C	25	2.5×10 <sup>4</sup>	2.8%/10³ hrs.

<sup>★ 50%</sup> upper confidence level best estimate failure rate.

TABLE 9: RELIABILITY TEST SUMMARY — HARRIS DIP OPTOISOLATOR

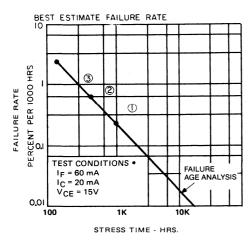
(NON-OPERATING STRESS TESTS - ALL TYPES COMBINED)

STRESS CONDITIONS	QUANTITY TESTED	TOTAL DEVICE HOURS	BEST ESTIMATE* FAILURE RATE			
150°C Storage	2956	$1.5 \times 10^{6}$	0.37 %/10 <sup>3</sup> hrs.			
Humidity Storage, $T_A = 85^{\circ}C$ , R.H. = $85\%$	3283	1.6 × 10 <sup>6</sup>	0.29%/10³ hrs.			
Temperature Cycle -65°C to +150°C	5884	5.9 × 10 <sup>5</sup> ~	0.035%/10~			
Salt Atmosphere MIL-5-750/1041, 35°C	25	600	0.13%/hr.			

<sup>\*50%</sup> upper confidence level best estimate failure rate.

Both storage tests showed no significant change in failure rate over the years. Temperature cycle exhibits a significant improvement: pre-1976 -0.15%; 1978-79 -0.04%; 1980 -0.012% per 10 cycles. This illustrates the effectiveness of process control steps and the 10-cycle temperature cycle followed by high temperature continuity screening of all Harris Semiconductor DIP couplers done prior to electrical parameter testing. Although the following section deals with IRED change with operation, it should also be noted that CTR shift has been noted on DIP optoisolators through temperature cycle. This shift is attributed to mechanical stress caused by unequal coefficients of expansion of the various parts of the optoisolator. Considerable difference is noted from manufacturer to manufacturer, and the Harris Semiconductor design proves stable, indicating the excellence of design. No statistically significant difference in reliability characteristics has been observed between the Harris sandwich, reflector and bar construction optoisolators. It is assumed that a much larger data base is needed to show any difference.

<sup>\*</sup>Accelerated test, test bias conditions in excess of device ratings.



## PERIODIC COMPARISON IN TIME POINTS

- 1. 346 units, pre 1976, 5.6 x 10<sup>s</sup> unit hrs.
- 2. 1203 units, 1978-79, 8.5 x 10<sup>s</sup> unit hrs.
- 3. 950 units, 1980, 3.9 x 105 unit hrs.

Fig. 59 - Operating life failure rate decrease with test time.

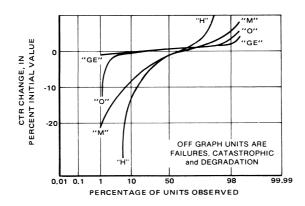


Fig. 60 - 6 pin DIP optoisolator reliability temperature cycle (-55° C to +150° C, 10 cycles) effect on CTR 90 to 100 units each type, 1980 date codes.

## RELIABILITY PREDICTION OF CIRCUITS CONTAINING IRED'S

The IRED phenomenon of light output decrease as a function of the time current flows through it, has been mentioned previously. This phenomenon is observed in all diode light and infrared emitters. The liquid epitaxial processed, silicon doped IRED provides superior performance in this regard. Still, this presents a dilemma to the circuit designer. Adequate margins for bias values require predicting a minimum value of light output from the IRED at the end of the design life of the equipment. Based on the results of tests performed at Harris and at customer facilities (who were kind enough to furnish test data and summaries) the Harris Application Engineering Center has developed design guidelines to allow the prediction of the approximate worst case, end of life, IRED performance.

<sup>\*</sup>Test conditions exceed maximum ratings

TABLE 10: SUMMARY OF TESTS USED TO OBTAIN IRED DESIGN GUIDELINES

T <sub>A</sub>	25°C	40°C	55°C	70°C	80°C	100°C
3mA	20 1000 Hr. 3mA					
5mA	20 1000 Hr. 1, 5mA					
10mA	16 1000 Hr. 1, 10mA		30 1000 Hr. 1, 10mA		30 1000 Hr. 1, 10mA	30 1000 Hr. 1, 10mA
20mA	27 500, 1000 Hr. 1, 5, 10, 20mA	e e e e e e e e e e e e e e e e e e e			108 1000 Hr. 10mA	
25mA	20 1500 Hr. 10mA	20 1500 Hr. 10mA	20 1500 Hr. 10mA	60 1500 Hr. 10mA		
50mA		20 1500 Hr. 10mA		40 1500 Hr. 10mA		
60mA	20 1000 Hr. 1, 5, 10, 20, 60mA		30 1000 Hr. 1, 10mA		313 1000, 3000, 5000 Hr. 1, 10, 60mA	30 1000 Hr. 1, 10, 60mA
75mA				20 1500 Hr. 10mA		
100mA	79 1K, 15K, 30K Hr. 1, 10, 60, 100mA		30 1000 Hr. 1, 10mA		30 1000 Hr. 1, 10, 60, 100mA	120 168, 1000, 1500 Hr. 1, 10, 60, 100ma
1A Pulsed	200 3000 Hr. 1, 10, 100mA					

This chart represents about 2.9 million device hours of operation on 924 dual in-line optocouplers and 311 hermetic IRED's.

**FORMAT OF DATA PRESENTATION:** 

SAMPLE TEST DURATION I<sub>FM</sub> CURRENT The basis of the prediction is the observed behavior of the ratio of light output after operation to the initial value of light output. It is also based on the observation that all devices do not behave identically in this ratio as a function of time, but that a distribution with identifiable tenth, fiftieth (median) and ninetieth percentile points exists at any time the ratio is calculated. Use of this tenth percentile ratio (90% of the devices are better than this) and the distribution of light output (or CTR for couplers) above the specified minimum value allows the product of specified minimum light output and tenth percentile ratio, predicted at end of life, to be used as a reasonable approximation of minimum end of life value. Although this does not represent the worst possible case, no correlation can be found between initial light output and rate of decrease in light output, so the percentage of devices expected to be less than the guideline derived number approaches zero. These guidelines as can be noted, are based on large sample sizes. To make the guideline development less obscure, the discussion will trace the steps followed in defining these design guidelines and, in the process, develop the guidelines. Although the majority of data is taken on Harris Semiconductor GaAls IRED's, it is found that the same general model fits the Harris Semiconductor GaAlAs IRED.

Since the original Harris Semiconductor model was published, based on data generated prior to 1976, considerable effort has been expended to define and minimize this decrease. Response of the light output of the IRED to operating time is considered to be comprised of two factors, stabilization and degradation. Further, two types of degradation are apparent, short-term and long-term degradation. Short-term degradation can be virtually eliminated, while long-term degradation can be minimized through process and material control. These factors can be visualized through plots of the ratio of IRED

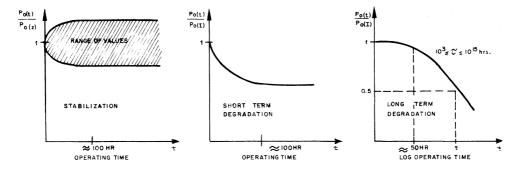


Fig. 61 - Factors affecting IRED operating output power.

output power, as it is operated, to its initial value (i.e., normalized output power vs. operating time). Various items have been identified as affecting these factors — crystal structure, impurities, mechanical and thermal stress. Most of the published information is of such gross definition that it only identifies the worst offenders. Rapid methods of assessing IRED performance have likewise proven disappointing. As a consequence, the tedious life test is the measure of performance improvement.

Analysis of life test results to characterize the change in power output is complicated by the difficulty in separating the magnitude of effect of each factor and the fact that these magnitudes can be functions of both stress conditions and monitoring conditions.

The problems with predicting response are the variety of test conditions at which both stress and measurement data have been taken, and the spread of data at the readout points. It was recognized that the decrease in light output was accelerated by either stressing the IRED harder, i.e., at a higher current  $(I_{FS})$  and/or temperature, or by monitoring the test results at lower current  $(I_{FM})$  levels. Precise acceleration factors have yet to be determined due to this variability. Fortunately, circuit design purposes can be served by a less precise model, which only attempts to serve the requirements of circuit design. For this approach, as mentioned before, attention is paid to the lower decile of the distribution of  $P_0(t)$  and its change with operating time. The objective is to approximate the mid portion of the longterm degradation plot with a straight line by utilizing data points beyond the short-term factor effects.

Significant progress has been made in improving the Harris Semiconductor IRED degradation since the first model was published. This is illustrated by comparison of the data published at that time with present units tested at the same stress levels. Present units are much more consistent than early

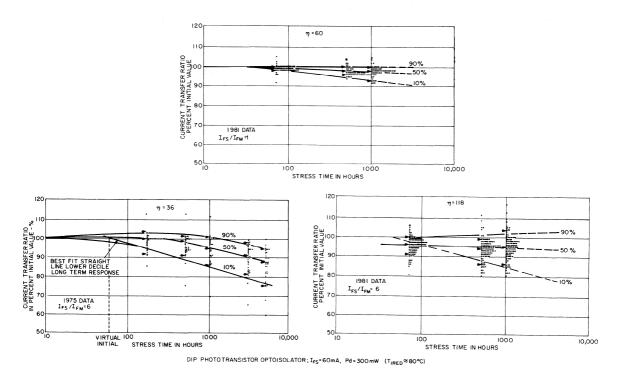


Fig. 62 - Life test results — illustrating observed change in IRED output with operating time.

units. This is evident in the smaller, tighter distribution with larger sample sizes. (See Figure 62.) Data taken at a greater variety of conditions, both more highly accelerated and simulated use conditions, and more precise readouts, indicates the original model was quite conservative for most applications. Recent data indicates the GaAs IRED, to a lower decile definition, degrades less than GaAlAs. The most precise data, with temperature and detector compensation, suggests that lower current operation (i.e. lower  $I_{FS}$ ), at a given stress temperature and  $I_{FS}$ / $I_{FM}$  ratio, has the higher degradation rates within the model. This conclusion is not consistent with all data, but implies that conservative circuit design should allow more margin for degradation at low ( $\leq$ 3mA) IRED bias currents.

The IRED degradation model predicts the slope of long-term lower decile response of the distribution of the ratio of light output after operation to initial value. This response is plotted in a straight line against the logarithm of operating time. Extrapolation of this straight line towards zero time defines a virtual initial time, when it intersects the initial value. Observations indicate the virtual initial occurs at or before 50 hours. For purposes of circuit design, the assumption of 50 hours for virtual initial time will be utilized to assure conservative design. The slope of this lower decile line can be defined in percent drop in light output per decade time. Slope and virtual initial completely define the predicted IRED output with operating time.

This model includes all Harris DIP optoisolators, discrete IRED's, both hermetic and plastic, and all H23-based product families. Note that GaAs and GaAlAs emitters differ in slope.

The question naturally arises of the applicability of this descriptive model to time periods beyond the one and five thousand hour times where the majority of the tests stopped. Fortunately, tests have been completed on discrete IRED's for 30,000 hours. These units were manufactured prior to 1970, and illustrate the improvement in IRED technology over the last decade. The results of these tests indicate that nothing unexpected happens at extremely long times, as can be seen in Figure 63.

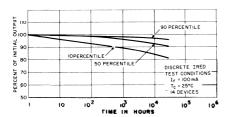


Fig. 63 - Long-term IRED life test results.

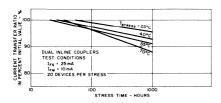


Fig. 64b - Effect of stress temperature on slope.

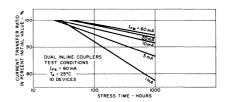


Fig. 64a - Effect of measurement current on slope.



Fig. 64c - Effect of stress current on slope.

When the response (best straight line) of various test conditions is plotted on a single graph, the acceleration due to raising stess current ( $I_{FS}$ ) is easily seen. Higher temperatures during stress cause the same effect, and can be accomplished by raising the ambient or by self-heating (in a optoisolator by dissipating power in the output device). Lowering the current at which the IRED light output is monitored, ( $I_{FM}$ ) also accelerate the phenomena, but analysis of many test results indicates that the ratio of  $I_{FS}/I_{FM}$  is the key factor-determining the slope dependence on bias.

When the temperature effect is plotted as an acceleration vs. temperature, a fair straight line fit is found, as illustrated in Figure 65. This temperature acceleration factor represents the ratios of the slopes of the lower decile lines of various temperature stresses. The fit is not perfect, but is good enough to be useful. The model contains data on all current IRED package options and appears to fit all equally.

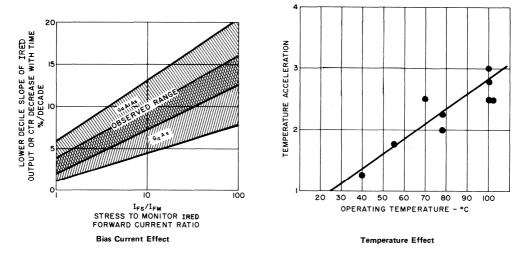


Fig. 65 - IRED output vs. time-slope prediction curves assuming a virtual initial time of 50 hours.

Utilizing the highest observed slope at  $I_{FS} = I_{FM}$ , a conservative equation for output power can be derived for each emitter material. Since most applications provide a relatively constant bias current to the IRED whenever energized, these equations provide the means to determine bias current required at equipment end of life. Note that degradation occurs only when current flows in the IRED. The IRED power output  $(P_0)$  at time tx can be predicted from:

when constant current bias for tx hours,  $25^{\circ}C \le T_A$  (ambient temperature,  ${}^{\circ}C$ )  $\le T_j$  max., and tx  $\ge 168$  hours is assumed.

High current pulse operation degradation has been studied at one point. 200 each TO-18 GaAs IRED's have been operated for 3000 hours with 1A pulses,  $80\mu$ sec wide, 60 pulses per second, at  $38^{\circ}$ C. Analysis of the degradation data indicates that only the time current flows through the IRED causes degradation (180 hours accumulated for these units) and that the degradation follows the model responses. The degradation rate appears to be slightly higher under this pulse condition, indicating a higher stress on the chip than the D.C. bias test. This is logical when the cyclic thermal and mechanical stress on the chip due to pulsing is considered. At this test condition, the GaAs slope was in the center of the GaAlAs area of Figure 65. Based on this data, it is concluded the equation for GaAs pulsed operation is:

$$P_{O(tx)} = P_{O(to)} \left[ 1 - 0.06(0.024 T_A + 0.4) \log \left( \frac{R tx}{50} \right) \right]$$

where R is the duty cycle of operation.

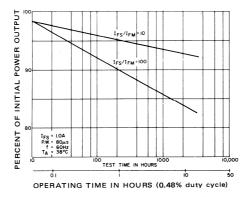


Fig. 66 - GaAs IRED pulsed operation.

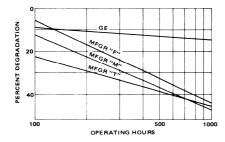
The following example illustrates the use of this model for circuit design. A CNY17-III phototransistor output optoisolator is desired to provide an input to a logic circuit. To provide a logic zero the isolator must sink 2.5mA at 0.3V. The CNY17-III specification assures this capability at  $I_F = 10$ mA initially. Equipment design life is 10 years (8.8 ×  $10^4$  hours) and the worst case duty cycle of operation is 80% "on" time. Ambient temperature in the equipment is maintained below 65°C.

 $\begin{array}{lll} \textit{Summary of example calculations} \\ \textit{Device} & - \textit{CNY17-III} \\ \textit{IRED material} & - \textit{GaAs} \\ \textit{Temperature} & - 65\,^{\circ}\textit{C} \\ \textit{Time} & - 8.8 \times 10^{4} \times 0.8 = 7 \times 10^{4} \, \text{hours} \\ \\ P_{o(tx)}/P_{o(to)} & = 1 - 0.04 \left[0.024 \, (65) \, + 0.4\right] \log \left(\frac{7 \times 10^{4}}{50}\right) \end{array}$ 

Therefore, the IRED bias must be 10/0.75 = 13.3mA, to assure end of life operation. Note that this example has not considered the effects of temperature, tolerances, or other components aging on IRED current requirements.

The design guideline, unfortunately, is only valid for our IRED's and DIP couplers. Life tests of competitive units at both maximum rating and accelerated test conditions indicate a wide variation of performance exists in the industry.

In applications where IRED degradation can result in undesirable malfunctions, it is recommended that vendor evaluation and reliability enhancement screening procedures be performed.



Transistor Photocoupler Data, Observed Lower Decile Data, 1980 Date Codes 20-30 Samples/Type. Test Conditions Stress:  $I_F$  = 60 mA, Pd = 300 mW Measurement:  $I_F$  = 10 mA,  $V_{CE}$  = 10 V CTR

Fig. 67 - IRED degradation, rate, competitive comparison accelerated life test results.

## RELIABILITY PREDICTION IN APPLICATION

Predicting component reliability in applications requires a failure rate prediction model. Although MIL-STD-217D provides this type of model, it is based on industry performance and appears strongly biased towards hermetic packaged, JAN-screened devices. A wide variety of reliability assessment information has been published and can be utilized to make predictions based on test data of specific device types and the actual environment they are to be applied in. This method requires that acceleration factors on each stress be determined, and that the stress in applications and in accelerated tests be defined; then the failure rate in accelerated tests can be proportioned to use condition failure rate. The use condition failure rates, by stress, are summed to provide overall failure rate. Advantages of this method include the fact that it is specifically tailored to the component and application, and that potentially high failure rate details are identified to be dealt with in the most economical fashion. Disadvantages include the assignment of stress acceleration factors, a wide variety of which have been published, and the availability of applicable accelerated stress data.

The preceding data provides an excellent base to assess the reliability of Harris Semiconductor optoelectronics components. If the designer provides adequate margins for tolerances, IRED degradation, and has a viable worst case circuit design, appropriate acceleration factors will allow these data to predict component reliability. The specific stress acceleration factors required are: detector blocking voltage and temperature effects; humidity intrusion effects; and temperature variation (due to power and environment) effects. Note the IRED is not considered separately, because its mechanical defects are covered in temperature cycle stress and any efficiency degradation by IRED degradation guidelines.

The sources of acceleration factors require engineering judgment to identify the most valid for the specific device. For the variety of DIP optoisolators Harris produces, the author prefers the following acceleration factors based on experience and familiarity with available literature:

TABLE 11: STRESS RESPONSE ACCELERATION FACTORS

STRESS	DEVICE	ACCELERATION FACTOR - *A	SOURCE
Blocking	PhotoSCR	$0.65 \left( \frac{V_2 - V_1}{V_m} \right) - 4323 \left( \frac{1}{T_2} - \frac{1}{T_1} \right)$	GE 6th Ed. SCR Manual, Fig 19.3
Blocking/Power	other discrete detection	$-3327\left(\frac{1}{T_2}-\frac{1}{T_1}\right)$	GE Pub. 300.1, Fig. 9
Blocking/Power	IC detectors	to be determined	
Humidity Intrusion	All	$1987 \left(\frac{1}{T_1} - \frac{1}{T_2}\right) - 2.424 \left(h_1^2 - h_2^2\right)$	Microelec. & Reliab., Vol. 20, pg. 219
Temperature Cycle	All	$328\left(\frac{1}{\triangle T_1} - \frac{1}{\triangle T_2}\right)$	independently derived

<sup>\*</sup>The ratio of stress level 1 response to stress level 2 response is F.R. 1/F.R. 2=10A.

CODE: F.R. - failure rate

V - blocking voltage

T - junction temperature in Kelvin

h - percent humidity ÷ 100

△T — range junction temperature changes

1 & 2 subscript — associates stress level

m subscript — maximum rating

It should be noted that this is strictly accurate only for responses that show a constant failure rate in time or to calculate the times that an identical proportion of failures occur for a linear stress response. The Harris DIP optoisolator has a decreasing failure rate as a function of time, which will make these estimates conservative.

An example, using the same CNY17-III used to calculate the effect of IRED degradation, will illustrate the prediction process. The temperature cycle calculation will assume a 25 °C to 65 °C cycle per day for equipment power up, power down. Additionally assume turn-on — turn-off of the optoisolator every 30 seconds, which will cause an emitter junction temperature change of (13.3mA x 1.2V)  $\div$  1.33mW/°C = 12°C plus (2.5mA x 0.3V)  $\div$  5.5mW/°C, i.e., 12.2°C total.

• Temperature Cycle: Daily — 
$$A_D = 328 \left( \frac{1}{65 - 25} - \frac{1}{150 - (-65)} \right)$$
;  $10^A = 4.7 \times 10^6$   
Switching —  $A_S = 328 \left( \frac{1}{12.4} - \frac{1}{150 - (-65)} \right)$ ;  $10^A = 8.4 \times 10^{24}$   
Failure Rates:  $0.000035$ /cycle ÷  $4.7 \times 10^6 \times 365$  day ×  $10$  yr. =  $2.7 \times 10^{-8}$   
 $0.000035$ /cycle ÷  $8.4 \times 10^{24} \times 2 \times 60$  min. ×  $24$  hr. ×  $365 \times 10$   
=  $4.4 \times 10^{-23}$ 

Temperature Cycle Failure Rate =  $2.7 \times 10^{-8}$ 

• Power Life: Accelerated test — 
$$T_2 = 75^{\circ}\text{C}$$
 (DIP at 300mW) + 25 + (60mA × 1.5V)   
÷ 5.5mW/°C<sup>†</sup>= 116°C = 389°K

Application stress —  $T_1 = 0.4^{\circ}\text{C}$  + (13.2mA × 1.2V) ÷ 5.5mW/°C + 65   
= 68.3°C = 341.3°K

$$A = -3327 \left(\frac{1}{389} - \frac{1}{341.3}\right); 10^{A} = 16$$
Failure Rate = 0.0064 ×  $10^{-3}$  × 7 ×  $10^{4}$  hrs ÷  $16 = 2.8 \times 10^{-2}$ 

• Humidity Life (assume ambient humidity 15% at 65°C, 85% at 25°C)

Power down — 
$$A_L = 1987 \left( \frac{1}{298} - \frac{1}{358} \right) - 2.424 (0.85^2 - 0.85^2), 10^A = 13$$
  
Power up —  $A_H = 1987 \left( \frac{1}{338} - \frac{1}{358} \right) - 2.424 (0.15^2 - 0.85^2), 10^A = 106$   
Failure Rate =  $0.0029 \times 10^{-3} (7 \times 10^4 + 106 + 1.8 \times 10^4 + 13) = 5.9 \times 10^{-3}$ .

†coupled thermal impedance, emitter to detector.

The sum of these is the total failure rate of the CNY17-III optoisolator expected over the 10 year equipment life, i.e.  $2.7 \times 10^{-8} + 2.8 \times 10^{-2} + 5.9 \times 10^{-3} = 3.4$  percent. This is an average failure rate of  $385 \times 10^{-9}$  per device hour for  $8.8 \times 10^4$  hours. Note that the most significant items are the Power Life stress followed by the 85% humidity estimate at 25°C (equivalent to a moist tropical environment). The failure rate can be improved by submitting the standard CNY17-III to reliability enhancement screening procedures, of course.

## RELIABILITY ENHANCEMENT OF OPTOISOLATORS

The optoisolator is unique in its application, construction, and the factors that affect its reliability. The major applications typically use the optoisolator to carry information between electronic logic and some form of power system. These are typically in relatively high cost systems where downtime is costly and sometimes critical. This places a premium on the reliability of the optoisolator, which is a reasonably-priced component subject to normal marketplace competitive pressures. These pressures are significant since over 10 manufacturers supply the common six-pin plastic dual in-line package optoisolator.

Each manufacturer utilizes unique semiconductor pellets for the light-electrical conversions. Each has unique methods and materials used to mount, connect, provide light path, and isolate ambient effects. Therefore, a wide variation of both reliability performance and consistency might be expected throughout the industry. Published studies confirm this and illustrate the variety of failure modes unique to the optoisolator, when compared to both discrete and integrated circuit semiconductors. 31,33,34

The uniqueness of the optoisolator does not mean that accelerated semiconductor reliability assessment test procedures are inappropriate to identify failure modes or screen out potentially unreliable devices. It means that these test procedures must be evaluated to identify failure modes and cost effective ways to remove potential application failures. Where high sensitivity to failure and/or high stress levels are present extra screening for reliability enhancement may be desirable. The available information indicates several levels of increasingly effective screens are possible.

Most optoisolator manufacturers can identify a cost effective reliability enhancement screen for their product. However, there may be conflicts between this action and other goals or priorities of the manufacturer. An optoisolator user can do the same for a given device, but is vulnerable to manufacturing process differences, both identified and unknown. The best compromise is a test sequence based on a broad sample of optoisolator data covering a number of manufacturers. This was impractical until recently.

In 1981 several large sample phototransistor optoisolator reliability studies were published in various parts of the world. These data have been analyzed to identify optoisolator failure modes and effective screening procedures. These procedures have been modified, as required, for the various detectors used in optoisolators (i.e., photodarlington, photoSCR, etc.). Such modifications are based on experience with the specific type of discrete semiconductor device. In these tests, the high stress levels are expected to accelerate failure response, when compared to application conditions. It is noted that the failure rates, per unit time, decrease as stress time increases (with the exception of storage life, which appears to show a wearout mechanism on specific designs). It is also apparent that different specific designs have different weak points. This reliability enhancement screening procedure will be designed to cost effectively address all these weak points. Table 12 shows the reliability test data for eleven manufacturers of optoisolators.

**TABLE 12: RELIABILITY TEST DATA COMPILATION** 

(DIP PHOTOTRANSISTOR OPTOCOUPLERS)

	t					MAN	JFACT	URER				
Stress Conditions*	R.O. Hrs.	1	2	3	4	5	6	7	8	9	10	11
IRED Fwd. Bias	168		<u>0(0)</u> <u>80</u>	70	$\frac{10(1)}{20}$		70	60	60	70		0(0)
4	1000		<del>0(1)</del> <del>80</del>	11(3) 70	$\frac{10(4)}{20}$		$\frac{0(10)}{70}$	60	1(0) 60	70		0(0)
High Temperature	168		$\frac{0(0)}{10}$	<del>0(0)</del> <del>10</del>			$\frac{0(1)}{10}$	<del>0(0)</del> <del>10</del>		<u>0(0)</u> 10		
Reverse Detector Bias	1000		<u>0(1)</u> 10	<u>0(0)</u> 10			1(1)	<u>0(0)</u> 10		2(0) 10		
Operating Stress	168	<u>0(0)</u> 27	<u>0(0)</u> 105	1(0)	<u>0(1)</u> 20	<u>1(0)</u> <u>29</u>	$\frac{0(1)}{35}$	<u>0(0)</u> 25	<u>0(0)</u> <u>25</u>	<u>0(0)</u> <u>35</u>	1(3) 28	<u>0(0)</u> 10
	1000	1(4) 27	1(1) 105	3(0) 65	$\frac{0(10)}{20}$	<u>1(4)</u> <u>29</u>	$\frac{1(1)}{35}$	<del>0(0)</del> <del>25</del>	<u>0(0)</u> 25	<del>0(0)</del> <del>35</del>	<b>2</b> (4) <b>28</b>	<u>0(0)</u> 10
Storage Life	168		<u>0(0)</u> 25	<u>0(0)</u> 25			<u>0(0)</u> 25	<u>0(0)</u> 25	<u>0(0)</u> 25	<u>0(0)</u> <u>25</u>		
	1000		<u>0(0)</u> <u>25</u>	1(0) 25			<u>0(0)</u> 25	13(1) 25	<u>0(0)</u> <u>25</u>	<u>5(0)</u> <u>25</u>		
Temperature Cycle		200	<del>5</del> <del>700</del>	500		19	<u>3</u> 590	<del>3</del> 500	<u>0</u> 500	500	36 100	
Humidity Life	168		<u>0(0)</u> <u>45</u>	35	<u>0(0)</u> 20		<u>0(0)</u> <u>35</u>	<u>0(0)</u> <u>25</u>	<u>0(0)</u> 25	35		<u>0(0)</u> 10
,	1000		<del>0(0)</del> <del>45</del>	35	3(0)		<del>0(0)</del> <del>35</del>	<u>0(0)</u> <u>25</u>	0(0) 25	35		$\frac{0(1)}{10}$

Total units tested: 2594 1.269 x 10<sup>6</sup> device hours of stress

Manufacturers Tested: Fairchild, Harris Semiconductor, General Instrument, Honeywell, Litronix, Motorola, RTC, Sharp, Siemens, Texas Instruments, TRW

The data shows 129 catastrophic failures and 42 parametric degradation failures on 2594 units. The catastrophic failures, opens and shorts, are mechanical integrity faults. These faults are normally screened out by temperature cycle testing. A comparison of temperature cycle failure-rate to catastrophic failure rates, by manufacturers, generally confirms the expected effectiveness. It is also noted that two manufacturers exhibited failure rates over 10% on this test. Screening procedures for degradation failure modes can be defined by identification of the failure modes. Table 13 compares degradation failure modes for five stress types.

<sup>\*</sup>See Section 3.6 for data summary containing specific conditions, and sample sizes.

 $<sup>\</sup>begin{array}{ccc} \text{Summation of Catastrophic Failures} & \underline{1(1)} & -\text{Summation of Degradation Limit Failures} \\ & \underline{25} & -\text{Summation of Samples Tested} \end{array}$ 

TABLE 13: SUMMARY OF 11 MANUFACTURERS' RELIABILITY PERFORMANCE FOR DEGRADATION FAILURE MODES

	Failure Criter	ia		# of Mfrs.	# of Mfrs.
Test	Degradation	Catas- trophic	Duration	Failing Degradation	Failing Catastrophically
IRED Fwd. Bias	10% of units fail CTR degradation limit	10% of units fail	168 Hrs 1000 Hrs	0 2	0
High Temp. Reverse Detector Bias	10% of units fail leakage or CTR limits	10% of units fail	168 Hrs 1000 Hrs	1 3	0 2
Operating Life	10% of units fail leakage or CTR limits	10% of units fail	168 Hrs 1000 Hrs	2 4	0
Storage Life	10% of units fail leakage or CTR limits	10% of units fail	168 Hrs 1000 Hrs	0 0	0 2
Humidity	10% of units fail leakage or CTR limits	10% of units fail	168 Hrs 1000 Hrs	0 1	0 0

- All tests were at or beyond maximum ratings.
- See Section 3.6 for data summary.
- From date code analyses all units were manufactured between early 1979 & early 1981.

Based on these data, storage and humidity tests show no promise as screening tools. Three types of defects appear common in the summary:

Mechanical — This is related to package material compatibility & construction.

Detector Pellet — Related to instability in h<sub>FF</sub> or leakage current.

IRED Pellet: — Related to light output degradation.

Analysis of failures, when available, tends to confirm the implications of the data. Defects noted as causes of failure were (in no particular order):

- Mechanical, open
  - broken bond wire at dielectric interface
  - bond wire lifted off pellet bond pad
  - epoxy pellet mount lifted off lead frame
  - pellet bond pad lifted off pellet
  - bond wire break at wedge bond heel

- Mechanical, short
  - bond wire droop to lead frame
  - bond wire droop to pellet edge
- IRED pellet degradation
  - light output degradation on forward bias
  - leakage increase due to pellet flaw
- Detector pellet degradation
  - h<sub>FE</sub>, instability
  - leakage increase due to visible pellet flaw
  - leakage increase
  - breakdown voltage drop due to leakage increase

Note that the apparent wearout in  $150^{\circ}$ C storage was due to both epoxy pellet mount and bond wire failures. Gross lumped failure rates observed are 6.8%, which, when the cause could be identified, break down to:

- Mechanical 5.0%
- Emitter Degradation 0.7%
- Detector Degradation 0.1%
- Emitter and/or Detector Degradation 1.0%
- Specific tests showed degradation failure rates up to 5.9%, while one manufacturer exhibited failure rates up to 70% on IRED bias testing.

THIS IMPLIES THAT A RELIABILITY ENHANCEMENT PROGRAM MUST ASSESS ALL PARTS OF THE OPTOCOUPLER DEVICE TO BE EFFECTIVE. There is no one-to-one correlation between reliability test failure rates and field failure rates in any given application. The tests illustrate weak areas that can cause field failures. A reliability enhancement program must attack these weak areas to significantly reduce field failures.

Cost of screening also enters into the design of cost effective reliability enhancement programs. A list of possible reliability enhancement tests, in order of increasing cost, illustrates this:

100% Screening Procedure	Estimated Relative Cost
Tightened Parameter Limits	1 x
High Temperature Storage	3x
Temperature Cycle & Continuity	4x
High Temperature Blocking	10x
Forward Bias Conduction	12x
Operating Life, All Junctions Biased	16x

Combining cost, failure mode, and time to failure information from the test summaries indicates:

- Many of the mechanical failures can be removed using extended temperature cycling. Detailed
  analysis of the individual data sets indicates a decreasing failure rate to 100 cycles, -55C to
  + 150C, for all but two manufacturers, with several increasing in failure rate beyond 200 cycles.
  Analysis also indicates the need for high temperature continuity testing of all wire bonds, at low
  voltage and current, following the temperature cycle;
- Pellet operating stress tests are required to identify IRED light output degradation, and detector
   h<sub>FE</sub> (gain) or leakage instability. Analysis of failure rate data, by manufacturer, indicates neither
   high temperature blocking stress nor conducting stress can in themselves ensure a significantly
   reduced failure rate in all applications.

The operating stress is most effective, and less costly than doing separate tests, in sequence, for each failure mode. In addition, study of IRED degradation indicates a minimum test time of 160 hours is required to quantify this phenomenon. Increased IRED response is noted at higher forward stress current, within device ratings. Increased response is noted on the detector at higher power levels, (which raises temperature) and higher voltages. Since the detector response is generally more rapid than the IRED, and dissipation should be at a maximum levels, the stress voltage is less critical and can be selected to provide best control of operating conditions. The limits on detector bias voltage are normally 0.25 to 0.9 times maximum rated voltage.

In some cases, the connections available to the optoisolator do not allow all biases to be optimized simultaneously. In such cases, power dissipation is controlled by utilizing a detector voltage supply and load resistor selected to dissipate maximum rated power when the detector bias current drops half of the supply voltage across the resistor. Feedback via the IRED can usually keep power dissipation within 10% of the desired value. In simpler cases, detector bias current and voltage are easily set by standard techniques. These cases are illustrated for simple detectors by the circuits shown in Figure 68.

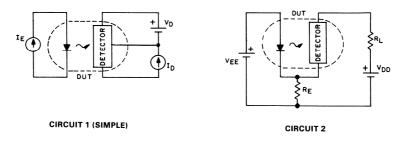


Fig. 68 - Burn-in circuit configurations.

The recommended reliability enhancement program uses temperature cycles and operating stess to identify potential field failures. The optimal stress levels deduced from this data, and six-pin DIP ratings, are:

Temperature cycle: -55 to +150°C, 10 cycles; 12 minute dwell at extremes, 3 minute dwell at 25°C, followed by 100°C continuity check.

Operating stress:  $P_d = 300 \text{mW}$ ,  $I_F = 60 \text{mA}$  if possible, t = 160 Hrs.

For our optoisolator, the recommended biases and operating stress are:

11-4				CIRCUIT 2						
Isolator Family	С	IRCUIT	1	V <sub>EE</sub>	$R_{E}$	$V_{DD}$	$R_L$	DET	ECTOR	BIAS
ramily	I <sub>E</sub>	$V_D$	I <sub>D</sub>	v	Ω	v	Ω	PIN 4	PIN 5	PIN 6
H11A,B,G	60mA	20V	15mA					Minus	Plus	Ref.
H11D	60mA	150V	2mA					Minus	Plus	Ref.
H11C				5V	51	200	100K	Open	Plus	Minus
H11F				5V	56	30	750	Minus	Plus	Minus
H11J	-			10 <b>V</b>	1.1K	250	43K	Minus	Plus	Minus
H11L				5V	56	12	0	Open	Minus	Plus

It is anticipated that this screening sequence will be  $\geq 90\%$  effective in removing potential failures in commercial/industrial applications over a large population of optoisolators.

At lower unit cost, for comparison, temperature cycle alone would be expected to be 40% to 60% effective. A temperature cycle followed by a 16Hr., 125°C detector HTRB would be expected to be 50% to 65% effective for the same conditions.

## Data Summary

The specific test data and sample sizes which form the basis for this reliability enhancement information are as follows:

	Sample			
Test	Mfrs.	Units	Stress Conditions	Duration
IRED Forward Bias	6	240	$T_A = 25^{\circ}C, I_{FS} = 100 \text{mA}$	2000 Hrs
	6	120	$T_A = 70^{\circ}C, I_{FS} = 50mA$	2000 Hrs
	6	60	$T_A = 70$ °C, $I_{FS} = Maximum Rating$	1000 Hrs
High Temperature Reverse Bias on Detector	6	60	$T_A = 150$ °C, $V_{CB} = 24$ V, $V_{EB} = 4$ V	1000 Hrs
Operating Stress	6	150	$T_A = 25$ °C, $V_{CB} = 20$ V, $I_E = 15$ mA, $I_F = 60$ mA	1000 Hrs
	6	60	$I_A = 25$ °C, $I_C = 2.5$ mA (10% Duty Cycle), $I_F = Maximum Rated$	1000 Hrs
	5	180	$I_A = 25$ °C, $V_{CB} = 20$ V, $I_E = 15$ mA, $I_F = 60$ mA	1000 Hrs
Storage Life	6	150	$T_A = 150$ °C	1500 Hrs
Temperature Cycle	6	2700	25°C to 125°C, continuous continuity monitor 10 min. ramp up & down, 20 min., 125°C dwell	5 cycles
	6	300	-55°C to 25°C to 125°C to 25°C, 12 min. dwell at extremes, 3 min. 25°C dwell	400 Cycles
	6	700	-65°C to 25°C to 150°C, 12min. dwell at extremes, 3 min. dwell at 25°C	100 Cycles
Humidity Life	6	60	$T_A = 40^{\circ}C, R.H. = 93\%, V_{ISO} = 500V$	1000 Hrs
	6	150	$T_A = 85^{\circ}C, R.H. = 85\%, No Bias$	1500 Hrs

# **Measurement of Optoelectronic Device Parameters**

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# MEASUREMENT OF OPTOELECTRONIC DEVICE PARAMETERS

## **IRED PARAMETERS**

Measurement of IRED parameters is relatively straight forward, since the electrical parameters are those of a diode. They can be measured on test equipment used to measure diode parameters, from the bench set-up of two meters and a power supply to the most automated semiconductor tester.

Light output measurements require the use of a spectrally calibrated photo cell or a calibrated thermo pile of at least 0.4" (1cm) in diameter. This allows collection of all the light power output of the IRED, matching the specification method and guaranteeing correlations of measurements. If pulse measurements are desired, a calibrated silicon photo cell is necessary because of its response time. It would be used in conjunction with a pulsed current source, and calibrated current probe to measure photocell output and an oscilloscope of sufficient speed and accuracy to provide the desired result. The photocell is the only device which is not a common electronics laboratory item, and such devices can be procured from sources such as Ealing Corp., E.G. & G. Electro Optics Div., United Detector Technology, and others.

The photocell should be calibrated at the wavelength of interest, traceable to the Bureau of Standards. Slightly different mechanical couplings to the photocell are used for each package type. The H23 emitter is placed, touching the cell cover glass, with the lens over the cell center. The hermetic emitters are placed in an aluminum collar, as illustrated. This arrangement will correlate within 10% with total power output readings taken using a calibrated integrating sphere.

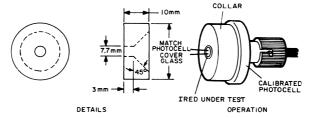


Fig. 69 - Aluminum collar measurements test fixture.

Radiant intensity  $(I_e)$  can be read with the same photocell in a different mechanical arrangement. In this case, the photocell is centered behind a thin, flat black aperture plate. It is placed in the housing that holds the IRED centered on the photocell and aperture centerline and spaced such that the IRED reference plane is over 4cm from the aperture. The aperture and photocell are sized and placed such that all irradience that passes through the aperture falls on the photocell active area. IRED distance and aperture size determine the solid angle of measurement. The housing that holds the IRED, aperture and photocell must be designed to eliminate reflective path photocell illumination.

Note that the power output drops with chip temperature and at power dissipation over a few mV the self-heating of the IRED chip will lower the power output. Normally, a  $300\mu$ s test pulse is used for IRED power output measurements.

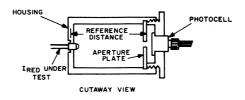


Fig. 70 - Radiant intensity test fixture.

## PHOTODETECTOR PARAMETERS

The measurement of electrical parameters of the photodetectors is identical to measurement of non-light sensitive devices, except for the light sensitive parameters. Such measurements are described in many common references and will not be detailed here. The most common problem parameter encountered is the leakage current measurement with the base open, as  $I_{CEO}$  is rarely measured on normal transistors. Understanding the sensitivity to dynamic and ambient light effects will aid in solving this problem.3 Dynamic effects must be considered, because the open base has no path but junction leakage to charge the junction capacitance. If the common, high source impedance bias circuit, for leakage current is used, the gain of the transistor multiplies the junction capacitance (Miller effect) of the collector base photodiode (  $\approx 25$ pF), and provides a long stabilization time constant. Note the "double barreled" effect of source impedance in that it is the resistance in the RC time constant and also is the load resistor that determines voltage gain ( $A_v \approx I/hie \cdot R_L \cdot hfe$ ). These effects indicate  $I_{CEO}$  should be measured by application of the bias voltage from a low impedance supply until junction capacitances are charged (now determined by the base emitter diode impedance), which can take up to 100msec, (with no external capacitances, switches, sockets, coaxial, etc. connected to the base) in a darlington. After junction capacitance is charged, the current measuring resistor is introduced to the circuit by removing the short across it. The charge balance at the base can be affected by the motion of conductive objects in the area, so best reproducibility will be obtained with an electrostatic shield. The electrostatic shield can also serve the purpose of shielding the detector from ambient light, the effects of which are obvious in leakage current measurement.

Measurement of the light parameters of a phototransistor requires a light source of known intensity and special characteristics. Lamps with defined spectral characteristics, i.e., calibrated standards, are available and, in conjunction with a thermopile or calibrated photocell and a solid mechanical positioning system, can be the basis of an optomeasuring system. The lamp is placed far enough from the detector to approximate a point source. Some relatively simple systems based on the response of a silicon photocell are available, but the assumption that all silicon devices have identical spectral response is implicit in their use for optical measurements. As different devices will have slightly different response curves, the absolute accuracy of these devices is impared, although excellent comparative measurements can be made. Another method which has fair accuracy is the use of a calibrated detector, L14C or L14N photodiode response for the phototransistors, to adjust the light source to the desired level. This will eliminate spectral problems as the calibrated device has an identical spectral response to the devices being measured. Accuracy will then depend on detector calibration, basic equipment accuracies, ambient control and mechanical position reproducibility.

Spectral response measurements require use of precision filters or a precision monochromator and a calibrated photocell or thermopile. As in the case of the IRED, it is recommended that these measurements be done by a laboratory specializing in optical measurements.

#### **OPTOCOUPLER MEASUREMENTS**

Measuring individual devices in the optocoupler is identical to measuring a discrete diode and a discrete device of the type of detector being considered. The measurement of isolation and transfer characteristics are not as obvious, and will be illustrated.

- 1. Isolation Parameters are always measured with the terminals of each device of the coupler shorted. This prevents the high capacitive charging currents, caused by the high dv/dt's applied during the measurement, from damaging either device. Safety precautions must be observed in these tests due to the very high voltages present.
- a). Isolation voltage is measured as illustrated below. Normally the surge voltage capacity is measured, and, unless the high voltage power supply has a fast shutdown ( $<0.5\mu sec$ ), the device under test will be destroyed if its isolation voltage capability is less than the high voltage supply setting. Crowbar techniques may be used in lab set-ups to provide rapid turn-off and forestall the test being described as "destructive." Steady-state isolation voltage is usually specified as a fixed percentage of the measured surge capability, although life tests are the proof of the rating. Application Engineering believes conservative design practices are required in the use of isolation voltage ratings, due to the transients normally observed when line voltages are monitored and the catastrophic effect, on the system, of a failure.

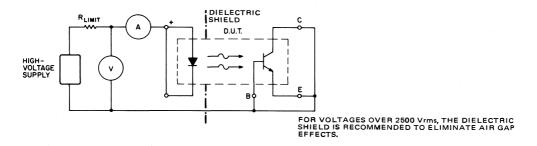


Fig. 71 - Isolation voltage test.

b). Isolation resistance is measured at voltages far below the surge isolation capability, and has less potential for damaging the device being tested. The test is illustrated schematically here, and requires the procedures normally used when measuring currents below a microampere.

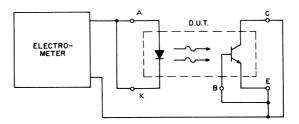


Fig. 72 - Measuring of isolation resistance.

c). Isolation capacitance is a straightforward capacitance measurement. The capacitance of couplers utilizing the Harris patented glass dielectric process is quite independent of applied voltage and frequency. Typical values are less than 1pF, limiting the selection of measurement equipment. The H11AV wide glass dielectric has less than 0.5pF, which requires socket shielding to accurately measure.

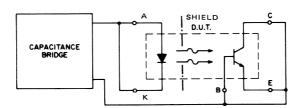
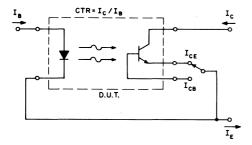


Fig. 73 - Input to output capacitance test circuit.

- **2. Transfer Characteristics** are normally easily measured on standard measurement equipment as the IRED can be treated as the input terminal of a discrete device.
- a). Current Transfer Ratio (CTR) can be tested as  $h_{FE}$  of a transistor, both the phototransistor and photodiode response, and Input Current to Trigger ( $I_{FT}$ ) can be tested as gate trigger current of an SCR. Pinout and the connection of base-emitter or gate-cathode resistors normally require use of special test sockets.



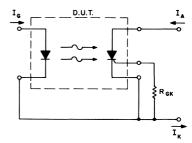


Fig. 74a - CTR tested as transistor HFE.

Fig. 74b - IFT tested as SCR IGT.

These sockets are illustrated above. Some commercial test equipment provides very poor resolution readings of CTR in the  $h_{FE}$  mode due to the readout system being designed for readings greater than 10. This would correspond to a CTR of 1000%, a reasonable value for a darlington, but not a transistor output coupler. Curve tracers are well suited for use in this manner and some allow measurements to be made with the IRED pulsed at high current and low duty cycles.

b). Switching times on simple detectors are measured using the technique illustrated below. Isolation of the input device from the output device allows a freedom of grounding which can simplify test set-up in some cases. The turn-on parameters are  $t_d$ —delay time and  $t_r$ —rise time. These are measured in the same manner on the phototransistor, photodarlington, and photoSCR output couplers. The turn-off parameters for transistor and darlington outputs are  $t_s$ —storage time and  $t_f$ —fall time.

 $t_d$  — delay time. This is the time from the 10% point of the final value of the input pulse to the 10% point of the final value of the output pulse.

t<sub>r</sub> - rise time. The rise time is the time the leading edge of the output pulse increases from 10% of the final value to 90% of the final value.

t<sub>s</sub> — storage time. The time from when the input pulse decreased to 90% of its final value to the point where the output pulse decreased to 90% of its final value.

t<sub>f</sub> — fall time. The time where an output pulse decreases from the 90% point of its final value to the 10% point of its final value.

SCR turn-off times are circuit controlled, and the measurement technique is detailed in the GE SCR Manual.

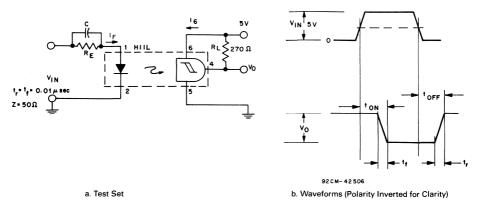


Fig. 75 - Switching time testing.

c). The parameters of the bilateral analog FET are of most interest at low level. Most of the parameters of interest can be read in the simple circuit in Figure 76, but some precautions are required to maintain accuracy. Kelvin contacts to the DUT are required and should insure the elimination of ground loop IR drop which can cause errors, dissimilar metal contacts or temperature gradients causing thermal voltage errors and electromagnetic pick up errors. The latter is especially important when 60Hz ac data is generated. Signal levels must be controlled to maintain bias within the linear region for accurate resistance measurements, since the maximum signal level for linear operation is a function of the DUT resistance. This effect is quantified by testing the H11F as an element of a resistive bridge and increasing the bridge signal level until distortion causes an output signal of specified amplitude.

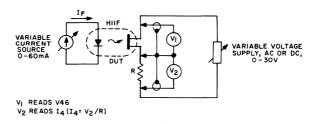


Fig. 76 - H11F parameter testing.

- d). Schmitt Trigger Parameter Measurement. The digital nature of the H11L transfer characteristics make it quite compatible with standard digital logic circuit test equipment in standard configurations.
- e). Triac Driver Testing. The triac driver family of devices is tested using the same techniques documented for discrete triac testing in the GE SCR Manual. The isolation between the IRED and switch allows convenient gate polarity selection. Two items require special attention: commutating dV/dt and zero voltage switch parameters. Most discrete triac test equipment for dV(c)/dt requires modification to lower the test current to the range of the triac driver. When testing zero voltage switch triac drivers, the blocking voltage effect on trigger sensitivity must be considered.

# Safety

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## **SAFETY**

## RELIABILITY AND SAFETY

Optoelectronics may be used in systems in which personal safety or other hazard may be involved. All components, including semiconductor devices, have the potential of failing or degrading in ways that could impair the proper operation of such systems. Well-known circuit techniques are available to protect against and minimize the effects of such occurrences. Examples of these techniques include redundant design, self-checking systems and other fail-safe techniques. Fault analysis of systems relating to safety is recommended. Potential device reaction to various environmental factors is discussed in the reliability section of this manual. These and any other environmental factors should be analyzed in all circuit designs, particularly in safety-related applications.

If the system analysis indicates the need for the highest degree of reliability in the component used, it is recommended that Harris Semiconductor be contacted for a customized reliability program.

## SAFETY STANDARDS RECOGNITION

Harris Semiconductor optoelectronic devices are tested and recognized by safety standards organizations around the world. These organizations are primarily interested in the potential electrical and fire hazards of optoisolators. This is reflected in standards existing only for these particular device types and in the requirements these standards place on the devices. As Harris introduces new optoelectronic devices they are evaluated to determine if an applicable standard exists, and submitted for approval testing if such standards apply.

Currently Harris optoelectronic devices are recognized by Underwriters Laboratories Inc. (U.L.) and Verband Deutscher Elektrotechniker e. V. VDE Profstelle (VDE). The approvals, as of this date, are:

TABLE 14: OPTOISOLATOR APPROVALS

(ALL STANDARD HARRIS SEMICONDUCTOR OPTOISOLATORS ARE COVERED UNDER U.L. COMPONENT RECOGNITION PROGRAM FILE No. E51868)

PART NUMBER	VDE SPECIFICATION NUMBER	CERTIFICATE NUMBER
CNY17 I CNY17 II CNY17 III CNY17 IV	0883/6.80, 0110/11.72, 0110B	22757, 35025
CNY51	0883/6.80, 0110/11.72, 0110B	22758, 35025
GFH601 II GFH601 III GFH601 IV	0883/6.80, 0110/11.72, 0110B 0804/1.82, 0806/8.81, 0110B	30415, 35025
H11A1 H11A3	0883/6.80, 0110/11.72, 0110B 0884*	22755, 35025 63725
H11A2 H11A4	0883/6.80, 0110/11.72, 0110B 0884*	22756, 35025 63725
H11AV1 H11AV1A H11AV2 H11AV2A H11AV3 H11AV3A	0883/6.80, 0110/11.72, 0110B 0860/8.81, 0806/8.81 0804/1.83, 0750T1/5.82 IEC601T1, IEC380, IEC65 0884*	30440, 35025 63724

## ISOLATION VOLTAGE SAFETY STANDARDS OVERVIEW POSSIBLE HAZARDS

## **Toxicity**

Although gallium arsenide and gallium aluminum arsenide are both arsenic compounds, under normal use conditions they should be considered relatively benign. Both materials are listed by the 1980 NIOH "Toxicology of Materials" with LD<sub>50</sub> values comparable to common table salt. Accidental electrical or mechanical damage to the devices containing these IRED pellets should not affect the toxic hazard, so the units can be applied, handled, etc. as any other semiconductor device. Although the pellets are small, chemically stable and protected by the device package, conditions that can break these crystaline compounds down into elements or other compounds should be avoided.

## Near Infrared Theshold Limit Value

The eye may be damaged from infrared light. The most applicable guideline to evaluate IRED's for this hazard is the 1979 "American Conference of Governmental Industrial Hygenists Handbook." On pages 90 and 91 recommended threshold limit values for pulse (item 1) and long term (item 3) infrared exposure are given. When operated within device maximum ratings, the maximum irradiance external to the IRED package doesn't approach these TVL's for any of the present GaAs or GaA1As devices.

To evaluate specific situations, the IRED pellet and its reflector represent a roughly Lambartian source of about 1mm diameter in all current discrete IRED types.

\* Approved voltage categories of DIN VDE 0884 from DIN VDE 0109/12.83, Table 1

VOLTAGES DERIVED FROM RATED MAINS	PREFERRED INSULATION TEST VOLTAGES FOR SERVICE CLASS			
VOLTAGES UP TO VAC (VRMS) OR VDC	ı	11	111	IV
50	330	500	800	1,500
100	500	800	1,500	2,500
150	800	1,500	2,500	4,000
350	1,500	2,500	4,000	6,000
600	2,500	4,000	6,000	

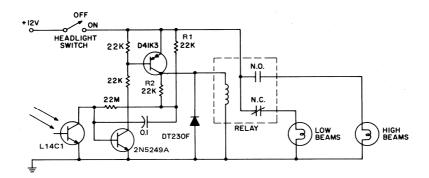
## **Optoelectronics Circuits**

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## OPTOELECTRONIC CIRCUITS

## LIGHT DETECTING CIRCUITS

Light detecting circuits are those circuits that cause an action based on the level of light received by the photo detector.



RELAY: 12V, 0.3A COIL: 20A, FORM C, CONTACTS OR SOLID-STATE SWITCHING OF 16A STEADY-STATE 150A COLD FILAMENT SURGE. RATING.

LENS: MINIMUM 1" DIAMETER, POSITIONED FOR ABOUT 10° VIEW ANGLE.

Fig. 77 - Headlight dimmer.

## Automatic Headlight Dimmer

This circuit switches car headlights to the low beam state when it senses the lights of an on-coming car. The received light is very low level and highly directional, indicating the use of a lens with the detector. A relatively large amount of hysteresis is built into the circuit to prevent "flashing lights." Sensitivity is set by the 22Megohm resistor to about 0.5 ft. candle at the transistor (0.01 at the lens), while hysteresis is determined by the R1,R2 resistor voltage divider, parallel to the D41K3 collector emitter, which drives the 22Megohm resistor; maximum switching rate is limited by the  $0.1\mu F$  capacitor to  $\approx 15/minute$ .

## Slave Photographic Xenon Flash Trigger

This circuit is used for remote photographic flash units that will flash at the same time as the flash attached to the camera. This circuit is designed to the trigger cord or "hot shoe" connection of a commercial portable flash unit and triggers the unit from the light produced by the light of the flash unit attached to the camera. This provides remote operation without the need for wires or cables between the various units. The flash trigger unit should be connected to the slave flash before turning the flash on (to prevent a dV/dt triggered flash on connection).

The L14C1 phototransistor has a wide, almost cosine viewing angle so alignment is not critical. If a very sensitive (long range), more directional remote trigger unit is desired, the circuit may be modified using a L14G2 lensed phototransistor as the sensor. The lens on this transistor provides a viewing angle

of approximately  $10^{\circ}$  and gives over a 10 to 1 improvement in light sensitivity (3 to 1 range improvement). Note that the phototransistor is connected in a self-biasing circuit which is relatively insensitive to slow changing ambient light, and yet discharges the  $0.01\mu F$  capacitor into the C106D gate when illuminated by a photo flash. For physically smaller size, the C106D may be replaced by a C205D, if the duty cycle is reduced appropriately.

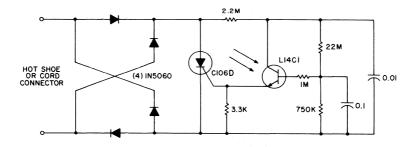


Fig. 78 - Sensitive, directional, slave photo flash trigger.

## Automatic Night Light Switches

These circuits are light level sensors that turn on a light when the visible light falls below a specific level. The most common of these circuits turns on street lamps and yard lights powered by 60 Hz lines.

## Line Voltage Operated Automatic Night Light

An example of this type of circuit is illustrated in Figure 79. It has stable threshold characteristics due to its dependence on the photo diode current in the L14C1 to generate a base emitter voltage drop across the sensitivity setting resistor. The double phase shift network supplying voltage to the ST-4 trigger insures triac triggering at line voltage phase angles small enough to minimize RFI problems with a lamp load. This eliminates the need for a large, expensive inductor, contains the dV/dt snubber network, and utilizes lower voltage capacitors than the snubber or RFI suppression network normally used.

The addition of a programmable unijunction timer can modify this circuit to turn the lamp on for a fixed time interval each time it gets dark. Only the additions to the previous circuit are shown in the interest of simplicity. When power is applied to the lamp, the 2N6028 timer starts. Upon completion of

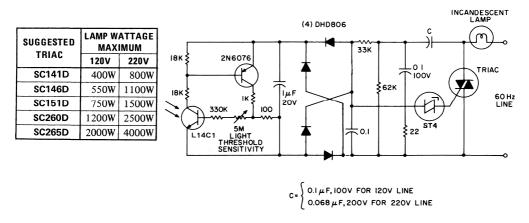


Fig. 79 - Line voltage operated automatic night light.

the time interval, the H11C3 is triggered and turns off the lamp by preventing the ST-4 from triggering the triac. The SCR of the H11C3 will stay on until the L14C1 is illuminated and allows the 2N6076 to commutate it off. Due to capacitor leakage currents, temperature variations and component tolerances, the time delay may vary considerably from nominal values.

Another common use for night light circuits is to turn on remote illumination, warning or marker lights which operate from battery power supplies. The simplest circuit is one that provides illumination

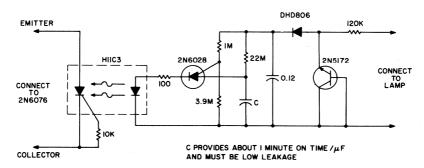
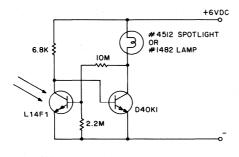


Fig. 80 - Automatic turn-off for night light.

when darkness comes. By using the gain available in darlington transistors, this circuit is simplified to use just a photodarlington sensor, a darlington amplifier, and three resistors. The illumination level will be slightly lower than normal, and longer bulb life can be expected, since the D40K1 saturation voltage lowers the lamp operating voltage slightly.

In warning and marker light applications a flashing light of high brightness and short duty cycle is often desired to provide maximum visibility and battery life. This necessitates using an output transistor which can supply the cold filament surge current of the lamp while maintaining a low saturation voltage. Oscillation period and flash duration are determined in the feedback loop, while the use of a phototransistor sensor minimizes sensitivity variations.



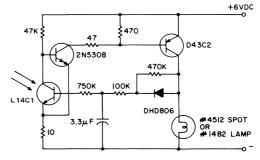


Fig. 81- Portable automatic night light.

Fig. 82 - Automatic night flashing light.

Another form of night light is line operated power outage lights, which provides emergency lighting during a power outage. The phototransistor should be positioned to maximize coupling of both neon light and ambient light into the pellet, without allowing self illumination from the 6V lamp. Many circuits of this type also use line voltage to charge the battery.

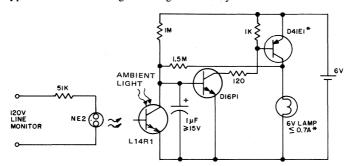


Fig. 83 - Line operated power outage light.

# Sun Tracker

In solar cell array applications and solar instrumentation, it is desired to monitor the approximate position of the sun to allow efficient automatic alignment. The L14G1 lens can provide about 15° of accuracy in a simple level sensing circuit, and a full hemisphere can be monitored with about 150 phototransistors.

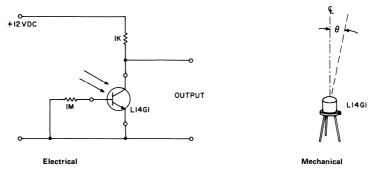


Fig. 84 - Sun tracking circuit.

The sun provides  $\approx 80 \text{ mW/cm}^2$  to the L14G1 when on the centerline. This will keep the output down to  $\leq 0.5 \text{V}$  for  $\theta \leq 7.5^{\circ}$ .

The sky provides  $\approx 0.5 \text{ mW/cm}^2$  to the L14G1 and will keep the output greater than 10V when viewed. White clouds viewed from above can lower this voltage to  $\approx 5\text{V}$  on some devices.

This circuit can directly drive TTL logic by using the 5V supply and changing the load resistor to  $430\Omega$ . Different bright objects can also be located with the same type of circuitry simply by adjusting the resistor values to provide the desired sensitivity.

## Flame Monitor

Monitoring a flame and direct switching of a 120V load is easily accomplished using the L14G1 for "point sources" of light. See Figure 85. For light sources which subtend over 10° of arc, the L14C1

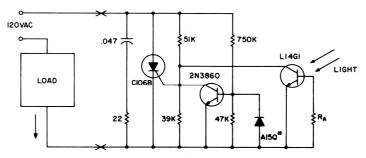


Fig. 85 - Flame out monitor switch.

\*The A15Q may be replaced by 100 pF shunting a DHD800. Wire for minimum crosstalk, 120V to gate, using minimum lead lengths. R<sub>A</sub> is selected from the following chart for light level threshold programming.

R <sub>A</sub> SELECTION GUIDE FOR ILLUMINATION									
HOLD OFF LIGHT LEVEL $\approx 20$ $\approx 40$ $\approx 80$ $\approx 200$ $\approx 400$ FOOT CANDLE									
R <sub>A</sub> , Incandescent Light	N.A.	1500	270	68	33	ΚΩ			
R <sub>A</sub> , Flame Light	220	75	30	12	6.2	ΚΩ			
R <sub>A</sub> , Fluorescent Light	N.A.	N.A.	2200	180	68	ΚΩ			

should be used and the illumination levels raised by a factor of 5. This circuit provides zero voltage switching to eliminate phase controlling.

## Brightness Controls

The illumination level of lighted displays should be lowered as the room ambient light drops to avoid undesirable or unpleasant visual effects. This circuit provides a very low cost method of controlling the light level. Circuit power is obtained from a relatively high source impedance transformer or motor windings, normally used to drive the low voltage lamps used in these functions. It should be noted that the bias resistors are optimized for the 20V,  $30\,\Omega$  source, and must be recalculated

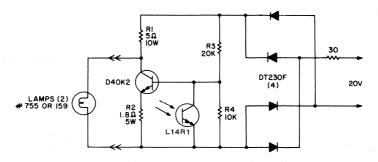
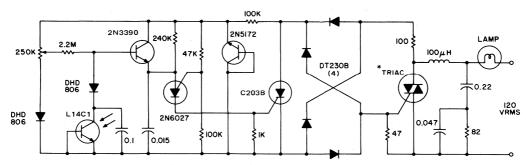


Fig. 86 - Ambient sensitive display illumination.

for other sources. The L14R1 is placed to receive the same ambient illumination as the display and should be shielded from the light of the display lamps.

Another form of automatic brightness control maintains a lamp at a constant brightness over a wide range of supply voltages. This circuit utilizes the consistency of photo diode response to control the phase angle of power line voltage applied to the lamp and can vary the power applied to the lamp between that available and  $\approx 30\%$  of available. This provides a candlepower range from 100% to less than 10% of nominal lamp output. The  $100\mu$ H choke, resistor and capacitors form a RLC filter network and is used to eliminate conducted RFI.

Many other light sensitive circuits are feasible with these versatile devices, and those included here are chosen to illustrate a range of practical, cost-effective designs.



\*The triac is matched to the lamp per chart in Figure 79.

Fig. 87 - Constant brightness control.

#### **DETECTING OBJECTS WITH LIGHT**

This section is devoted to circuits that use a light source and a light sensor, or arrays of either or both, to sense objects by affecting the light path between the source and detector. Normally, the light is blocked or reflected by the object to be sensed, although modulation of the transmission medium is also common.

## Paper Sheet Discriminator for Printing and Copying Machines

A common problem with sheet paper conveying systems is the inadvertant transport of two sheets of paper, instead of one, due to mutual adherence by vacuum or static charges. The simple circuit depicted in Figure 88 outputs power to the drive motor when one or no sheets are being fed, but interrupts motor power when two or more superimposed sheets pass through the optodetector slot. The optodetector may be either an H21B darlington interruptor module or an H23B matched emitter-detector pair. The output from the optodarlington is coupled to a Schmitt trigger, comprising transistors  $Q_1$  and  $Q_2$  for noise immunity and minor paper opacity variation immunity. When the Schmitt is "on," gate current is applied to the SC148D output device. The dc power supply for the detector and Schmitt is a simple R-C diode half-wave configuration chosen for its low cost (fewer diodes, no transformers) and minimum bulk. While such a supply is directly coupled to the power triac, this is precluded by current drain considerations (50mA dc for the gate drive alone). Note that direct coupling of the Schmitt to the output triacs is preferred as *RFI is virtually* eliminated with the quasi-DC gate drive.

To further reduce dc drain on the power supply, the LED drive current is separately derived from a diode bridge and current limiting capacitor. In addition to minimum dissipation and zero loading on the dc supply, this connection also has the merit of maximizing LED current at each zero voltage crossover of the ac sinewave, thus guaranteeing that drive to the Schmitt is solid (at least with no or one sheet of paper) as the triacs commutate off and back on again. The fact that the Schmitt switches twice each cycle, in phase with the zero diode current points, is now an advantage since gate drain on the dc supply is *completely* eliminated during these "off" periods. Because the "off" periods coincide with maximum instantaneous ac supply voltage when the triac is always hard on (thanks to the phase-shifted LED current), the circuit is virtually immune to the load power factor variations associated with ac motors.

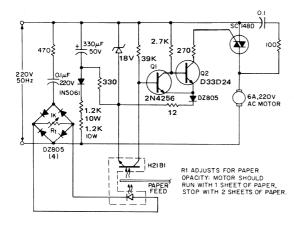


Fig. 88 - Paper sheet discriminator with zero voltage switching triac motor drive.

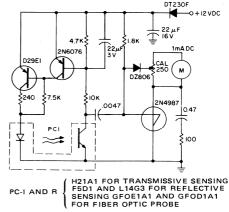


Fig. 89 - Optical pickup tachometer.

## Optical Pick Up Tachometer

Remote, non-contact, measurement of the speed of rotating objects is the purpose of this simple circuit. Linearity and accuracy are extremely good and normally limited by the milliammeter used and the initial calibration. This circuit is configured to count the leading edge of light pulses and to ignore normal ambient light levels. It is designed for portable operation since accuracy is not sensitive to supply voltage within supply voltage tolerances. As illustrated in Figure 89, full scale at maximum sensitivity of the calibration resistance is read at about 300 light pulses per second. A digital volt meter may be used, on the 100 mV full scale range, in place of the milliammeter, by shunting its input with a  $100 \, \mu$ F capacitor. This R-C network replaces the filtering supplied by the analog meter.

# Drop Detector

The self-biasing configuration is useful any time small changes in light level must be detected, for example, when monitoring very low flow rates by counting drops of fluid. In this bias method, the photodarlington is DC bias stabilized by feedback from the collector, compensating for different photodarlington gains and light emitting diode outputs. The  $10\mu$ F capacitor integrates the collector voltage feedback, and the 10M resistor provides a high base source impedance to minimize effects on optical performance. The detector drop causes a momentary decrease in light reaching the chip, which causes collector voltage to momentarily rise, generating an output signal.

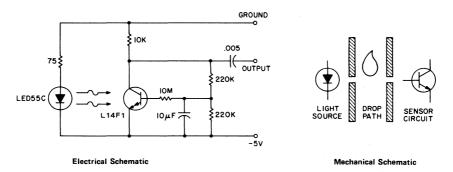


Fig. 90 - Low light level drop detector.

The initial light bias is small due to output power constraints on the light emitting diode and mechanical spacing system constraints. The change in light level is a fraction of this initial bias due to stray light paths and drop translucence. The high sensitivity of the photodarlington allows acceptable output signal levels when biased in this manner. This compares with unacceptable signal levels and bias point stability when biased conventionally, i.e., base open and signal output across the collector bias resistor.

## Paper Tape Reader

When computer peripheral equipment is interfaced, it is convenient to work with logic signal levels. With a nominal 4V at the output dropping to -0.6V on illumination, this circuit reflects the requirements of a high-speed, paper tape optical reader system. The circuit operates at rates of up to 1000 bits per second. It will also operate at tape translucency such that 50% of the incident light is transmitted to the sensor, and provide a fixed threshold signal to the logic circuit, all at low cost. Several circuit tricks are required. Photodarlington speed is enhanced by cascode constant voltage biasing. The output threshold and tape translucency requirements are provided for by sensing the output voltage and providing negative feedback to adjust the cascode transistor bias point. Circuit tests confirmed operating to 2000 bits per second at ambient light levels equal to signal levels.

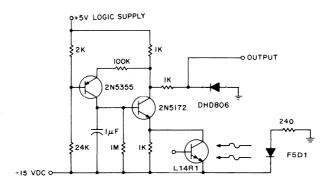


Fig. 91 - High speed paper tape reader circuit.

## Motor Speed Control Circuits

These controls may be of the open loop type, where light just provides a no-contact, non-wearing circuit input from a person or machine which monitors the output of the motor, or a closed loop type, where the light monitors motor speed as a tachometer and maintains a fixed, selected, speed over a range of load and line conditions.

Closed loop, tachometer feedback control systems utilizing the H21A1 and a chopper disc, provide superior speed regulation when the dynamic characteristics of the motor system and the feedback system are matched to provide stability. The tachometer feedback systems illustrated in Figure 92 were designed around specific motor/load combinations and may require modification to prevent hunting or oscillation with other combinations. This dc motor control utilizes the optachometer circuit previously shown to control a P.U.T. pulse generator which drives the D44E1 darlington transistor which powers the motor.

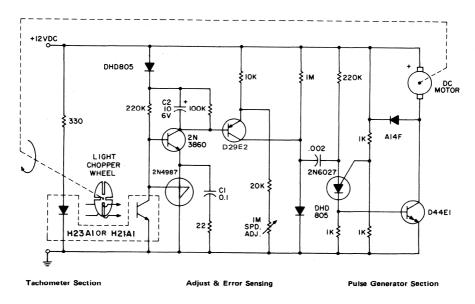


Fig. 92 - DC motor, tachometer feedback, PWM, speed control.

The ac motor control in Figure 93 illustrates feedback speed regulation of a standard ac induction motor, a function difficult to accomplish otherwise than with a costly, generator type, precision tachometer. When the apertured disc attached to the motor shaft allows the light beam to cross the

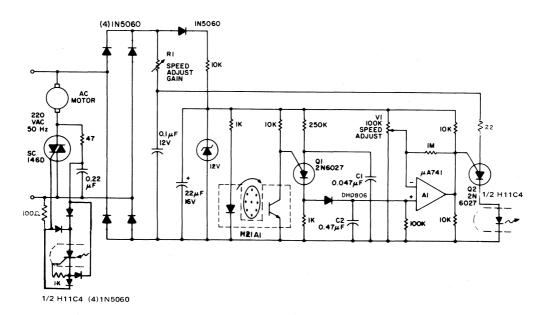
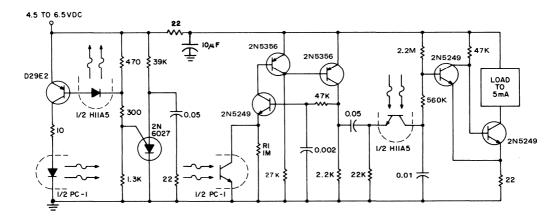


Fig. 93 - Closed loop ac motor speed control with optical tachometer.

interupter module, the programmable unijunction transistor,  $Q_1$ , discharges capacitor,  $C_1$ , into the much larger storage capacitor,  $C_2$ . The voltage on  $C_2$  is a direct function of the rotational speed of the motor. Subsequently, this speed-related potential is compared against an adjustable reference voltage,  $V_1$ , through the monolithic operational amplifier,  $A_1$ , whose output, in turn, establishes a dc control input to the second P.U.T. ( $Q_2$ ). This latter device is synchronized to the ac supply frequency and furnishes trigger pulses in conventional manner to the triac at a phase angle determined by the speed control,  $R_1$ , and by the actual speed of the motor.

# Long Range Object Detector

When long ranges must be worked with IRED light sources, and when high system reliability is required, pulsed mode operation of the IRED is required. Additional reliability of operation is attained by synchronously detecting the photodetector current, as this circuit does. PC-1 is an IRED and phototransistor pair which detect the presence of an object blocking the transmission of light from the



PC-1 SELECTION	TRANSMISSION RANGE	REFLECTIVE RANGE
H23A1	5"	1"
LED56 and L14Q1	12"	3"
LED56 and L14G1	18"	41/2"
LED55C and L14G1	32"	8"
1N6266 and L14G3	48"	12"
F5D1 and L14G3	80"	20"
F5D1 and L14P2	200"	50"

Fig. 94 - Long range object detector.

IRED to the phototransistor. Relatively long distance transmission is obtained by pulsing the IRED, with about  $10\mu$ sec pulses, at a 2msec period, to 350mA via the 2N6027 oscillator. The phototransistor current is amplified by the 2N5249 and 2N5356 amplifier to further increase distance and allows use of the H11A5, also pulsed by the 2N6027, as a synchronous detector, providing a failsafe, noise immune signal to the 2N5249 pair forming a Schmitt trigger output.

This design was built for battery operation, with long battery life a primary consideration. Note that another stage of amplification driving the IRED can boost the range by 5 to 10 times, limited by the IRED  $V_{\rm F}$ , and a higher supply voltage for the IRED can double this.

## Transmitting Information With Light

Transmission of electronic information over a light beam is the major use of optoelectronics today. These applications range from the use of optocouplers transmitting information between IC logic circuits and power circuits, between power lines and signal circuits, between telephone lines and control circuitry, to the pulse modulated systems which transmit information through air or fiber optics over relatively great distances.

## Analog Information

The circuits illustrated here are designed to transmit analog, i.e., linear signals, optoelectronically. In this section the trade-offs between communication distance, fidelity, noise immunity and other design constraints are illustrated by example in an attempt to provide an understanding of this technology. Simple voice transmission systems can be made using infrared light through air as the signal path. Power dissipation in the IRED limits the ultimate capability of this type of system for distance and modulation frequency, due to the trade-off of power dissipation, pulse width and pulse frequency. In applications where transmission of information without electromagnetic interference is imperative, a relatively low cost system can be built around an IRED, a phototransistor, and low cost glass fiber optics, which can provide transmission over distances greater than 1km, or at rates over 100KHz using low cost driving circuitry. Higher frequency systems for long distance operation require pulse generators capable of generating short ((200nsec), high current pulses with leading edge overshoot, adding considerably to system expense, and heat sinking of the IRED. Laser diode systems provide higher performance at higher cost, and telecommunications fiber optic transmission systems provide an example of the practical limits of this technology. Using the low cost Harris IRED's and detectors, frequency modulation and pulse data transmission are compatible with moderate frequency systems. The Harris Semiconductor GaAlAs and GaAs IREDs are very efficient and have excellent stability due to the liquid epitaxial processing, which also defines its switching parameters and speed of response. This response time varies from about 100 to 500nsec, depending on bias level, and indicates that, for a given IRED power dissipation, and frequency of operation, there is an optimum input pulse width which will maximize pulse power output and, thereby, range of transmission. For the system illustrated in the next application, this was determined to be about 500nsec, although power output was within 10% of the maximized value for widths from 170nsec to over 1 usec. This was determined by monitoring the power output with a photo cell connected phototransistor (the photo response with a low value load resistor is about an order of magnitude faster than the IRED) as the pulse width to the IRED is changed, maintaining other system parameters constant. Peak power input for the desired maximum power dissipation can be calculated for each pulse width and multiplied by the normalized peak power out and efficiency, at that pulse width and input power, respectively, to obtain a set of values of peak available power out, as a function of pulse width, at the frequency, waveshape and average power dissipation desired. Plotting the set of values produced the curve shown in Figure 95, which allowed analytical system optimization. It should be noted that peak light output occurred 50 to 100nsec after peak input

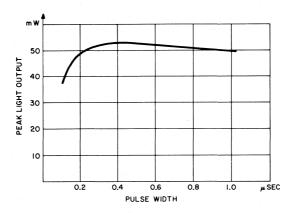


Fig. 95 - Peak light output expected for P<sub>AVE</sub> = .25W, f = 80kHz operation.

current was reached, and the IRED continued to emit light for  $1\mu$ sec after the input current pulse had decreased to negligible levels, which places a peak repetition rate and peak envelope power optimization constraint on designs over 500KHz. To minimize turn on and turn off times of these IRED's, about 1/2nC of charge, per mA forward current, must be injected at turn on and removed at turn off. This, and the compatibility of the beam with focusing systems, is why most high frequency systems are designed around the expensive, relatively short lived, GaAs laser diode.

A relatively simple FM (PRM) optical transmitter was designed around a programmable unijunction transistor (PUT) pulse generator using this information. The basic circuit can be operated at 80KHz and is limited by the PUT-capacitor combination, as higher frequency demands smaller capacitance, which provides less peak output. As illustrated, 60KHz is the maximum modulation frequency. Pulse repetition rate is relatively insensitive to temperature and power supply voltage and is a linear function of  $V_{\rm IN}$ , the modulating voltage. Tested with the receiver illustrated below, useful information transfer was obtained in free air ranges of 12 feet ( $\approx$ 4m). Lenses or reflectors at the light emitter and detector increases range and minimizes stray light noise effects. Greater range can also be obtained by using a higher power output IRED such as the F5D1 in combination with the L14P2 phototransistor. Average power consumption of the transmitter circuit is less than 3 watts.

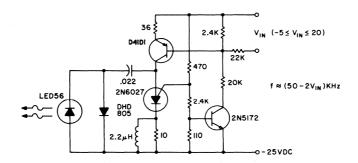


Fig. 96 - 50kHz center frequency FM optical transmitter.

For maximum range, the receiver must be designed in the same manner as a radio receiver front end, since the received signals will be similar in both frequency component and in amplitude of the photodiode current. The major constraint on the receiver performance is signal to noise ratio, followed by e.m. shielding, stability, bias points, parts layout, etc. These become significant details in the final design. This receiver circuit consists of a L14G2 detector, two stages of gain, and a FM demodulator (which is the tachometer circuit, previously illustrated, modified to operate up to 100KHz). Note that

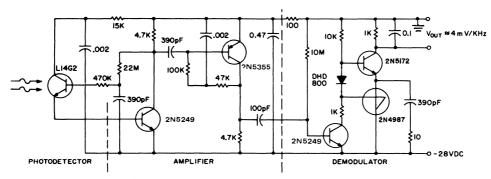


Fig. 97 - Receiver for 50kHz FM optical transmitter.

better sensitivity can be obtained using more stages of stabilized gain with AGC, which lower cost and sensitivity may be obtained by using an H23A1 emitter-detector pair and/or by eliminating amplifier stages. For some applications, additional filtering of the output voltage may be desired.

Fiber optics are extensively used for information transfer, especially at high frequency for wide band width. Often there is a requirement for a low frequency, low cost information transmission link where the isolation, noise immunity and safety features of fiber optics are advantageous.

Many information transfer systems require a two-way flow of information. Although a full duplex system can be implemented in fiber optics, it normally requires two fiber transmitter-receiver sets. Many system needs can be fulfilled by a half-duplex system, in which information can flow in both directions, but only one direction at any given time. The conventional method of building a half-duplex link requires a separate emitter and detector, connected with directional couplers, at each end of the fiber. A half-duplex link illustrating emitter-detector operation is shown in Figure 98. This schematic represents a full, general purpose system, including: approximately 50db compliance range with 1V

RMS output; passive receive, transmit priority (voice-activated) switching logic; 100Hz to 50kHz frequency response; and does not require exotic (expensive) components or hardware. The system is simple, inexpensive, and can be upgraded to provide more capability through use of higher gain band-width amplifier stages. Conversely, performance and cost may be lowered simply by removing undesired features.

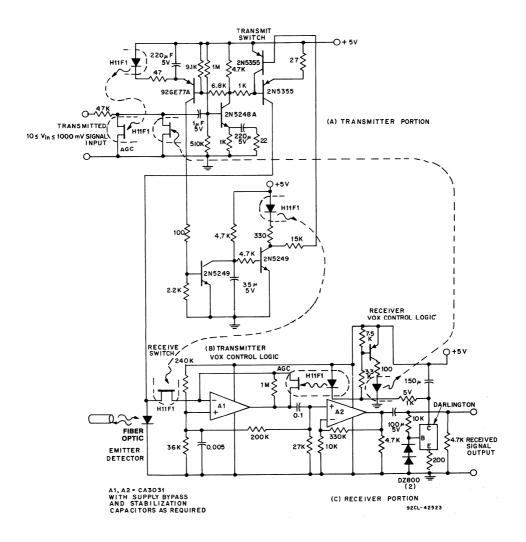


Fig. 98 - Half duplex information link.

UNITS

Circuit operation is easily understood by following the signal through the three portions of the circuit. Both AGC (automatic gain control) circuits utilize the H11F bilateral analog FET optoisolator's variable resistance characteristic to attenuate the signal or modify the feedback path to provide AGC. In these circuits the peak value of the output signal is compared to the  $V_{BE(on)}$  of a transistor-signal peaks which exceed V<sub>BE(on)</sub> turn the transistor on. Collector current of the transistor is capacitively filtered and supplies current to the IRED of the H11F. This lowers the resistance of the analog FET detector, which controls the signal level. In the transmitter, the signal enters via a 47K-H11F AGC attenuator network and passes through two stages of bipolar transistor amplification. The fiber optic emitter bias current from the output of the transistor is about 50mA dc modulated by approximately 80mA peak-to-peak ac for input signals within the compliance of the AGC network (about 10mV RMS to over 2V RMS). IRED bias is normally off until an input signal to the transmitter reaches AGC levels through the VOX control logic which clamps the transmitter output transistor off. The AGC signal level provides pulses of current to the VOX logic which are amplified, filtered and turns off both the clamp on the output transistor (activating the transmitter) and the switch that allows fiber optic emitter photodiode current to flow into the receiver (disabling the receiver). The receiver consists of the VOX controlled H11F bilateral analog FET switch, a transimpedance amplifier stage with AGC control of the gain and a voltage amplifier with a fixed gain of 30db. Note the forward dc bias on the fiber optic emitter provided by the transimpedance amplifier must be below V<sub>F</sub>, yet provide ac signal swings. This receiver gives a reasonable compromise between gain-bandwidth and complexity. It requires 22 components (including op-amp and capacitors) to provide 2.5V p-p output signal for infrared outputs ranging from about  $1\mu W$  to over  $200\mu W$ .

Linear AC Analog Coupler All methods of transmitting D.C. analog information via optical isolation have challenging limitations. Analog A.C. signal isolation with high linearity is much easier. Although I.C. output couplers are advertised for this function, a very simple bias circuit allows the

TANAMETER	I.C. SPECIFICATION	41435 DATA	Civilia
Supply Current	$2 \leq I_S \leq 10$	1 ≤ I <sub>S</sub> ≤ 3	mA
Gain	≥ 100	≥ 200	mV/mA
Voltage Swing	4	5	Volts
Distortion	5	0.3	%
Step Response	1.4	6	μsec
Bandwidth	≥ 100	120	KHz
D.C. Output	$0.2 \leq V_{O} \leq 6$	$1 \leq V_O \leq 6$	Volts

I C SPECIFICATION

Fig. 99 - Linear A.C. coupler.

PERFORMANCE COMPARISON: I.C. COUPLER TO 4N35

4N35 transistor output optocoupler to better the I.C. performance at much lower cost. The circuit is illustrated in Figure 99. Operation is as follows: with the coupler biased in the linear region by the 10mA dc bias on the IRED and the voltage divider on the phototransistor base, photodiode current flows out of the base into the voltage divider, producing an ac voltage proportional to the ac current in the IRED. The transistor is biased as an emitter follower and requires less than 10% of the photodiode current to produce the low impedance ac output across the emitter resistor. Note that the IH11AV1 may be substituted for the 4N35 to provide VDE line voltage rated isolation of less than 0.5pF.

<u>Linear PRM Analog Coupler</u>—A minimum parts count version of this system also provides isolated, linear signal transfer useful at shorter distances or with an optocoupler for linear information transfer. Although the output is low level and cannot be loaded significantly without harming accuracy, a single I.C. operational or instrumentation amplifier can supply both the linear gain and buffering for use with a variety of loads.

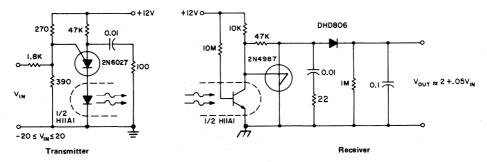


Fig. 100 - Minimum parts count linear PRM isolation circuit.

<u>DC Linear Coupler</u> —The accuracy of direct linear coupling of analog current signals via an optocoupler is determined by the coupler linearity and its temperature coefficient. Use of an additional coupler for feedback can provide linearity only if the two couplers are perfectly matched and identically biased. These are not practical constraints in most equipment designs and indicate the need for a different design approach. One of the most successful solutions to this problem can be illustrated by using an H23 emitter-detector pair and an L14H4, as illustrated in Figure 101. The H23 detector and L14H are placed so both are illuminated by the H23 IRED emitter. Ideally, the circuit is mechanically designed such that the H23 emitter may be positioned to provide  $V_{OUT}=2.8V$  when  $V_{IN}=0$ , thereby

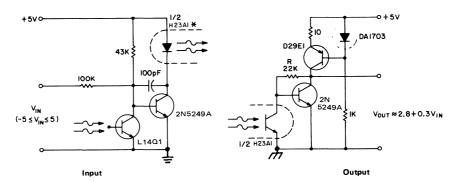


Fig. 101 - Linear optical coupler circuit.

insuring collector current matching in the detectors. Then all three devices are locked in position relative to each other. Otherwise, R may be adjusted to provide the proper null level, although temperature tracking should prove worse when R is adjusted. Note that the input bias is dependent on power supply voltage, although the output is relatively independent of supply variations. Testing indicated linearity was better than could be resolved, due to alignment motion caused by using plastic tape to lock positions. The concept of feedback control of IRED power output is useful for both information transmission and sensing circuitry.

<sup>\*</sup>Closely positioned to illuminate L14Q1 and H23A1 Detector, such that  $V_{OUT}\cong 2.8V$  at  $V_{IN}$  = 0.

# Digital Information

The circuits illustrated here are used to transmit information in the form of switch states, i.e., on and off (or zero and one states). Most of these circuits are designed to interface with commercial integrated circuit logic by receiving and/or providing signal for the logic circuit. Due to switching speeds of both emitters and detectors, no optocoupler can provide true speed compatability with only the slowest logic families. For this reason, the logic compatibility of these circuits is level compatibility at worst case conditions, i.e., zeros and ones will meet the I.C. specified levels over the ranges of conditions specified.

TTL — This is the most common logic family, has the most functions available, and is the basis for the IEEE digital interface standard for programmable instruments. There is also a wide variety of standard types of TTL (i.e. high speed, Schottky, LSI, etc.) each of which has different logic level or logic level conditions (primarily source and sink currents) each of which can place different requirements on an optocoupler required to interface with it. To simplify some problems of interfacing TTL logic with optocouplers, Harris surveyed the specifications of SSI devices (single function devices, i.e., "or" gates, flip-flops, etc.) and has specified a series of photo transistor and photoSCR couplers to be level compatible with the common 7400, 74H00 and 74S00 series TTL over the range of gate parameters, power supply and temperature variations specified. These couplers are designated the H74 series and, are very cost effective. They are specified with specific values of 5% tolerance bias resistors in a defined configuration. This eliminates any chance of misapplication or circuit malfunction. The circuits and logic truth table in Figures 102 and 103 illustrate application of this series of couplers. Noise margin considerations are minimized with these couplers since the slow switching speeds of the optocoupler do not allow reaction to the high speed hash that is provided for by noise margins.

	TEST CONDITIONS							LIMITS			
PARAMETER	-		I <sub>SINK</sub> Min.   Max.		Min.	Max.	Units				
V <sub>OUT</sub> (1)	4.5V	:				-0.4mA	2.4		Volts		
V <sub>OUT</sub> (0)	4.5V				12.0mA			0.4	Volts		
V <sub>IN</sub> (1)		5.5V		1.0mA			2.0		Volts		
V <sub>IN</sub> (0)		5.5V	-1.6mA					0.8	Volts		

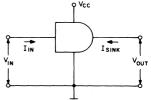
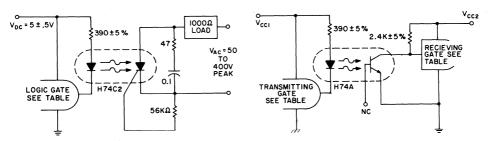


Fig. 102 - Characteristics required of TTL gates which are to be interfaced by H74 series.



LOGIC TO POWER COUPLING H74 BIAS CIRCUIT

Fig. 103 - H74 series TTL logic coupling.

LOGIC TO LOGIC COUPLERS H74A1 BIAS CIRCUIT

Fig. 103 - H74 series TTL logic coupling.

For higher speed applications, up to 1mHz NRZ, the Schmitt trigger output H11L series optoisolator provides many other attractive features. The 1.6mA drive current allows fan-in circuitry to drive the IRED, while the 5Volt,  $270\Omega$  sink capability and 100nsec transition times of the output add to the logic coupling flexibility.

Low power TTL, low power Schottky clamped TTL, MSI TTL and SI TTL circuits will not generally provide the current sinking capability indicated in the H74 bias chart. The H74 series optocoupler can still provide the means of using a general purpose circuit that will interface with all these types and between all the types. A simple stage of transistor amplification as an output buffer allows the low current sink capability (down to  $100\mu$ A) to drive the IRED. The logic sense is not changed. Logic zero out provides current to the IRED which activates the output of the optocoupler.

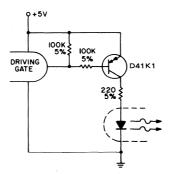


Fig. 104 - IRED drive from low power, MSI and LSI TTL.

High threshold versions of TTL (HNIL, etc.) can normally be used without buffering by increasing the bias resistor values to keep worst case currents within the TTL range at the higher supply voltages used with these logic circuits.

<u>CMOS</u> — Like all low power (bipolar and MOS) logic, CMOS inputs are easily driven by optocoupler outputs. Although some couplers are advertised by CMOS output compatible, careful examination reveals the CMOS gate must be capable of sinking/sourcing several hundred microamps to drive the light source. As standard CMOS logic operates down to 3V supply voltages and is specified as low as  $30\mu$ A maximum current sinking/sourcing capability, it is again necessary to use a buffer transistor to provide the required current to the IRED if CMOS is to drive the optocoupler. As in the case of the low output TTL families, the H74A output can drive a multiplicity of CMOS gate inputs or a standard TTL input given the proper bias of the IRED. The optocoupler driving circuit is illustrated in Figure 105. When the H11L1 is used, a lower gain transistor such as the 2N4256 can be used with a 1k ohm resistor.

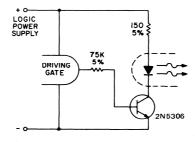


Fig. 105 - General purpose CMOS IRED bias circuit.

Note the logic sense is changed, i.e., a one logic state drives the IRED on. This circuit will provide worst case drive criteria to the IRED for logic supply voltages from 3V to 10V, although lower power dissipation can be obtained by using higher value resistors for high supply voltages. If this is desired, remember the worst case drive must be supplied to the IRED with minimum supply voltage, minimum temperature and maximum resistor tolerances, gate saturation resistance and transistor saturation voltages applied. For the H74 devices, minimum IRED current at worst case conditions (zero logic state output of the driving gate) is 6.5mA, while the H11L1 is 1.6mA.

<u>PMOS and NMOS</u> — These logic families have current source and sink capabilities similar to the previously mentioned CMOS worst case. Normal logic supply voltages range from 6V to 30V at these drive levels and bias circuitry design must account for this. N MOS provides higher current sinking than sourcing capability, while P MOS is normally the opposite. As these logic families are found in a wide variety of custom and standard configurations (from calculators to micro computers to music synthesizers, etc.), a generalized optocoupler bias circuit is impossible to define. The form of the circuit will be similar to the low output TTL circuit for N MOS and similar to the CMOS circuit for P MOS. Bias resistor constraints are as previously mentioned.

#### Telecommunications Circuits

The largest information transmitting system is the United States telephone system, many functions of which could benefit from application of optocouplers. This section will document a few of these applications, although it should be noted that very detailed knowledge of the particular telephone system and its interaction with the optocoupler circuit is required to ensure proper circuit operation and prevent damage to the phone system.

Ring Detectors — These circuits are designed to detect the 20Hz,  $\approx 86$ V rms ring signal on telephone lines and initiate action in an electrically isolated circuit. Typical applications would include automatic answering equipment, interconnect/interface and key systems. The circuits illustrated in Figures 106-108 are "bare bones" circuits designed to illustrate concepts. They may not eliminate the

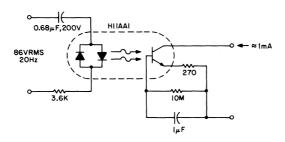
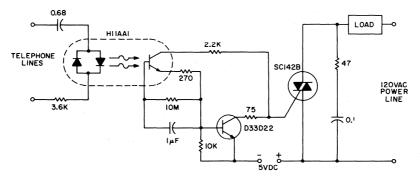


Fig. 106 - Simple ring detector circuit.

ac/dc ring differentiation, 60Hz noise rejection, dial tap rejection and other effects that must be considered in field application. The first ring detector is the simplest and provides about a 1mA signal for a 7mA line loading for 1/10sec after the start of the ring signal. The time delay capacitor provides a degree of dial tap and click suppression, as well as filtering out the zero crossing of the 20Hz wave.

This circuit provides the basis for a simple example, a ring extender that operates lamps and buzzers from the 120V, 60Hz power line while maintaining positive isolation between the telephone

line and the power line. Use of the isolated tab triac simplifies heat sinking by removing the constraint of isolating the triac heat sink from the chassis.



Maximum Load: 500 W Lamp or 800 W Inductive or Resistive

Fig. 107 - Remote ring extender switch.

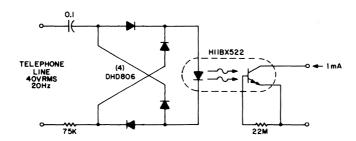


Fig. 108 - Low line loading ring detector.

Lower line current loading is required in many ring detector applications. This can be provided by using the H11B2 photodarlington optocoupler, which is specified to provide a 1mA output from a 0.5mA input. The following circuit allows ring detection down to a 40V RMS ring signal while providing 60Hz rejection to about 20V RMS. Zero crossing filtering may be accomplished either at the input bridge rectifier or at the output, similar to the method employed with the H11AA1 illustrated earlier. Dependable ring detection demands that the circuit respond only to ring signals, rejecting spurious noise

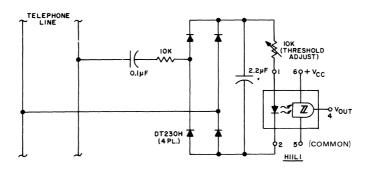


Fig. 109 - Ring detector using H11L1.

of similar amplitude, such as dialing transients. The configuration shown in Figure 109 relies on the fact that ring signals are composed of continuous frequency bursts, whereas dialing transients are much lower in repetition rate. The DC bridge-filter combination at the H11L input has a time constant such that it cannot react to widely spaced dialing transients, but will detect the presence of relatively long duration bursts, causing the H11L to activate the downstream interconnect circuits at a precisely defined threshold.

<u>Line Current Detection</u> — Detection of line current flow and indicating the flow to an electrically remote point is required in line status monitoring at a variety of points in the telephone system and auxiliary systems. The line should be minimally unbalanced or loaded by the monitor circuit, and relatively high levels of 60Hz induced voltages must be ignored. The H11AA1 allows line currents of either polarity to be sensed without discrimination and will ignore noise up to approximately 2.5mA.

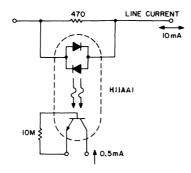


Fig. 110 - Polarity insensitive line current detector.

In applications where greater noise immunity or a polarity sensitive line current detection is required, the H11A10 threshold coupler may be used. This phototransistor coupler is specified to provide a minimum 10% current transfer ratio at a defined input current while having less than  $50\mu$ A leakage at half that input current — over the full -55°C to + 100°C temperature range. The input current range at which the coupler is "on" is programmable by a single resistor from 5mA to 10mA. Figure 111 illustrates a line current detector which indicates the polarity of line currents over 10mA while

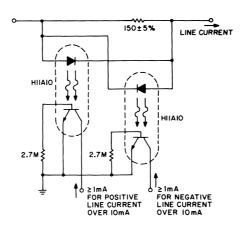


Fig. 111 - Polarity indicating line current detector.

ignoring line currents of less than 5mA. This circuit will maintain these margins over a -55°C to +100°C temperature range. At slightly more cost, the H11L1 may be used in this circuit to provide tighter threshold limits, hysterisis and digital output.

<u>Indicator Lamp Driver</u> — A simple "solid state relay" circuit provides a simple method of driving the 10V ac telephone indicator lamps from logic circuitry while maintaining complete isolation between the 10V line and the logic circuit.

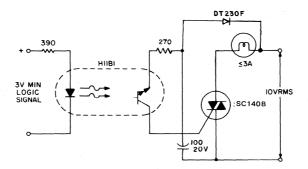


Fig. 112 - Isolated, logic controlled, indicator lamp switch.

Dial Pulse Indicator — A dial pulse indicator senses the switching on and off of the 48Vdc line voltage and transmits the pulses to logic circuitry. A H11A10 threshold coupler, with capacitor filtering, gives a simple circuit which can provide dial pulse indication yet reject high levels of induced 60Hz noise. The DHD805 provides reverse bias protection for the LED during transient over-voltage situations. The capacitive filtering removes less than 10msec of the leading edge of a 40V dial pulse, while providing rejection of up to 25V RMS at 60 Hz.

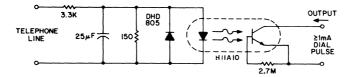


Fig. 113 - Dial pulse indicator.

<u>Digital Data Line Receiver</u> — When digital data is transmitted over long lines ( $\geq 1$  meter) proper transfer is often disturbed by the parasitic effects of ground level shifts and ground loops, as well as by extraneous noise picked up along the way. An optocoupler such as the H11L, combining galvanic isolation to minimize ground loop currents and their concomitant common mode voltages, with predictable switching levels to enhance noise immunity, can significantly reduce erratic behavior. Resistor R<sub>S</sub> is programmed for the desired switching threshold, C<sub>S</sub> is an (optional) speed-up capacitor, and CR1 is an LED used as a simple diode to provide perfect line balance and a discharge path for C<sub>S</sub> if the speed-up capacitor is used.

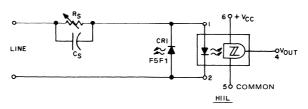


Fig. 114 - Digital data line receiver.

## **OPTOISOLATOR SWITCHING CIRCUITS**

The bilateral analog FET optocoupler can also be utilized as an isolated control analog switch, and will be illustrated in the next few examples. A series-parallel combination of the optocouplers can be utilized as an analog commutator. A FET high input impedance op-amp connected as a unity-gain follower is normally used as a buffer between the signal source and the load. The switch circuit can be viewed as part of a combination of two series-connected variable resistors in parallel with the input signal source. The input to the op-amp forms an equivalent voltage-divider network. If  $R_{on} = 3K\Omega$  and  $R_{\rm off} = 300 M\Omega$ , the variation of the voltage dividing ratio is from 0.00001 to 0.99999 which implies the error due to the opto-bilateral switches is about 0.001 %. Because the switching speed of the optocoupler bilateral switch (0% and 100% signal levels) is less than 50µsec, this analog commutator works accurately for repetition rates below 20KHz. For a 200mV dc input signal, the analog commutator has a rise time (0% to 99%) of about 5 $\mu$ sec and a fall time (99% to 0%) of about 4 $\mu$ sec. The rise time (acquisition time,  $\tau_A$ ) and fall time (recovery time,  $\tau_R$ ) of the commutator with a source impedance of  $3M\Omega$  is also a function of input voltage. For a specific input voltage, the inverse of  $(\tau_A + \tau_R)$  will determine the upper limit of the operating frequency range of the commutator, and approaches 50KHz at high input voltages. This technique allows a four-channel analog multiplexer to be constructed by adding three more input and control channels.

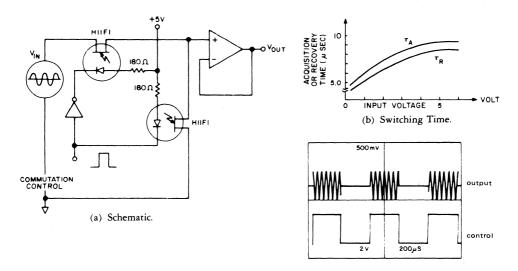


Fig. 115 - Analog commutator circuit.

The multiplexer allows selection of any of the four signal sources via the address selection and enable pulse. Switching transients have been observed during the transition of the control signal. These transients (about 500nsec) are much shorter than the acquisition time and recovery time (several micro-seconds), and do not affect the operation of the multiplexer. To illustrate the operation of the multiplexer, four different waveforms are fed into four input channels, then sequentially multiplexed. Different dc offset voltages are applied to each channel so that the signal associated with each channel can be clearly identified in the output waveform, as illustrated. The cross-talk between adjacent channels at various frequencies has been analyzed, and degrades about 20db per decade as frequency increases. With a 100kHz input signal, the adjacent channel rejection is about 62db, increasing to 100 db at 1kHz. This figure can be further reduced with careful circuit layout.

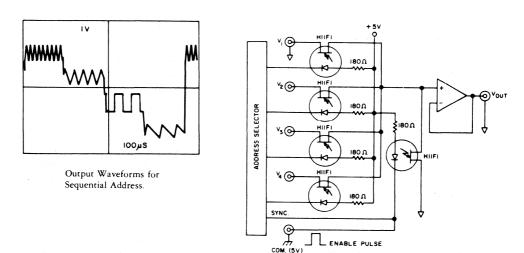


Fig. 116 - Four channel multiplexer.

Optically coupled isolators can replace transformers in a zero-voltage detector for synchronizing the firing of a thyristor in three-phase control applications. The optoisolators eliminate the need for a low-pass filter, required in standard detectors for eliminating spurious zero-crossings caused by the thyristor's switching transients. They provide high-voltage isolation and much lower capacitive coupling to the circuit than a standard transformer, approximating the coupling of double-shielded types.

The IRED's in the H11AA1 optoisolator are inserted in each of three legs of a delta network. During most of the cycle, all phototransistors are on. At times when the voltage between any two lines is within about 15V of zero, however, no current will flow through the IRED's connected across those lines. Therefore its corresponding phototransistor will be off, causing pin 2 of the 74LS221 one-shot to change states and a phase-identification pulse (P) to be generated twice every cycle.

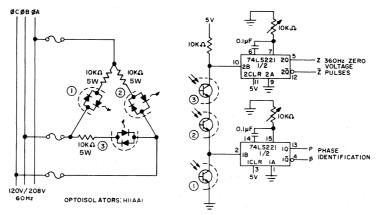


Fig. 117 - Three phase line synchronizer.

In the case illustrated, the phototransistors are wired so that a pulse will be generated at the output each time the input voltage, as measured across  $\phi_a$  and  $\phi_b$ , passes through zero. Note that the one-shot should be adjusted so that the trailing edge of the output pulse corresponds to the actual zero-crossing point.

Identification pulses are also generated for all three phases collectively and these can be accessed, if required, at the zero-voltage pulse output (Z). These pulses occur three times as often as P.

Because at least one IRED is conducting at any one time, no transient will normally be generated, so no low-pass filter is needed. Furthermore, the phototransistor's response of a few microseconds acts to suppress any transients that might occur near the zero-voltage points, thereby increasing the circuit's noise immunity.

#### **POWER CONTROL CIRCUITS**

The evolution of the optoelectronic coupler has made it practical to design a completely solid state relay. A solid state relay can perform not only the same functions as the original electro-mechanical relay, but can also provide solid state reliability, zero voltage switching and, most importantly, a direct interface between integrated circuit logic and power line.

## Solid State Relays (AC Output Modules)

A zero voltage switching design for ac solid state relays meets all the above criteria and is a combination of four individual functions. It consists first of an input circuit. The input terminals of this part of the relay are analogous to the coil of an EMR (electromechanical relay). It is effectively a resistive network and can be designed to accept a large range of input values. Circuits are designed to accept either digital or analog signals and to limit input current requirements to enable direct interfacing to logic circuits. The second part of a solid state relay consists of an isolation function performed by an optocoupler. A coupler provides, by means of a dielectric medium, an isolation path to transfer the input signal information to a third function; which is the zero voltage switching network. The ZVS network monitors the line voltage and controls the fourth (power) function, selecting the "on" or "off" state.

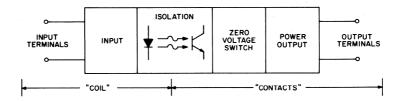


Fig. 118 - Solid state relay block diagram.

A reliable solid state relay design incorporates the correct choice of components and a careful consideration of the system to be interfaced. There are a variety of circuit configurations that are possible, each with its own advantages and disadvantages.

<u>Input (Coil) Circuits</u> — The first design consideration is the relay input (or coil) characteristics. It can be a simple current limiting resistor ( $\cong 330\Omega$  for TTL) in series with a light emitting diode, or it can be as complex as a Schmitt trigger circuit exhibiting hysteresis characteristics.

The input circuit should be designed around the available input signal. When working with logic signals, consider the complete capabilities of the gate output. A logic gate can operate in both the sinking or sourcing mode. Some MOS (or CMOS) circuits supply only about  $20\mu a$ , while TTL gates can offer up to 50ma in the sink mode and -1.6ma in the source mode. These are the input currents available to drive the solid state relay. In most circuits, the relays IRED will require 0.5mA to 20 mA of drive current at a minimum voltage of 1.5V (the drop across the diode) in order to achieve workable output currents in the detector device. The low level MOS logic signals normally indicate the need to use transistor buffer (or signal amplification) stages in the input circuit.

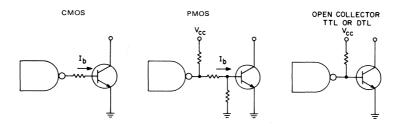


Fig. 119 - Connection of transistor buffers to logic circuits.

Generally, direct TTL connection to the optocoupler using SSI gates of the 54/74, 54H/74H and 54S/74S logic families, which guarantee  $V_0$  (0) (maximum) of 0.4V sinking  $\geq$  12mA, is made with the IRED ''on'' for a logic zero. For CMOS circuits the logic ''1'' output is the best means of operation, using an NPN transistor buffer. The buffer circuit in Figure 120 illustrates the advantage of a low saturation voltage, high gain transistor.

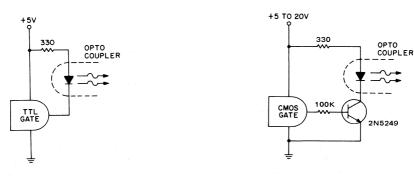


Fig. 120a - Direct connection of TTL  $I_0 \ge 7mA$ .

Fig. 120b - NPN buffered CMOS connection  $I_0 \ge 7mA$ .

In the case where analog signals are being used as the logic control, hysteresis, via a Schmitt trigger input, similar to the one in Figure 121, can be used to prevent "chatter" or half wave, power output. Circuit operation is as follows: at low input voltages  $Q_1$  is biased in the off state.  $Q_2$  conducts and biases  $Q_3$  and, thereby, the IRED off. When the base of  $Q_1$  reaches the biasing voltage of 0.6V-plus the drop across  $R_D$ ,  $Q_1$  turns on.  $Q_3$  is then supplied base drive, and the solid state relay input will be activated. The combination of  $Q_3$  and  $Q_4$  acts as a constant current source to the IRED. In order to turn-off  $Q_3$  base drive must be reduced to pull it out of saturation. Because  $Q_2$  is in the off-state as signal is reduced,  $Q_1$  will now stay "on" to a base bias voltage lower by the change in the drop across  $R_D$ . With these values, highest turn-off voltage is 1.0V, while turn "on" will be at less than 4.1V supplied to the circuit.

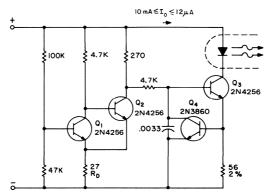


Fig. 121 - Hysteresis input circuit.

For ac or bi-polar input signals there are several possible connections. If only positive signals are to activate the relay, a diode (such as the A14) can be connected in parallel to protect the IRED from reverse voltage damage, since, its specified peak reverse voltage capability is approximately 3 volts. If ac signals are being used, or activation is to be polarity insensitive, a H11AA coupler which contains two LED's in antiparallel connection can be used.



Fig. 122 - H11AA1 ac input photon coupled isolator.

For higher input voltage designs, or for any easy means of converting a dc input relay to ac, a full wave diode bridge can be used to bias the IRED.

Isolation and Zero Voltage Switching Logic — Figure 123 presents two simple circuits providing zero voltage switching. These circuits can be used with full wave bridges or in antiparallel to provide full wave control and are normally used to trigger power thyristors. If an input signal is present during the time the ac voltage is between 0 to 7V, the SCR will turn-on. But, if the ac voltage has risen above this range and the input signal is then applied, the transistor,  $Q_1$ , will be biased to the "on" state and will hold the SCR and, consequently, the relay "off" until the next zero crossing.

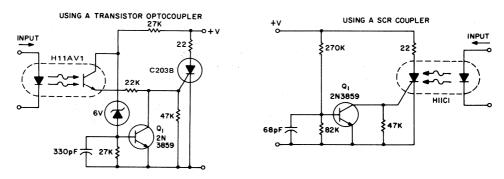


Fig. 123 - Normally open, two terminal, zero voltage switching half wave contact circuits.

The transistor circuit has excellent common mode noise rejection due to use of the H11AV1, which has under 0.5pf isolation capacitance. The SCR coupler circuit can be modified to provide higher sensitivity to input signals as illustrated below. This allows the lower cost 4N39 (H11C3) to be used with the  $\geq 7$ mA drive currents supplied by the illustrated input circuits.

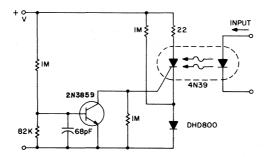


Fig. 124 - High sensitivity, normally open, two terminal, zero voltage switching, half wave contact circuit.

A normally closed contact circuit that provides zero voltage switching can also be designed around the 4N39 SCR optocoupler. The following circuit illustrates the method of modifying the normally open contact circuit by using the photoSCR to hold off the trigger SCR.

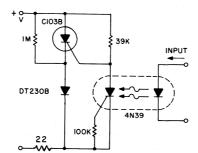
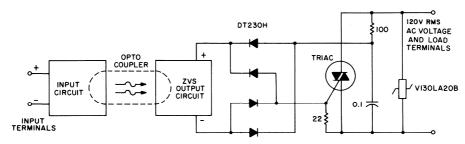


Fig. 125 - Normally closed, half wave ZVS contact circuit.

Integrated Solid State Relay Designs — A complete zero-voltage switch solid state relay contains an input circuit, an output circuit, and the power thyristor. The choice of specific circuits will depend on the designer's immediate needs. The circuit in Figure 126 can incorporate any of the previously described input and output circuits. It illustrates a triac power thyristor with snubber circuit and Harris MOV® Varistor transient over-voltage protection. The  $22\Omega$  resistor shunts di/dt currents, passing through the bridge diode capacitances, from the triac gate, while the  $100\Omega$  resistor limits surge and gate currents to safe levels. Although the circuits illustrated are for 120Vrms operation, relays that operate on 220V require higher voltage ratings on the MOV, rectifier diodes, triac and pilot SCR. The voltage divider that senses zero crossing must also be selected to minimize power dissipation in the transistor optoisolator circuit for 220V operation.



TRIAC TYPE MATCHED TO LOAD CURRENT REQUIREMENTS, SEE TABLE 17 AND 18.

Fig. 126 - Zero voltage switching solid state relay.

Higher line voltage may be used if the diode, varistor, ZVS and power thyristor ratings are at compatible levels. For applications beyond triac current ratings, antiparallel SCR's may be triggered by the ZVS network, as illustrated below.

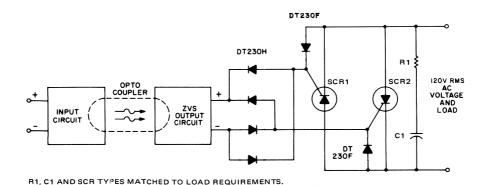
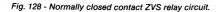


Fig. 127 - Zero voltage switching, solid state relay with antiparallel SCR output.

Other solid state ZVS circuits are available. Figure 128 is effective for lamp and heater loads. Some circuits driving reactive loads require integral cycle, zero voltage switching, i.e., an identical number of positive and negative half cycles of voltage are applied to the load during a power period. The circuit in Figure 129, although not strictly a relay due to the three terminal power connection, performs the integral cycle ZVS function when interfaced with the previous coil circuits.

# USING A SCR COUPLER INPUT CIRCUITS DHD 806 DHD 806



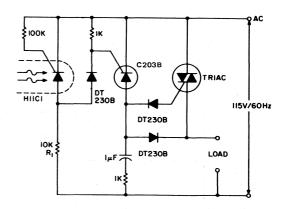


Fig. 129 - Normally closed integral cycle, zero voltage switching, contact circuit.

As an aid in determining the applicability of triacs to various jobs and in selection of the proper triac, a chart has been prepared giving the characteristics of common incandescent lamp and motor loads. These loads have high surge currents associated with them, which could complicate triac selection without this chart.

TABLE 15: TYPICAL INCANDESCENT IN-RUSH CURRENT RATINGS

WATTAGE	RATED VOLTS	TYPE	AMPS. STEADY STATE	HOT/COLD RESIST. RATIO	THEORETICAL PEAK IN-RUSH (170V pk) (Amps)	RATED (LUMENS /WATT)	HEATING TIME TO 90% LUMENS (Sec.)	LIFE RATED HOURS AVERG.	GENERAL ELECTRIC TRIAC SELECTION
25	120	Vacuum	0.21	13.5	4.05	10.6	.10	1000	SC141
60	120	Gas Filled	0.50	13.0	9.70	14.0	.10	1000	SC141/240
100	120	Gas Filled	0.83	14.3	17.3	17.5	.13	750	SC141/240
100(proj)	120	Gas Filled	0.87	15.5	19.4	19.5	.16	50	SC141/240
200	120	Gas Filled	1.67	16.0	40.5	18.4	.22	750	SC146/245
300	120	Gas Filled	2.50	15.8	55.0	19.2	.27	1000	SC146/245
500	120	Gas Filled	4.17	16.4	97.0	21.0	.38	1000	SC250/260
1000	120	Gas Filled	8.3	16.9	198.0	23.3	.67	1000	SC250/260
1000(proj)	120	Gas Filled	8.7	18.0	221.0	28.0	.85	50	SC250/260

For 240 volt lamps, wattage may be doubled.

TABLE 16: FULL-LOAD MOTOR-RUNNING AND LOCKED ROTOR CURRENTS IN AMPERES CORRESPONDING TO VARIOUS AC HORSEPOWER RATINGS

HODGE	110 -	- 120 V	OLTS	220	- 240	VOLTS	MTR. LOCK-RTR. CURRENT AMPS.			T AMPS.	G.E. TRIAC* SELECTION		
HORSE- POWER	Single- Phase	Two- Phase	Three- Phase	Single- Phase	Two- Phase	Three- Phase	Single 110-120	Phase 220-240	Two or Th 110-120	ree Phase 220-240	120V	240V	
1/10	3.0	_	_	1.5	_	_	18.0	9.0	_	_	SC141/240	SC141/240	
1/8 1/6	3.8 4.4	_	_	1.9 2.2	_	_	22.8 26.4	11.4 13.2	_	_	SC146/245 SC146/245		
1/4	5.8	_	_	2.9	_		31.8	17.4		_	SC250	SC141/240	
1/3 1/2	7.2 9.8	- 4.0	4.0	3.6 4.9	2.0	2.0	43.2 58.8	21.6 29.4	_ 24	12	SC260 SC265	SC146/245 SC260	

<sup>\*</sup>Assumes over-current protection has been built in to limit the duration of an locked-rotor condition. Source: Information for these charts was taken from National Electric Code, 1971 Edition.

Other AC Relay Designs — The "contact" circuitry can be simplified when zero voltage switching is not required. Several methods of providing this function are illustrated in Figures 130 and 131. Note that an SCR coupler in a bridge, using a high value of gate resistance connected directly across the ac line, can give commutating dv/dt and dv/dt triggering problems, which are not present in the ZVS circuits or at low voltages, and that not all these circuits are TTL drive compatible at the input.

The lowest parts count version of a solid state relay is an optoisolator, the triac driver H11J. Unfortunately, the ability of the H11J to drive a load on a 60Hz line is severely limited by its power dissipation and the dynamic characteristics of the detector. These limit applications to 30-50mA resistive loads on 120Vac, and slightly higher values at lower voltages.

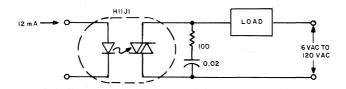


Fig. 130 - Simple "solid state ac relay."

This is compatible with neon lamp drive, pilot and indicator incandescent bulbs, low voltage control circuits, such as furnace and bell circuits (if dv/dt sufficient) — but less benign loads require a discrete triac.

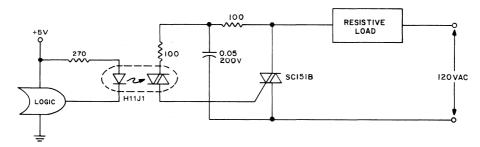


Fig. 131 - Minimum parts count isolated logic triggered triac.

The H11J1 triac trigger optocoupler potentially allows a simple power switching circuit utilizing only the triac, a resistor and the optocoupler. This configuration will be sensitive to high values of dv/dt and noise on normal power line voltages, leading to the need for the configuration shown in Figure 131, where the triac snubber acts as a filter for line voltage to the optocoupler. As the snubber is not usually used for resistive loads, the cost effectiveness of the circuit is compromised somewhat. Even with this disadvantage, the labor, board space, and inventory of parts savings of this circuit often prove it cost optimized for isolated logic control of power line switching. In applications where transient voltages on the power line are prevalent, provisions should be made to protect the H11J1 from break-over triggering.

If load current requirements are relatively low (i.e., maximum forward RMS current ≤ 500mA), an ac solid state relay can be constructed quite simply by the connection of two H11C optically coupled SCR's in a back-to-back configuration as illustrated in Figure 132.

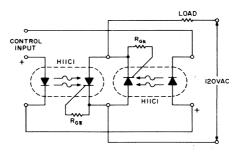


Fig. 132 - Using two photon couplers to provide a simple ac relay.

Where analog signals are being used as the logic control, hysteresis, via a Schmitt trigger input (illustrated in Figure 121) can be used to prevent "chatter" or half wave power output. Circuit operation is straightforward, and will not be described. This basic circuit can be easily modified to provide the latching relay function as illustrated below. Latching is obtained by the storage of gate trigger energy from the preceding half cycle in the capacitors. Power must be interrupted for more than one full cycle of the line to insure turn-off. Resistors R and capacitors C are chosen to minimize dissipation while assuring triggering of the respective SCRs each cycle.

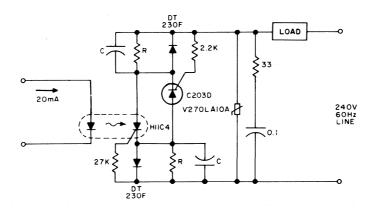


Fig. 133 - Latching ac solid state relay.

A pulse of current, over 10msec duration, into the H11C4 IRED, assures triggering the latching relay into conduction.

In microprocessor control of multiple loads, the minimum cost per load is critical. A typical application example is a large display involving driving arrays of incandescent lamps. This circuit provides minimal component cost per stage and optocoupler triggering of triac power switches from logic outputs. The minimal component cost is attained by using more complex software in the logic. A darlington output optocoupler provides gate current pulses to the triac, with cost advantages gained from eliminating the current limiting resistor and from the low cost coupler. The trigger current source is a dipped tantalum capacitor, charged from the line via a series resistor with coarse voltage regulation being provided by the darlington signal transistor. The resistor and capacitor are shared by all the darlington-triac pairs and are small in size and cost due to the low duty cycle of pulsing. Coupler IRED current pulses are supplied for the duration of one logic clock pulse  $(2-10\mu\text{sec})$ , at 0.4 to 1msec intervals, from a LED driver I.C.

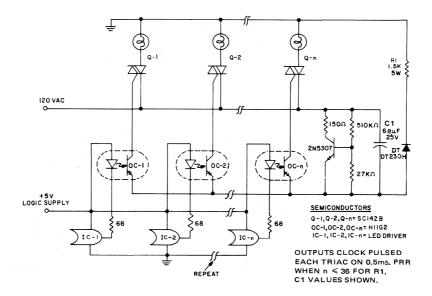


Fig. 134 - Microprocessor triac array driver.

The pulse timing is derived from the clock waveform when the logic system requires triac conduction. A current limiting resistor is not used, which prevents Miller effect slowdown of the H11G2 switching speed to the extent the triac is supplied insufficient current to trigger. Optodarlington power dissipation is controlled by the low duty cycle and the capacitor supply characteristics.

<u>High Voltage AC Switching</u> — A basic circuit to trigger an SCR is shown in Figure 135. This circuit has the disadvantage that blocking voltage of the photon coupler output device determines the circuit blocking voltage, irrespective of higher main SCR capability.

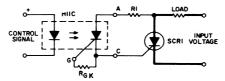


Fig. 135 - Circuit to trigger an SCR.

Adding a capacitor  $(C_1)$  to the circuit, as shown in Figure 136 will reduce the dv/dt seen by the photon coupler output device. The energy stored in  $C_1$ , when discharged into the gate of  $SCR_1$ , will improve the di/dt capability of the main SCR.

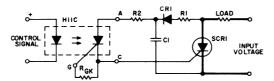
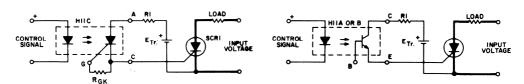


Fig 136 - Deriving the energy to trigger an SCR from its anode supply with an energy storing feature.

Using a separate power supply for the coupler gives added flexibility to the trigger circuit; it removes the limitation of the blocking voltage capability of the photon coupler output device. The flexibility adds cost. Also, more than one power supply may be necessary for multiple SCR's if no common reference points are available.



Photon Coupler With SCR - Output

**Photon Coupler With Transistor Output** 

Fig. 137 - Photon coupler triggering main SCR<sub>1</sub> using separate power supply.

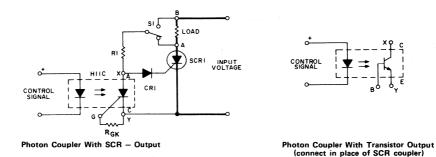


Fig. 138 - Normally closed configurations.

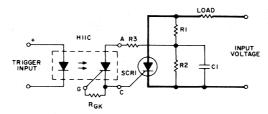


Fig. 139 - Triggering SCR with photon coupler and supply voltage divider.

In Figure 138,  $R_1$  can be connected to Point A, which will remove the voltage from the coupler after  $SCR_1$  is triggered, or to Point B so that the coupler output will always be biased by input voltage. The former is preferred since it decreases the power dissipation in  $R_1$ . A more practical form of SCR triggering is shown in Figure 140. Trigger energy is obtained from the anode supply and stored in  $C_1$ . Coupler voltage is limited by the zener voltage. This approach permits switching of higher voltages than the blocking voltage capability of the output device of the photon coupler. To reduce the power losses in  $R_1$  and to obtain shorter time constants for charging  $C_1$ , the zener diode is used instead of a resistor.

A guide for selecting the component values would consist of the following steps:

- 1) Choose  $C_1$  in a range of 0.05 to 1 microfarad. The maximum value may be limited by the recharging time constant  $(R_L + R_1) C_1$  while the minimum value will be set by the minimum pulse width required to ensure SCR latching.
- 2) R<sub>2</sub> is determined from peak gate current limits (if applicable) and minimum pulse width requirements.

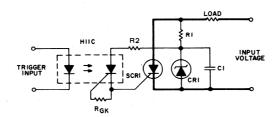


Fig. 140 - Triggering SCR with photon coupler with low voltage reference.

- 3) Select a zener diode. A 25 volt zener is a practical value since this will meet the usual gate requirement of 20 volts and 20 ohms. This will also eliminate spurious triggering due to voltage transients.
- 4) Photon coupler triggering is ideal for SCR's driving inductive loads. By ensuring that the LASCR latches on, it can supply gate current to SCR<sub>1</sub> until it stays on. The following table lists values for R<sub>1</sub> and R<sub>2</sub> along with their power dissipation when the SCR is off for different values of I<sub>GT</sub> and applied ac voltage.
- 5) Component values for dc voltage are easily computed from the following formulae:

$$R_1 = \frac{E_{IN} - V_Z}{I_G}$$
 Where: 
$$V_Z = \text{zener voltage}$$
 
$$P_{(R_1)} = I_G \cdot (E_{IN} - V_Z)$$
 
$$P_{(\text{zener})} = I_G \cdot V_Z$$

TABLE 17: COMPONENT VALUES AND POWER DISSIPATION ASSUMING 25V ZENER DIODE,  $50/60~\mathrm{Hz}$  AC LINE VOLTAGES

EIN(RMS)	IGT	R <sub>1</sub>	P(R1)	R <sub>2</sub>	P <sub>(R2)</sub>	P <sub>(zener)</sub>
380	50	3500	17.4	560	.5	1.1
	100	2000	34.8	330	1.0	2.2
	150	1200	52.2	220	1.5	3.4
	200	1000	69.6	150	2.0	4.5
	300	600	105.0	100	3.0	6.7
440	50	4250	20.5	560	.5	1.1
	100	2100	41.0	330	1.0	2.2
	150	1500	62.0	220	1.5	3.4
	200	1000	82.0	150	2.1	4.5
	300	750	125.0	100	3.1	6.7
600	50	5800	29.0	560	1.1	1.1
	100	3000	58.0	270	1.6	2.2
	150	2000	86.0	200	2.1	3.4
	200	1500	115.0	150	2.7	4.5
	300	1000	175.0	100	3.2	6.7

The following circuit utilizes the principle for triggering SCR's connected in series. A snubber circuit R2C2 as shown may be necessary since R1 and C1 are tailored to obtain optimized triggering and not for dv/dt protection.

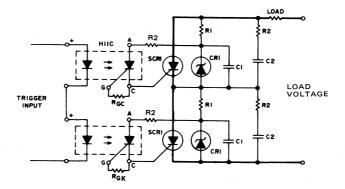


Fig. 141 - High voltage switch.

A photon coupler with a transistor output will limit the trigger pulse amplitude and rise time due to CTR and saturation effects. Using the H11C1, the rise time of the input pulse to the photon coupler is not critical, and its amplitude is limited only by the H11C1 turn-on sensitivity.

All the applications shown so far have the load connected to the anode, but the load can be connected to the cathode, illustrated in Figure 142.

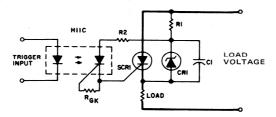


Fig. 142 - Connection of load to cathode of main SCR.

<u>Three Phase Circuits</u> — Everything mentioned about single phase relays or single phase switching or triggering with photon couplers applies also to three phase systems.

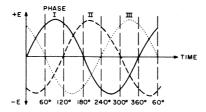


Fig. 143 - Voltage waveform in three phase systems.

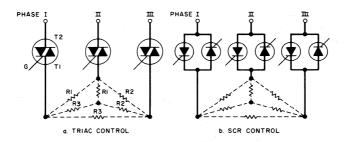


Fig. 144 - Y-OR Δ- connected resistive or inductive load.

Figures 143 and 144 illustrate voltage waveforms in a three phase system which would appear on the triac MT-2 terminal before triggering and at the MT-1 terminal after triggering. The use of the H11C to isolate the trigger circuitry from the power semiconductor will simplify the trigger circuitry significantly. In some cases the GE3020 series triac driver will allow further circuit simplification, if dynamic and transient effects are compatible.

Following are three phase switches for low voltage. Higher currents can be obtained by using inverse parallel SCR's which would be triggered as shown. For higher voltages and higher currents, the circuits of the previous page can be useful in three phase circuits.

To simplify the following schematics and facilitate easy understanding of the principles involved, the following schematic substitution is used (Note the triac driver is of limited use at  $3\phi$  voltage levels):

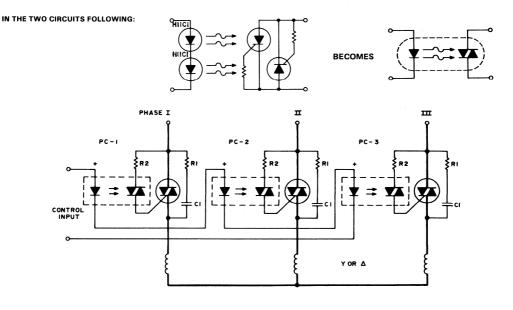


Fig. 145 - Three phase switch for inductive load.

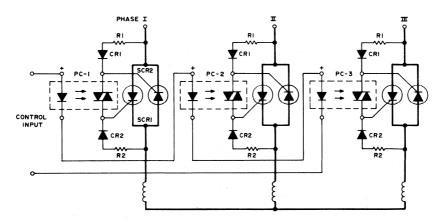


Fig. 146 - Three phase switch with inverse parallel SCR's for inductive load and Y or ∆ connections.

Many other ac power control circuits are practical and cost effective. The intent of this section was to stimulate the circuit designer by presenting a variety of circuits featuring opto control.

#### DC Solid State Relay Circuits

The dc relay built around an optocoupler is neither a relay nor strictly dc. This section will describe relay function circuits that did not fit the ac solid state relay 60Hz power line switching function, as well as strictly dc switching.

<u>DC Latching Relay</u> — The H11C readily supplies the dc latching relay function and reverse polarity blocking, for currents up to 300mA (depending on ambient temperature). For dc use, the gate cathode resistor may be supplemented by a capacitor to minimize transient and dv/dt sensitivity. For pulsating dc operation, the capacitor value must be designated to either retrigger the SCR at the application of the next pulse or prevent retriggering at the next power pulse. If not, random or undesired

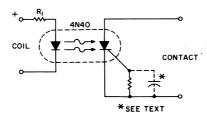
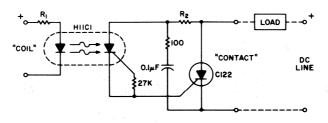


Fig. 147 - DC latching relay circuit.

operation may occur. For higher current contacts, the H11C may be used to trigger an SCR capable of handling the current, as illustrated in Figure 148.



COIL VOLTAGE	6	12	24	48	120	V
RI VALUE	470	1.1K	2.4K	4.7K	12K	Ω

LINE VOLTAG	E 12	24	48	120	V
C122 PART	U	F	A	В	D
R2 VALUE	200	470	1 K	2.2K	Ω

12 A

15 A

NO HEAT SINK RATINGS AT $T_A \leqslant 50^\circ$				
I CONTACT, MAX.	PULSE WIDTH	DUTY CYCLE		
0.67 A	D.C.	100%		
4.0 A	160 msec.	12%		
8.0 A	160 msec.	3%		

160 msec.

160 msec.

FOR HEAT SINK RATINGS SEE CI22 SPECIFICATION SHEET NUMBER 150.35 AND APPLICATION NOTE NUMBER 200.55

Fig. 148 - High current dc latching relay.

1%

0.3%

Heat sinking on this, and all high current designs, must be designed for the load current and temperature environment.

The phototransistor and photodarlington couplers act as dc relays in saturated switching, at currents up to 5mA and 50mA, respectively. This is illustrated by the H11A5 application as a high speed synchronous relay in the long range object detector shown in Figure 87. When higher currents or higher voltage capabilities are required, additional devices are required to buffer or amplify the photocoupler output. The addition of hysteresis to provide fast switching and stable pick up and drop out points can also be easily implemented simultaneously. Illustrated below are normally open and

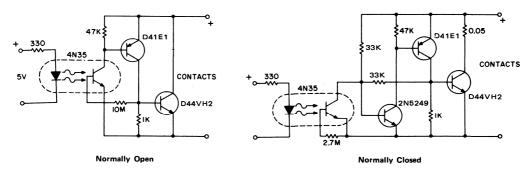


Fig. 149 - 10A, 25Vdc solid state relays.

normally closed dc solid state relays. These circuits provide several approaches to implement the dc relay function and are intended to stimulate the creativity of other circuit designers, and serve as practical, cost effective examples.

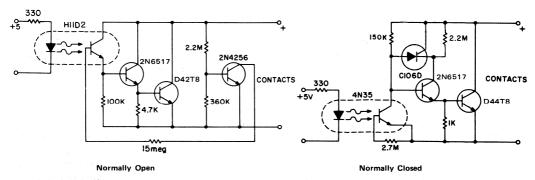


Fig. 150 - 0.25A, 300Vdc solid state relay.

#### Other Power Control Circuits

Many forms of power control circuitry using optoelectronics do not fit the definition of a relay, although optoelectronics is beneficial to their operation.

<u>Electric Vehicle Battery Saver</u> — The battery life, and therefore operating cost, of an electric vehicle is severely affected by overdischarge of the battery. This circuit provides both warning and shutdown. An electronic switch is placed in series with the propulsion motor contactor coil. Three modes of operation are possible:

- 1) When the propulsion power pack voltage is above the 63V trip point the electronic switch has no effect on operation;
- 2) When the propulsion power pack no load voltage is below 63V, power will not be supplied to the propulsion motor since the electronic switch will prevent contactor operation;
- 3) When the propulsion power pack loaded voltage drops below 63V the contactor will close and open due to the electronic switch. This "bucking" operation indicates to the operator need to charge the batteries.

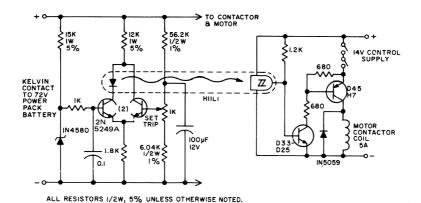


Fig. 151 - Electric vehicle battery saver.

20 kHz Arc Welding Inverter (Full Power Modulation and No-Load Shutdown) — The Class A series resonant inverter portrayed in Figure 152 is well-known and respected for its high efficiency, low cost, and small size, provided that operating frequency is greater than about 3kHz. The disadvantages are (at least in high power versions) the difficulty in effecting smooth RFI-less output voltage modulation without significant added complexity, and a natural tendency to "run away" under no-load (high Q) conditions. The 20kHz control circuit depicted in Figure 153 overcomes these shortcomings by feeding back into the asymmetrical thyristor trigger pulse generators (Figure 154 signals that simultaneously shut the inverter down, when its output voltage exceeds a preset threshold, and time-ratio modulates the output. This feedback is accomplished with full galvanic isolation between input and output thanks to an H11L opto Schmitt coupler. The fundamental 20kHz gate firing pulses are generated by a PUT relaxation oscillator  $Q_1$ . The pulses are then amplified by transistors  $Q_2$  and  $Q_3$ . The 20 kHz sinusoidal load current flowing in the primary of the output transformer is then detected by a current transformer CT1, with operational amplifier A1 converting the sine wave into a square wave whose transitions coincide with the load current zero points. Consequently, each time the output current changes, phase A1 also changes state and, via transistor Q4, either connects the thyristor gate to a minus 8Vdc supply (for minimum "gate assisted" turn-off time and highest reapplied dV/dt capability) or

disables this supply to prepare the thyristor for subsequent firing.

Because firing always occurs at a fixed time interval (determined by the PUT time constant R1  $\times$  C1) after each load current zero point, the circuit operating frequency always coincides with the natural resonant frequency, the fixed time interval being chosen to equal thyristor turn-off time,  $t_q$ . Note that reliable PUT oscillation is guaranteed by turning it off solidly via  $Q_5$  each time  $Q_4$  reapplies negative bias to the thyristor gate. The H11L opto Schmitt is connected in parallel with  $Q_5$ . If the load is removed (termination of a weld), causing the inverter output voltage to rise precipitously, the V56MA varistor will conduct to energize the H11L input diode, and the H11L output stage will likewise clamp off the PUT. Oscillation then ceases until the output voltage falls once again below the off threshold voltage of the H11L.

Modulation intelligence is coupled into this same H11L through two additional PUT's,  $Q_6$  and  $Q_7$   $Q_6$  oscillates at a fixed 1.25kHz, which establishes the modulation frequency. Duty cycle is determined by a second oscillator,  $Q_7$ , whose conduction state (on or off) establishes or removes current from the H11L diode. With a 20kHz fundamental inverter frequency and a modulation frequency of 1.25kHz, the resultant time ratio controlled power output is given by

$$P_{OUT} = \left(P_{M} \times \frac{t}{\tau}\right)$$

where  $P_M = 100\%$  continuous output power. Minimum power is one cycle of 20kHz ( $50\mu s$ ) in the 1.25kHz modulation frame ( $800\mu s$ ), that is, 6.25%  $P_M$ .

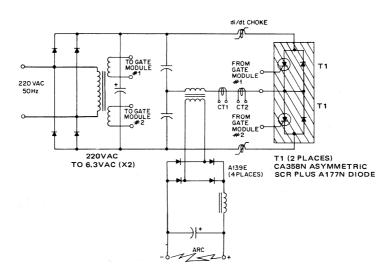


Fig. 152 - Class "A" - 3kW welding inverter.

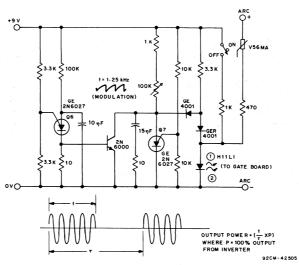


Fig. 153 - Power modulator (with on-off switch & open circuit protection)

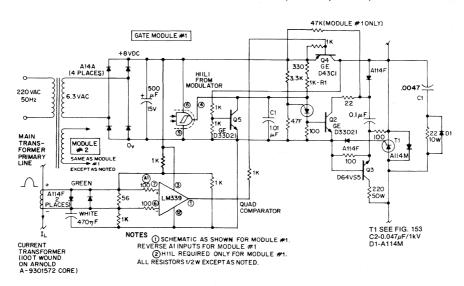


Fig. 154 - 20kHz inverter gate drive module.

Glow Plug Driver —Model airplanes, boats, and cars use glow plug ignitions for their miniature (0.8cc - 15cc) internal combustion engines. Such engines dispense with the heavy on-board batteries, H.T. coil, and "condenser" required for conventional spark ignition, while simultaneously developing much higher RPM (hence power) than the compression ignition (diesel) motors. The heart of a glow plug is a platinum alloy coil heated to incandescence for engine starting by an external battery, either 1.5 Volts or 2 Volts. Supplementing this battery, a second 12 Volt power supply is frequently required for the engine starter, together with a third 6 Volt type for the electrical fuel pump.

Rather than being burdened by all these multiple energy sources, the model builder would prefer to carry (and buy) a single 12 Volt battery, deriving the lower voltages from this by use of suitable electronic step-down transformers (choppers). The glow driver illustrated in Figure 155 does this and offers the additional benefit of (through negative feedback) maintaining constant plug termperature independent of engine flooding, or battery voltage while the starter is cranking.

In this circuit, the PUT relaxation oscillator  $Q_1$  turns on the output chopper transistor  $Q_2$  at a fixed repetition rate determined by R1 and C1. Current then flows through the glow plug and the parallel combination of the current sense resistor R2 and the LED associated with the H11L Schmitt trigger. With the plug cold (low resistance), current is high, the H11L is biased "on," and  $Q_3$  conducts to sustain base drive to  $Q_2$ . Once the plug has attained optimum operating temperature, which can be monitored by its ohmic resistance, the H11L is programmed (via  $R_p$ ) to switch off, removing base drive from  $Q_3$  and  $Q_2$ .

However, since the H11L senses glow plug current, not resistance, this is only valid if supply voltage is constant, which is not always the case. Transistor  $Q_4$  provides suitable compensation in this case; if battery voltage falls (during cold cranking, for instance), the collector current of  $Q_4$  rises, causing additional current to flow through the LED, thus delaying the switch-off point for a given plug current. The circuit holds plug temperature relatively constant, with the plug either completely dry or thoroughly "wet," over an input voltage range of 8 to 16 Volts. A similar configuration can be employed to maintain constant temperature for a full size truck diesel glow plug (28 Volts supply, 12 Volts glow plug); in this case, since plug temperature excursions are not so great, a hysteresis expansion resistor  $R_{\rm H}$  may be required.

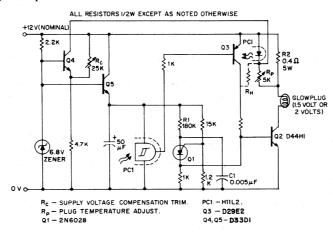


Fig. 155 - Glow plug driver.

Switching Power Supply with Optocoupler Isolated Constant Voltage Feedback — By virtue of its PNPN structure, which is that of a thyristor, the output stage of an H11C photo thyristor coupler may also be connected as a bilateral (symmetrical) PNP or as a unilateral (conventional) PNP transistor. Some suggested uses of the device in the former mode are outlined in the opening chapters of this Manual. Often overlooked, however, is the fact that ordinary PNP transistor optocouplers are rare and that concomitantly the H11C photo thyristor coupler can fill this function in sockets demanding PNP logic. Such a situation is illustrated in Figure 156, a low voltage high current output, switching dc power supply is running off the 220 Volt ac input. In this circuit, an ST2 diac relaxation oscillator ( $Q_3$ , C1, and the diac) initiates conduction of the output switching transistor  $Q_1$ , the on-time of which is maintained constant by a separate timing/commutation network consisting of  $Q_2$ , C2, the SUS and SCR 1. Output voltage, consequently, is dependent on duty cycle. To compensate for unwanted variations of output voltage due to input voltage or load resistance fluctuations, an H11C wired as a linear-mode

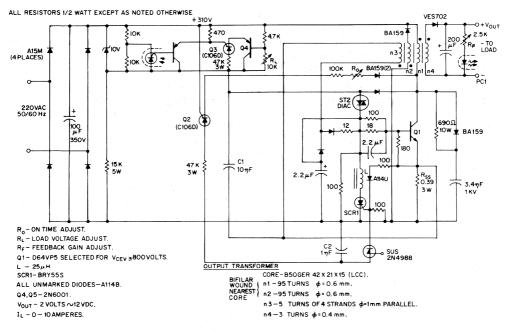


Fig. 156 - 12V switching power supply.

unilateral PNP transistor in a stable differential amplifier configuration is connected into the galvanically isolated negative feedback loop that determines duty cycle, hence output voltage. Of further interest, in this circuit, is the use of several low current, high voltage (400 Volt  $V_{DRM}$ ) thyristors ( $Q_2,\,Q_3$ ) also used as PNP remote base transistors. Short-circuit protection is assured by coupling  $Q_1$  collector current feedback into the turn-off circuitry via  $R_{SS}$ .

Low Power ( $P_{OUT} \ge 50$  Watts from 220 Volts AC Input) Zero Voltage Switch Temperature Controller—The "zero voltage switching" technique is widely used to modulate heating and similar types of ac loads where the time constant associated with the load (tens of seconds to minutes) is sufficiently long to allow smooth proportional modulation by time ratio control, using one complete cycle of the ac input voltage as the minimum switching movement. This method of control, illustrated in Figure 157, reduces Radio Frequency Interference (inherent in competing phase-control systems) significantly. Despite its attractions, the traditional triac-based ZVS is virtually unusable for the control of very low power loads, especially from 220 Volt ac inputs due to the triac's reluctance to latch-on into the near-zero instantaneous currents that flow through it and the load near the ac voltage zero crossover points. The circuit of Figure 158 side-steps the latching problem by employing a pair of very sensitive low current reverse blocking thyristors (C106) connected in antiparallel; these are triggered by a simple thermistor modulated differential amplifer  $(Q_1, Q_2)$ , with zero voltage logic furnished by an H11AA1 ac input optocoupler. With the NTC thermistor TH calling for heat, transistor  $Q_1$  is cut off and  $Q_2$  is on, which would normally provide continuous base drive to  $Q_3$ , with consequent triggering of either SCR, or of SCR 2 via SCR 1, depending on phasing of the ac input.

Note that when the ac input voltage is positive with respect to SCR 2, SCR 1 is reverse biased and, in the presence of "gate" current from  $Q_3$ , behaves as a remote base transistor, whose output provides via blocking diode CR1, positive gate trigger current for SCR 2. When the ac input polarity is reversed (SCR 1's anode positive), SCR 1 behaves as a direct fired conventional thyristor. "Trigger" current to SCR1, however, is not continuous, even when TH is calling for heat and  $Q_2$  is delivering base current to  $Q_3$ . In this situation,  $Q_3$  is inhibited from conduction by the clamping action of PC1, an H11AA

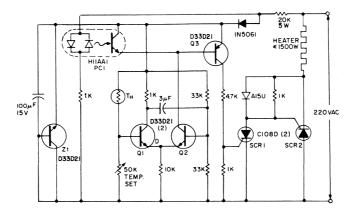


Fig. 157 - Low power (>50W) ZVS proportional temperature controller.

photocoupler, except during those brief instants when the ac input voltage is near zero and the coupler input diodes are deprived of current.

Through these means, triggering of either SCR can occur only at ac voltage crossing points, and RFI-less operation results. The proportional control feature is injected via the positive feedback action of capacitor  $C_M$ , which converts the differential amplifier  $Q_1,\,Q_2$  into a simple multivibrator, whose duty cycle varies from one to 99 percent according to the resistance of TH. Zener diode Z1 is optional, being preferred when maximum immunity from ac voltage induced temperature drift is desired.

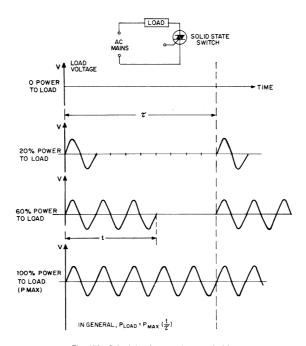


Fig. 158 - Principle of zero voltage switching.

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# **Glossary of Symbols and Terms**

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# **GLOSSARY OF SYMBOLS AND TERMS**

Optoelectronics spans the disciplines of electronics, photometry, radiometry and optics with dashes of physics and statistical analysis. The same word or symbol can have two different meanings, depending on the discipline involved. To simplify use of this glossary, words and symbols are separately listed, alphabetically; following each is the common discipline of usage and then the definition, as used in this Handbook.

#### **OPTOELECTRONIC SYMBOLS**

A	— electronic	— gain of an amplifier.
A	— optic	— area.
A	— reliability	<ul> <li>acceleration factor, describes change in a predicted basic phenomena response due to secondary conditions denoted by subscript.</li> </ul>
$\mathbf{\hat{A}}_{_{\mathbf{c}}}$		— Angstrom, a unit of wavelength equal to 10 <sup>-10</sup> meters. Archaic.
$\mathbf{B}_{\mathbf{L}}$	— photometric	<ul> <li>luminous intensity of an area light source, usually expressed in candela/unit area.</li> </ul>
$\mathbf{B_r}$	— radiometric	<ul> <li>radiant intensity of an area source, Radiance, usually expressed in Watts/unit area.</li> </ul>
β	<ul><li>electronic</li></ul>	— Beta, current gain of a transistor. See h <sub>FE</sub> .
C	— electronic	<ul> <li>inter-element capacitance, primarily junction capacitance, of a component. Terminals indicated by subscripts.</li> </ul>
C.T.	— photometric	<ul> <li>Color Temperature. The temperature of a black body, when its color best approximates the designated source. Normally used for lamps, and determined at .45 and .65 microns.</li> </ul>
CTR	— electronic	<ul> <li>Current Transfer Ratio. The ratio of output current to input current, at a specified bias, of an optocoupler. Usually in percent.</li> </ul>
DIP	— electronic	<ul> <li>Dual In-Line Package. Standard integrated circuit and optocoupler flat package with two rows of terminals on opposite sides. May be plastic or ceramic bodied.</li> </ul>
di/dt	— electronic	<ul> <li>Critical rate-of-rise of current rating of a thyristor. Higher rates may cause current crowding and device damage.</li> </ul>
dv/dt	— electronic	<ul> <li>Critical rate-of-rise of voltage parameter of a thyristor. Higher rates may cause device turn-on via junction capacitance charging currents providing gate signal.</li> </ul>
E	— photometric	<ul> <li>Illumination. Luminous flux density incident on a receiver, usually in lumens per unit of surface.</li> </ul>
$\mathbf{E_e}$		— Irradiance. See H.
<i>f</i> /#	— optic	<ul> <li>Lens parameter. The ratio of focal length to lens diameter.</li> </ul>
F	— optic	<ul> <li>Focal length of a lens or lens system.</li> </ul>
F	— photometric	— Illumination. Total luminous flux incidents on a receiver, normally in lumens. $F = \int E \cdot dA$ .
GaAs	— electronic	<ul> <li>Gallium Arsenide. The crystalline compound which forms IRED's when suitably doped.</li> </ul>
GaAlAs	— electronic	<ul> <li>Gallium Aluminum Arsenide. Another crystalline compound used to form both IRED's and LED's.</li> </ul>

Н	— radiometric	— Irradiance. Radiant flux density incident on a receiver, usually in Watts per unit area. $E_{\rm e}$ also used.
$\mathbf{H}_{\mathbf{E}}$	— radiometric	<ul> <li>Effective irradiance. The irradiance perceived by a given receiver, usually in effective Watts per unit area.</li> </ul>
$\mathbf{h}_{\mathrm{FE}}$	— electronic	<ul> <li>Current gain of a transistor biased common emitter. The ratio of collector current to base current at specified bias conditions.</li> </ul>
HTRB	— reliability	- High temperature reverse bias operating life test.
$I_A$	— electronic	- Thyristor or diode anode current, I <sub>TM</sub> is preferred terminology
_ <b>_A</b>		for thyristors.
$I_B$	— electronic	— Transistor base current.
$\mathbf{I_C}$	— electronic	— Transistor collector current.
I <sub>CB(on)</sub>	— electronic	- Utilized for phototransistors and photodarlingtons to denote
-CB(0ff)		photodiode current in the illuminated condition. This provides differentiation from both photodiode plus amplifier illuminated current and offstate leakage current.
T	— electronic	<ul> <li>Dark current. The leakage current of an unilluminated</li> </ul>
$\mathbf{I}_{\mathbf{D}}$	- electronic	photodetector.
$\mathbf{I_E}$	<ul><li>electronic</li></ul>	— Transistor emitter current.
$\mathbf{I_F}$	<ul><li>electronic</li></ul>	- Forward bias current, usually of IRED. Additional subscript
<b>I</b> L	— electronic	<ul> <li>denotes measurement of stress bias condition, if required.</li> <li>Light current. The current through an illuminated photodetector at specified bias conditions.</li> </ul>
$\mathbf{I}_{\mathbf{L}}$	— photometric	<ul> <li>Luminous intensity of a point source of light, normally in candela.</li> </ul>
IR	— radiometric	<ul> <li>Infrared. Radiation of too great a wavelength to be normally perceived by the eye. Radiation between 0.78 and 100</li> </ul>
		microns wavelength.
IRED	— electronic	<ul> <li>Infrared emitting diode. A diode which emits infrared radiation when forward bias current flows through it.</li> </ul>
L	— photometric	<ul> <li>Luminance of an area source of light, usually in lumens per unit area.</li> </ul>
LASCR	— electronic	<ul> <li>Light activated silicon control rectifier. Also photo SCR.</li> </ul>
LED	<ul><li>electronic</li></ul>	<ul> <li>Light emitting diode.</li> </ul>
<b>\( \hat{\lambda} \)</b>	— electronic	<ul> <li>Predicted failure rate of an electronic component subjected to specific stress and confidence limit.</li> </ul>
$\lambda$	— radiometric	— Wavelength of radiation.
m	— optics	- Magnification of a lens. Ratio of image size to source size.
m	<ul><li>physics</li></ul>	- Meter, international standard unit of length.
MSCP	— photometric	<ul> <li>Mean spherical candle power. Average luminous power output, of a source, per sterradian.</li> </ul>
n.a.	— optics	— Numerical aperture of a lens. n.a. = $2f/\#$ .
$\eta$	— radiometric	<ul> <li>Conversion efficiency of an electrically powered source. The ratio of radiant power output to electrical power input.</li> </ul>
OPA	— quality	<ul> <li>Outgoing process average of portion defects shipped, usually expressed in parts per million. It is derived from the sampling data and the lot acceptance rates.</li> </ul>
		and the second s

P	— radiometric	- Power, total flux in Watts.
$P_{D}$	— electronic	— Power dissipated as heat.
PPM	— quality	- Fraction of defectives observed expressed in parts per million.
	†	Equal to number defective times one million divided by
		number inspected. For zero defects a statistically derived
100		factor is used to estimate the defect density.
PPS	— electronic	<ul> <li>Repetition rate in pulses per second.</li> </ul>
PRM	— electronic	<ul> <li>Pulse rate modulation, coding an analog signal on a train of</li> </ul>
	creeti ome	pulses by varying the time between pulses.
PUT	— electronic	<ul> <li>Programmable Unijunction Transistor. A thyristor specified</li> </ul>
101	— electronic	to provide the unijunction transistor function.
Si	— electronic	
31	— electronic	— Silicon. The semiconductor material which is selectively
		doped to make photodiodes, phototransistors, photo- darlington and photoSCR detectors.
SCR	— electronic	
SCK	— electronic	<ul> <li>Silicon Controlled Rectifier. A thryistor, reverse blocking, which can block or conduct in forward bias, conduction</li> </ul>
		between anode and cathode being initiated by forward bias of
		the gate-cathode junction.
$T_{\mathbf{A}}$	— electronic	- Ambient temperature.
		•
$\mathbf{T_{C}}$	— electronic	<ul> <li>Case temperature, the temperature of a specified point on a component.</li> </ul>
$\mathbf{T}_{\mathbf{J}}$	— electronic	- Junction temperature, the temperature of the chip of a
•		semiconductor device. This is the factor which determines
		maximum power dissipation.
t	— electronic	- Time. Subscripts indicate switching times (d-delay, f-fall,
		r—rise and s—storage), intervals in reliability prediction
		(o—operating, x—equivalent operating), etc.
UCL	— reliability	- Upper confidence level. A statistical determination of the
		confidence of a prediction of the highest level of an
		occurrence based on the apercent of occurrences in a quantity
		from a homogeneous population.
UJT	<ul><li>electronic</li></ul>	- Unijunction transistor. A three-terminal, voltage threshold
		semiconductor device commonly used for oscillators and time
		delays.
V	<ul><li>electronic</li></ul>	- Voltage. Subscripts indicate the terminals which the voltage is
		measured across, the first subscript commonly denoting the
		positive terminal.
$\mathbf{W}$	<ul> <li>radiometric</li> </ul>	- Radiant emittance. The flux density, in Watts/unit area,
		emitted by the surface source.

#### OPTOELECTRONIC TERMS

Acceleration Factor	<ul> <li>reliability — a factor which describes the change in a predicted phenomena caused by a secondary effect.</li> </ul>
Angstrom Unit	<b>- radiometric</b> $-10^{-10}$ meters, obsolete term used to describe wavelength of radiation.
Anode	<ul> <li>electronic — the main terminal, of a device, which is normally biased positive. See cathode.</li> </ul>

Bandgap	— electronic	<ul> <li>the potential difference between the atomic valence and conduction bands. This determines the forward voltage drop and frequency of light output of a diode.</li> </ul>
Base	<ul><li>electronic</li></ul>	— the control terminal of a transistor.
Beta	— electronic	<ul> <li>common emitter current gain of a transistor. Collector current divided by base current.</li> </ul>
Bias	— electronic	— the electrical conditions of component operation or test.
Black Body	<ul> <li>radiometric</li> </ul>	— a body which reflects no radiation. Its radiation spectrum is a
. •		simple function of its temperature.
Candela	— photometric	<ul> <li>unit of luminous intensity, defined by 1/60 cm<sup>2</sup> of a black body at 2042°K.</li> </ul>
Cathode	— electronic	- the main terminal, of a device, which is normally biased
Cathout	ciecti ome	negative. See anode.
Chatter	— electronic	<ul> <li>a rapid, normally undesired, oscillation of relay contacts between the open and closed state.</li> </ul>
Collector	— electronic	<ul> <li>the main terminal of a transistor in which current flow is normally relatively independent of voltage bias.</li> </ul>
Color Temperature	— photometric	<ul> <li>the temperature of a black body when its color best approximates the designated source. Normally used for lamps and determined at .45 and .65 microns.</li> </ul>
Commutating dv/dt	— electronic	<ul> <li>a measure of the ability of a triac to block a rapidly rising voltage immediately after conduction of the opposite polarity.</li> </ul>
Coupled dv/dt	— electronic	<ul> <li>a measure of the ability of an opto thyristor coupler to block when the coupler is subjected to rapidly changing isolation voltage.</li> </ul>
Coupler	<ul><li>electronic</li></ul>	— abbreviation for optocoupler.
Critical Angle	— optics	<ul> <li>the largest angle of incidence of light, on the interface of two transmission mediums, that light will be transmitted between the mediums. Light at greater angles of incidence will be reflected.</li> </ul>
Current Transfer Ratio	— electronic	<ul> <li>the ratio of output current to input current, at a specified bias, of an optocoupler.</li> </ul>
Dark Current	— electronic	— Leakage current, usually $I_{\text{CEO}}$ , of a photodetector with no incident light.
Darlington	— electronic	<ul> <li>A composite transistor containing two transistors connected to multiply current gain.</li> </ul>
Detector	— radiometric	<ul> <li>A device which changes light energy (radiation) to electrical energy.</li> </ul>
Diffraction	— optics	<ul> <li>The phenomena of light bending at the edge of an obstacle.</li> <li>Demonstrates wave properties of light.</li> </ul>
Diode	— electronic	<ul> <li>A device that normally permits only one direction of current flow. A P-N junction diode will generate electricity when the junction is illuminated.</li> </ul>
Doping	— electronic	<ul> <li>The addition of carrier supplying impurities to semiconductor crystals.</li> </ul>
<b>Duty Cycle</b>	— electronic	<ul> <li>The ratio of on time to period of a pulse train.</li> </ul>
Efficiency	— electronic	— In this handbook, refers to the ratio of output power of a
		source to electrical input power.

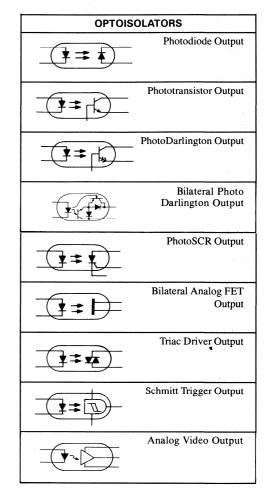
Effective Irradiance	— electronic	— Irradiance as perceived by a detector.
Emittance	radiometric	— Power radiated per unit area from a surface.
Emitter	— electronic	<ul> <li>Main terminal of a transistor which bias voltage normally has</li> </ul>
Emittei	— electronic	a major effect on current.
Emitter	_ radiometric	<ul> <li>A source of radiation.</li> </ul>
Epitaxial Epitaxial	- electronic	<ul> <li>Material added to a crystalline structure which has and</li> </ul>
Epitaxiai	- ciccironic	maintains the original crystals' structure.
f/number	— optics	Ratio of focal length to lens diameter.
Fiber Optics	— optics	<ul> <li>Transparent fiber which transmits light along the fiber's axis</li> </ul>
Ther optics	optics	due to the critical angle at the fiber's circumference.
Foot Candle	<ul><li>photometric</li></ul>	— Illumination level of one lumen per square foot.
Foot Lambert	<ul><li>photometric</li></ul>	<ul> <li>Brightness of source of one lumen per square foot.</li> </ul>
Gallium Arsenide	<ul><li>electronic</li></ul>	<ul> <li>A crystalline compound which is doped to form IRED's.</li> </ul>
Gallium	<ul><li>electronic</li></ul>	— Another crystalline compound which is doped to form IRED's
Aluminum Arse	nide	and LED's.
Gate	— electronic	- Control terminal of an SCR or, a logic function component.
Hash	<ul><li>electronic</li></ul>	- Random, high frequency noise on a signal or logic line.
Illumination	- photometric	— Light level on a unit area.
Infrared	<ul> <li>photometric</li> </ul>	- Radiation of longer wavelength than normally perceived by
		the eye, i.e., .78 to 100 microns wavelength.
Interrupter Module	— electronic	<ul> <li>Optoelectronic device which detects objects which break the light beam from an emitter to a detector.</li> </ul>
Irradiance	<ul><li>radiometric</li></ul>	<ul> <li>Radiated power per unit area incident on a surface, broadband analogy to illumination.</li> </ul>
Isolation Voltage	— electronic	<ul> <li>The dielectric withstanding voltage capability of an optocoupler under defined conditions and time.</li> </ul>
Light	— photometric	<ul> <li>Radiation normally perceived by the eye, i.e., .38 to .78 microns wavelength.</li> </ul>
Light Current	— electronic	<ul> <li>Current through a photodetector when illuminated under specified bias conditions.</li> </ul>
Lumen	— photometric	<ul> <li>Unit of radiant flux through one steradian from a one-candela source.</li> </ul>
Micron	<ul><li>radiometric</li></ul>	- 10 ° meters.
Modulation	— electronic	<ul> <li>The transmission of information by modifying a carrier signal—usually its amplitude or frequency.</li> </ul>
Monochrometer	— photometric	<ul> <li>An instrument which is a source of any specific wavelength of radiation over a specified band.</li> </ul>
Monochromatic	— photometric	— Of a single color, wavelength.
Nanometer	- radiometric	
Normalized	- electronic	- Presentation of the change in a parameter, due to a test
		condition change, made by dividing the final value by the initial value.
Optocoupler	— electronic	- A single component which transmits electrical information,
•		without electrical connection, between a light source and a light detector.
Optoisolator	— electronic	— Optocoupler.

Peak Spectral Emission	— radiometric	— Wavelength of highest intensity of a source.
Photoconductor	— electronic	— A material with resistivity that varies with illumination level.
Photocoupler	— electronic	- Optocoupler.
Photodarlington	<ul><li>electronic</li></ul>	- Light sensitive, darlington connected, transistor pair photo-
en e		detector.
Photodetector	— electronic	<ul> <li>A device which provides an electrical signal when irradiated by infrared, visible, and/or ultraviolet light.</li> </ul>
Photodiode	<ul><li>electronic</li></ul>	<ul> <li>p-n junction semiconductor diode photodetector.</li> </ul>
Photon	<ul><li>electronic</li></ul>	<ul> <li>Quantum of light from wave theory.</li> </ul>
PhotoSCR	<ul><li>electronic</li></ul>	- LASCR.
Phototransistor	<ul><li>electronic</li></ul>	<ul> <li>A transistor photodetector.</li> </ul>
Photovoltaic Cell	— electronic	<ul> <li>A photodiode connected to supply electricity when illuminated.</li> </ul>
Point Source	— radiometric	<ul> <li>A source with maximum dimension less than 1/10 the distance between source and detector.</li> </ul>
Reflector Module	— electronic	<ul> <li>Component containing a source and detector which detects objects which complete the light path by reflecting the light.</li> </ul>
Silicon	— electronic	<ul> <li>Crystalline element which is doped to make photodiode, phototransistor, photodarlington, photoSCR, etc. detectors.</li> </ul>
Silicon Controlled Rectifier	— electronic	<ul> <li>A reverse blocking thyristor which can block or conduct in forward bias, conduction between the anode and cathode being initiated by forward bias of the gate cathode junction.</li> </ul>
Source	<ul><li>radiometric</li></ul>	<ul> <li>A device which provides radiant energy.</li> </ul>
Spectral Distribution	— radiometric	<ul> <li>A plot, usually normalized, of source intensity vs. wavelength observed.</li> </ul>
Spectral Sensitivity	— radiometric	— A plot of detector sensitivy vs. wavelength detected.
Steradian	- radiometric	— Unit of solid angle. A sphere contains $4\pi$ steradians.
Synchroneous Detection	— electronic	<ul> <li>A technique which detects low level pulses by detecting only signal changes which occur at the same time as the pulse.</li> </ul>
Thermopile	<ul> <li>radiometric</li> </ul>	<ul> <li>A very broadband, heat sensing, radiation detector.</li> </ul>
Transistor	— electronic	<ul> <li>Three-terminal semiconductor device which behaves as a current controlled current source.</li> </ul>
Triac	— electronic	<ul> <li>A thyristor which can block or conduct in either polarity.</li> <li>Conduction is initiated by forward bias of a gate—MTI junction.</li> </ul>
Triac driver	— electronic	<ul> <li>A low current thyristor used to control power thyristors.</li> <li>Usually a photodetector in an optoisolator.</li> </ul>
Tungsten	— radiometric	— The element normally used for incandescent lamp filaments.
Unijunction Transistor	— electronic	<ul> <li>A three-terminal voltage threshold semiconductor device normally used for oscillators and time delays.</li> </ul>
Wavelength	— radiometric	— The speed of light divided by the frequency of the electromagnetic radiation-wave theory of light.
Watt	— electronic	— Unit of power, a volt ampere.
Watt	— photometric	— Unit of power, 685 lumens at 0.555 microns wavelength.

#### OPTO ELECTRONIC DEVICES

#### SCHEMATIC SYMBOLS USED IN THIS MANUAL

DISCRETE D	EVICES
Light or Infrared Emitting Diode	A
Photodiode	A K
PhotoDarlington	B
Phototransistor	° E
	B
Photo SCR or LASCR	A K
Photo Schmitt Trigger	



# U

# **Bibliography and References**

Bibliography and References	 164

## **BIBLIOGRAPHY AND REFERENCES**

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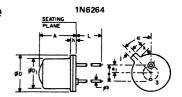
# **Technical Data**

Emitter Specifications	
Detector Specifications	
Optoisolator Specifications	
Optointerrupter Specifications	
European "Pro Electron" Registered Types	
Generic Optoisolator Specifications	

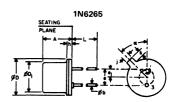
#### 1N6264, 1N6265

# Infrared Emitter Gallium Arsenide Infrared Emitting Diode

The 1N6264 and 1N6265 Series are gallium arsenide, light emitting diodes which emit non-coherent, infrared energy. They are ideally suited for use with silicon detectors. The 1N6264 has a lens which provides a narrow beam angle while the 1N6265 has a flat window for a wide beam angle which is useful with external lensing.



SYMBOL	INC MIN.	HES MAX.	MILLIN MIN.	METERS MAX.	NOTES
A		.255		6.47	
	.016	.021	.407	533	
40	.209	.230	5.31	584	
øD₁	.180	.188	4.57	4.77	İ
· ·	.10	ONOM.	2.54	NOM.	2
•1	.05	O NOM.	1.27	NOM.	2
h		.030		76	
- i	.031	.044	.79	141	
. k	.036	.046	. ,92	1.16	1,
L I	1.00		25.4		
α	4	50		45°	3



SYMBOL	INCI MIN.	HES MAX	MILLIMETERS		NOTES
	MITTE.		min.		MUIES
Α :		. 155	l	3.93	
øb	.016	.021	.407	533	
40	.209	.230	5,31	5,84	
øD₁	180	.187	4,57	4.77	
•	. IOONOM.		2.54 NOM.		2
•,	.05	ONOM.	1.27 NOM		2
h	-	.030	١.	.76	
j	.031	.044	.79	1.11	
k	.036	.046	.79 .92	1.16	1
L	1.00		25.4		
Œ	45*		4	5.	3



- 1. Measured from maximum diameter of device.
- Leads having max. diameter .021" (.533mm) measured in gaging plane .054" + .001" - .000 (137 + 025 -000mm) below the reference plane of the device shall be within .007" (.778mm) their true position relative to a maximum width tab.
- 3. From centerline tab.

#### absolute maximum ratings: (25°C unless otherwise specified)

	•		
Voltages			
† Reverse Voltage	$V_R$	3	volts
Currents			
† Forward Current (continuous)	$I_F$	100	mA
† Forward Current (pw 1 µs, 200 Hz)	$I_{\mathbf{F}}$	10	Α
Dissipation			
† Power Dissipation $(T_A = 25^{\circ}C)^*$	$\mathbf{P}_{\mathbf{T}}$	170	mW
Power Dissipation $(T_C = 25^{\circ}C)^{**}$	$P_{T}^{-}$	1.3	W
Temperatures			
† Junction Temperature	$T_J$	-65 to +150	°C
† Storage Temperature	$T_{stg}$	-65 to +150	°C
† Lead Soldering Time (1/16" [1.6mm]		260	°C
from case for 10 sec.)			

<sup>\*</sup>Derate 1.36 mW/°C above 25°C ambient.

#### electrical characteristics: (25°C unless otherwise specified)

		SYM.	MIN.	TYP.	MAX.	UNITS
† Reverse Le	eakage Current					
$(V_R = 1)$	3V)	$I_R$		_	10	$\mu$ A
† Forward V	oltage/					
$(I_F = 1)$	00 mA)	$V_{\mathrm{F}}$	_	1.4	1.7	Volts
† Total Pow	er Output (note 1)					
$(I_F = 1)$	00 mA)	$P_{o}$	6		-	mW
† Peak Emis	sion Wavelength					
$(I_F = 1)$	00 mA)	$\lambda_{p}$	935	945	955	nm
Spectral S	hift with Temperature	•	_	.28	_	nm/°C
† Spectral B	andwidth – 50%	Δλ	man		60	nm
† Half Inten	sity Beam Angle					
1N6264	4	$\theta_{\rm HI}$	_	_	20	deg
1N626	5	$\theta_{\rm HI}$	_		80	deg
Rise Time	- 0-90% of Output	t <sub>r</sub>	_	1.0	_	μs
Fall Time	- 100-10% of Output	$t_{\mathbf{f}}$	-	1.0	_	μs

#### Note 1

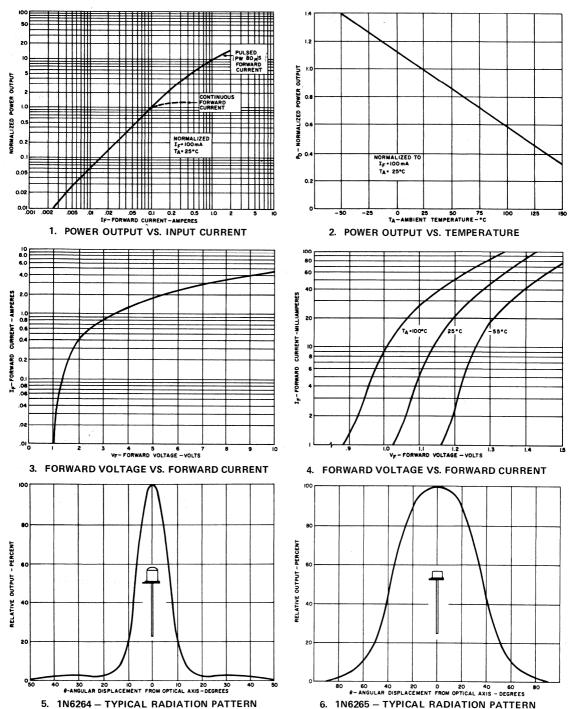
Total power output,  $P_O$ , is the total power radiated by the device into a solid angle of  $2\pi$  steradians.

† Indicates JEDEC registered values.

<sup>\*\*</sup>Derate 10.4 mW/°C above 25°C case.

#### 1N6264, 1N6265

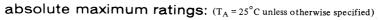
#### TYPICAL CHARACTERISTICS



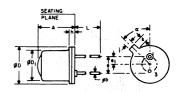
#### 1N6266

# Infrared Emitter Gallium Arsenide Infrared Emitting Diode

The 1N6266 is a gallium-arsenide, infrared emitting diode which emits non-coherent, infrared energy with a peak wavelength of 940 nanometers. This device is characterized to precisely define the infrared beam along the mechanical axis of the device.



Voltages			
*Reverse Voltage	$V_R$	3	Volts
Currents			
*Forward Current (Continuous)	$I_{\mathbf{F}}$	100	mA
*Forward Current (pw 1 µsec 200Hz)	$I_{\mathbf{F}}$	10	A
Dissipation			
*Power Dissipation (T <sub>A</sub> = 25°C) †	$P_{T}$	170	mWatts
*Power Dissipation ( $T_A = 25^{\circ}C$ ) † Power Dissipation ( $T_C = 25^{\circ}C$ )	$P_{T}$	1.3	Watts
Temperatures			
*Junction Temperature	$T_{J}$	-65 to +150	°C
*Storage Temperature	$T_{STG}$	-65 to +150	°C
*Lead Soldering Time (1/16", 1.6mm,	$T_L$	-65 to +150 +260	°C
from case for 10 sec.)	_		
†Derate 1.36mW/°C above 25°C ambient. ††Derate 10.4mW/°C above 25°C case.			

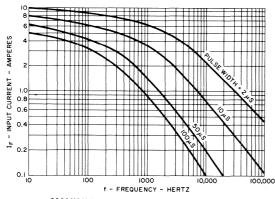


SYMBOL	INC	HES MAX.	MILLIN	METERS MAX.	NOTES		
Δ.		255		6.47			
مَ	.016	021	407	533			
øD	209	230	5.31	5.84			
øD <sub>1</sub>	.180	.188	4.57	4,77			
-	.100	NOM.	2.54 NOM.		. ?		
•,	.050 NOM.		1.27 NOM		.050 NOM. 1.27 NOM.		2
, i	- 1	.030		.76			
- i - 1	.031	.044	.79	1.11			
. 1	.036	046	,92	1.16	1		
	1.00		25.4				
α	. 4	5*		45°	3		



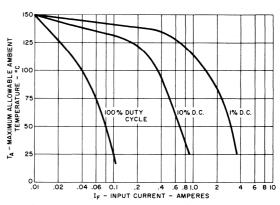
- Measured from maximum diameter of device.
- Leads having max. diameter .021" (.533mm) measured in gaging plane .054" - .001" - .000 (137 + 025 -000mm) below the reference plane of the device shall be within .007" (.778mm) their true position relative to a maximum width tab.
- 3. From centerline tab.

#### MAXIMUM RATING CURVES



\*Indicates JEDEC registered values.

MAXIMUM PULSE CAPABILITY



MAXIMUM TEMPERATURE VS. INPUT CURRENT

#### 1N6266

#### electrical characteristics: (T<sub>A</sub> = 25°C unless otherwise specified)

Static Characteristics	SYMBOL	MIN.	TYP.	MAX.	UNITS
*Reverse Leakage Current (V <sub>R</sub> = 3V)	$I_R$			10	μΑ
*Forward Voltage $(I_F = 100 \text{ mA})$	$V_{ m F}$	0.9	- <u>-</u>	1.7	Volts
*Radiant Intensity $(I_F = 100 \text{ mA}, \omega = 0.01 \text{ Sr})$	$I_e$	25			mW/sr
*Peak Emission Wavelength $(I_F = 100 \text{ mA})$	$\lambda_p$	935		955	nm
Spectral Shift with Temperature		<u> </u>	.28	AMOUNT	nm/°C
*Spectral Bandwidth - 50%	Δλ			60	nm
*Half Intensity Beam Angle	$ heta_{ ext{HI}}$			20	de g-
Rise Time	t <sub>r</sub>	_	1.0	_	μs
Fall Time	$t_{\mathbf{f}}$	_	1.0		μs

<sup>\*</sup>Indicates JEDEC registered values.

l,

#### INFRARED EMITTING DIODE RADIANT INTENSITY

The design of an Infrared Emitting Diode (IRED)-photo-detector system normally requires the designer to determine the minimum amount of infrared irradiance received by the photodetector, which then allows definition of the photo-detector current. Prior to the introduction of the 1N6266, the best method of estimating the photodetector received infrared was to geometrically proportion the piecewise integration of the typical beam pattern with the specified minimum total power output of the IRED. However, due to the inconsistencies of the IRED integral lenses and the beam lobes, this procedure will not provide a valid estimation.

The 1N6266 now provides the designer specifications which precisely define the infrared beam along the device's mechanical axis. The 1N6266 is a premium device selected to give a minimum radiant intensity of 25 mW/steradian into the 0.01 steradians referenced by the device's mechanical axis and seating plane. Radiant intensity is the IRED beam power output, within a specified solid angle, per unit solid angle.

A quick review of geometry indicates that a steradian is a unit of solid angle, referenced to the center of a sphere, defined by  $4\pi$  times the ratio of the area projected by the solid angle to the area of the sphere. The solid angle is equal to the projected area divided by the squared radius.

Steradians = 
$$4\pi A/4\pi R^2 = A/R^2 = \omega$$
.

As the projected area has a circular periphery, a geometric integration will solve to show the relationship of the Cartesian angle  $(\alpha)$  of the cone, (from the center of the sphere) to the projected area.

$$\omega = 2\pi (1-\cos \frac{\alpha}{2}).$$

Radiant intensity provides an easy, accurate tool to calculate the infrared power received by a photodetector located on the IRED axis. As the devices are selected for beam characteristics, the calculated results are valid for worst case analysis. For many applications a simple approximation for photodetector irradiance is:

$$H \cong I_e/d^2$$
, in mw/cm<sup>2</sup>

where d is the distance from the IRED to the detector in cm

IRED power output, and therefore  $I_e$ , depends on IRED current. This variation  $(\Delta I_e/\Delta I)$  is documented in Figure 1, and completes the approximation:  $H = I_e/d^2$   $(\Delta I_e/\Delta I)$ . This normally gives a conservative value of irradiance. For more accurate results, the effect of precise angle viewed by the detector must be considered. This is documented in Figure 2  $(\Delta I_e/\Delta\omega)$  giving:

$$H = I_e/d^2 (\Delta I_e/\Delta I)$$
 in  $mw/cm^2$ .

For worst case designs, temperature coefficients and tolerances must also be considered.

The minimum output current of the detector  $(I_L)$  can be determined for a given distance (d) of the detector from the IRED.

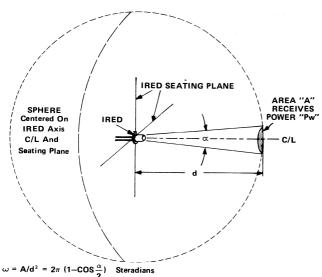
$$I_L = (S)H \cong (S)I_e/d^2$$
or

$$I_L = (S)H = (S) (I_e/d^2) (\Delta I_e/\Delta \omega) (\Delta I_e/\Delta I)$$

where S is the sensitivity of the detector in terms of output current per unit irradiance from a GaAs source.

#### 1N6266

#### IRED RADIANT INTENSITY SPECIFICATION CONCEPT



#### **MATCHING A PHOTOTRANSISTOR WITH 1N6266**

Assume a system requiring a 10mA I<sub>L</sub> at an IRED to detector spacing of 2cm (seating plane to seating plane), with bias conditions at specification points.

Given:  $d_1 = 2 \text{ cm}$ ;  $I_{L_1} = 10 \text{ mA min.}$ ;  $I_{e} = 25 \text{ mW/Steradian}$ Then:  $H_1 \cong Ie/D_1^2 = 25/(2)^2 = 6.25 \text{ mW/cm}^2$ .

Detector Evaluation:

I∟ MIN. @		H (Tungsten) ≅		H(GaAs)	S(GaAs)	
TYPE	mA	mw/cm²		mw/cm²	mA/mw/cm <sup>2</sup>	
L14G1	6	10		3	2	
L14G2	3	10		3	1	

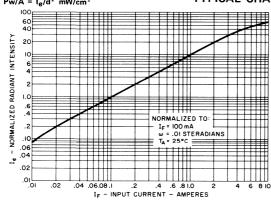
Calculated  $I_L = d_1$  is:

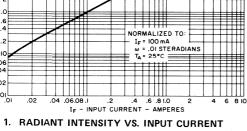
L14G1 (S) 
$$H_1 = (2) 6.25 = 12.5 \text{ mA}$$
  
L14G2 (S)  $H_1 = (1) 6.25 = 6.25 \text{ mA}$ 

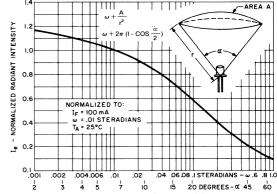
Since the system requires an  $I_L$  of 10 mA minimum the correct device to use is the L14G1.

#### mW/Steradian $H = Pw/A = I_e/d^2 mW/cm^2$

#### TYPICAL CHARACTERISTICS

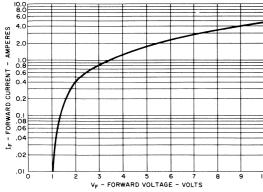


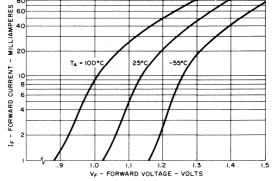




#### 2. INTENSITY AND POWER VS. ANGLE Δ le/Δω

 $\Delta$  le/ $\Delta$ l





3. FORWARD VOLTAGE VS. FORWARD CURRENT

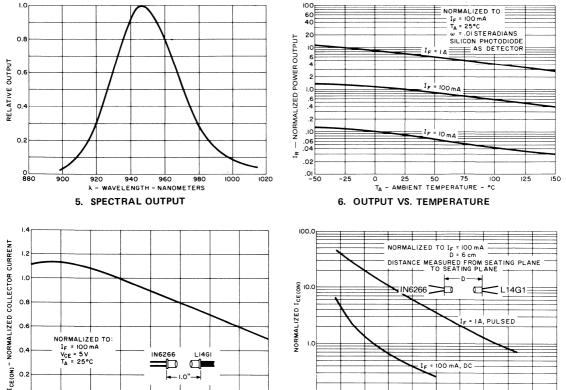
FORWARD VOLTAGE VS. FORWARD CURRENT

170

15

#### 1N6266

#### TYPICAL CHARACTERISTICS



7. OUTPUT VS. TEMPERATURE IRED/PHOTOTRANSISTOR PAIR 8. IL VS. DISTANCE IRED/PHOTOTRANSISTOR PAIR

-50

-25

25

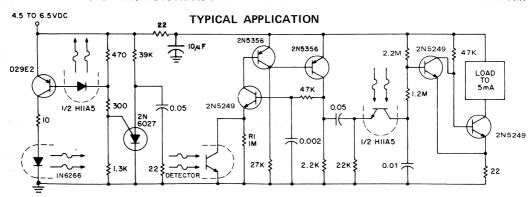
50

T - TEMPERATURE - °C

75

100

125



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DETECTOR SELECTION	TRANSMISSION RANGE	REFLECTIVE RANGE
L14Q1	12''	3"
L14G3	48''	12"

OBJECT DETECTOR FEATURING LOW POWER CONSUMPTION AND LONG-RANGE CAPABILITY.

# Infrared Emitter Gallium Aluminum Arsenide Infrared Emitting Diode

The F5D and F5E Series are infrared emitting diodes. They exhibit high power output and a typical peak wavelength of 880 nanometers and provide a significant increase in system efficiency, when used with silicon detectors, compared to GaAs infrared emitting diodes. The F5D Series has a lens which provides a narrow beam angle while the F5E Series has a flat window for a wide beam angle which is useful with external lensing.



F5D1, F5D2, F5D3 F5E1, F5E2, F5E3

#### absolute maximum ratings: (25°C, unless otherwise specified)

Voltage	SYMBOL		UNITS
Reverse Voltage	$V_R$	3	V
Current			
Forward Current (continuous)	$I_{F}$	100	mA
Forward Current (pw, 1 µs; 200 Hz)	$I_{\rm F}$	10	Α
Forward Current (pw, 10 µs; 100 Hz)	$ m I_F^{'}$	3	Α
Dissipation			
Power Dissipation $(T_{\Delta} = 25^{\circ}C)^*$	$P_{T}$	170	mW
Power Dissipation $(T_C = 25^{\circ}C)^{**}$	$P_{T}^{'}$	1.3	W
Temperatures			
Junction Temperature	$T_{r}$	-65 to +150	°C
Storage Temperature	$T_{stg}$	-65 to +150	°C
Lead Soldering Time (1/16" [1.6mm] from case for 10 sec.)	$T_L^{sig}$	+260	°C

<sup>\*</sup>Derate 1.36 mW/°C above 25°C ambient.

#### electrical characteristics: (25°C, unless otherwise specified)

	SYMBOL	MIN.	TYP.	MAX.	UNITS
Reverse Leakage Current					
$(V_R = 3V)$	$I_{\mathbf{R}}$	-	<u> </u>	10	$\mu$ A
Forward Voltage					
$(I_F = 100 \mathrm{mA})$	$ m V_{ m F}$	_	_	1.7	Volts
$(I_F = 1 A)$	$V_{f F}$	_	-	3.5	Volts

#### optical characteristics: (25°C, unless otherwise specified)

Total Power Output		SYMBOL	MIN.	TYP.	MAX.	UNITS
$(I_F = 100 \mathrm{mA})(\mathrm{Note}\ 1)$	- F5D1, F5E1	$P_{o}$	12		_	mW
	- F5D2, F5E2		9			mW
Peak Emission Wavelength	- F5D3, F5E3		10.5	. <del>-</del>	<del></del>	m <b>W</b>
$(I_F = 100 \mathrm{mA})$		$\lambda_{p}$	_	880		nm

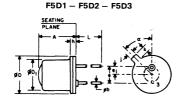
<sup>\*\*</sup>Derate 10.4 mW/°C above 25 °C case.

#### optical characteristics (continued): (25°C, unless otherwise specified)

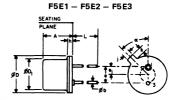
	SYMBOL	MIN.	TYP.	MAX.	UNITS
Spectral Shift with Temperature		_	.3	_	nm/°C
Spectral Bandwidth - 50%	Δλ	_	80	_	nm
Half Intensity Beam Angle - F5D1, F5D2, F5D3 - F5E1, F5E2, F5E3	$ heta_{ m HI}$	<u>-</u>		20 80	Deg. Deg.
Rise Time 0-90% of Output (Note 2)	t <sub>r</sub>		1.5	_	μs
Fall Time 100-10% of Output (Note 2)	$t_{\mathbf{f}}^{\circ}$	_	1.5	_	μs

#### NOTES:

- 1. Total power output,  $P_0$ , is the total power radiated by the device into a solid angle of  $2\pi$  steradians.
- 2. At  $I_F = 100 \,\text{mA}$ ,  $t_r \le 10 \,\text{ns}$  input current pulse.







SYMBOL	INC	HES	MILLIMETERS		NOTES
3 T WIBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	_	.255	-	6.47	
φb	.016	.021	.407	.533	
φD	.209	.230	5.31	5.84	
$\phi D_1$	.180	.188	4.57	4.77	
е	.100 NOM		2.54 NOM		2
e <sub>1</sub>	.050	NOM	1.27 NOM		2
h	_	.030	_	.76	
j	.031	.044	.79	1.11	
k	.036	.046	.92	1.16	1
L	1.00	_	25.4	_	
α	45°	45°	45°	45°	3

#### NOTES:

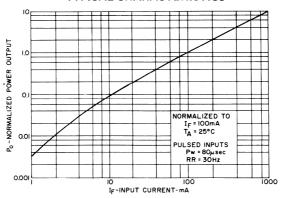
- Measured from maximum diameter of device.
- Leads having maximum diameter .021" (.533mm) measured in gauging plane .054" + .001" .000 (137 + 025 000mm) below the reference plane of the device shall be within .007" (.778mm) their true position relative to a maximum width tab.
- 3. From centerline tab.

SYMBOL	INC	HES	MILLIN	MILLIMETERS	
STIVIBUL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	_	.155	_	3.93	
φb	.016	.021	.407	.533	
φD	.209	.230	5.31	5.84	
$\phi D_1$	.180	.188	4.57	4.77	
е	.100 NOM		2.54 NOM		2
e <sub>i</sub>	.050 I	MON	1.27	NOM	2
h	-	.030	_	.76	
j	.031	.044	.79	1.11	
k	.036	.046	.92	1.16	1
L	1.00	-	25.4	_	
α	45°	45°	45°	45°	3

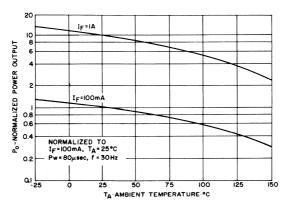
#### NOTES:

- 1. Measured from maximum diameter of device.
- Leads having maximum diameter .021" (.533mm) measured in gauging plane .054" + .001" .000 (137 + 025 000mm) below the reference plane of the device shall be within .007" (.778mm) their true position relative to a maximum width tab.
- 3. From centerline tab.

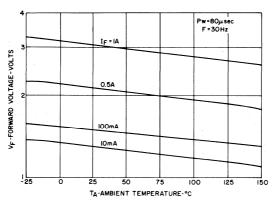
TYPICAL CHARACTERISTICS



#### 1. POWER OUTPUT VS. INPUT CURRENT

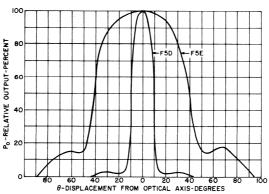


#### 2. POWER OUTPUT VS. TEMPERATURE

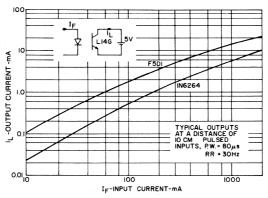


#### 3. FORWARD VOLTAGE VS. TEMPERATURE

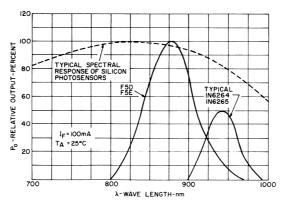




#### 4. TYPICAL RADIATION PATTERN



5. OUTPUT VS. INPUT WITH L14G DETECTOR



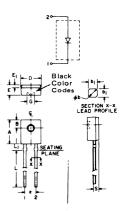
6. OUTPUT VS. WAVELENGTH

#### F5F1

# Infrared Emitter Gallium Arsenide Infrared Emitting Diode

The F5F1 is a Gallium-Arsenide, infrared emitting diode which emits non-coherent, infrared energy with a peak wavelength of 940 nanometers. It is packaged in a clear, side looking, epoxy encapsulant.

#### absolute maximum ratings: (25°C) (unless otherwise specified) **VOLTAGES** SYMBOL UNITS Reverse Voltage $V_R$ CURRENT Forward Current (continuous) $I_{\rm F}$ 60 mA Forward Current (Peak, pw = $1\mu$ s, PRR $\leq 300$ pps) 3 Α DISSIPATION Power Dissipation\* 100 mW **TEMPERATURES** °C Junction Temperature -55 to + 100 $T_{I}$ °C Storage Temperature $T_{STG}$ -55 to +100Lead Soldering Temperature 260 °C $T_L$



SYM	MILLI-		INC	HES	NOTES
	MIN	MAX	MIN	MAX	
Α	5.59	5.80	.220	.228	
В	1.78	NOM.	.070	NOM.	2
φb	.60	.75	.024	.030	1
b <sub>1</sub>	.51	NOM.	.020	NOM.	1
D	4.45	4.70	.175	.185	
E	2.41	2.67	.095	.105	
E <sub>1</sub>	.58	.69	.023	.027	
e	2.41	2.67	.095	.105	3
G	1.98	NOM.	.078	NOM.	
L	12.7	_	.500	-	
L <sub>1</sub>	1.40	1.65	.055	.065	
s	.83	.94	.033	.037	3

#### NOTES

- Two leads. Lead cross section dimensions uncontrolled within 1.27 MM (.050") of seating plane.
- Centerline of active element located within .25 MM (.010") of true position.
- As measured at the seating plane.
- 4. Inch dimensions derived from millimeters.

#### electrical characteristics: (25°C)

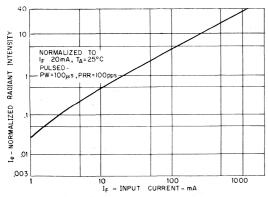
(5 seconds maximum, 1.6mm from case)

	SYMBOL	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage, $I_R = 10\mu A$	$V_{(BR)R}$	6	·		V
Forward Voltage, $I_F = 60 \text{mA}$	$V_{F}$	_	1.5	1.7	V
Reverse Leakage Current, $V_R = 5V$	$I_R$			100	nA
Capacitance, $V = 0$ , $f = 1MHz$	$C_{i}$		30		pF
optical characteristics:					
Radiant Intensity, $I_F = 20 \text{mA}$ , $\omega = 0.06 \text{sr}$	$I_e$	0.28	_		mW/sr
Peak Emission Wavelength, I <sub>F</sub> = 60mA	$\lambda_{\rm p}$	935	<u> </u>	955	nm
Spectral Bandwidth — 50%	Δλ			60	nm
Half Intensity Beam Angle	$ heta_{ ext{HI}}$		30		deg.

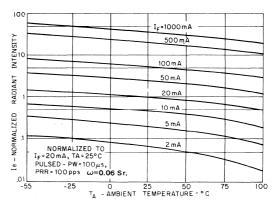
 $<sup>\</sup>dagger I_e$  measured with a 0.45cm aperture placed 1.6cm from the tip of the lens, on the lens center line perpendicular to the plane of the leads.

<sup>\*</sup>Derate 1.33mW/°C above 25°C ambient

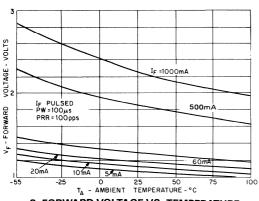
#### F5F1



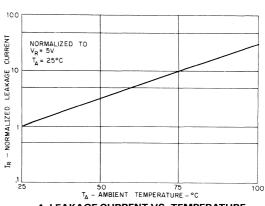
1. RADIANT INTENSITY VS. INPUT CURRENT



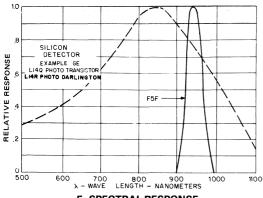
2. RADIANT INTENSITY VS. TEMPERATURE



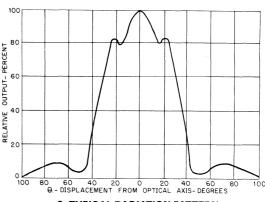
3. FORWARD VOLTAGE VS. TEMPERATURE



4. LEAKAGE CURRENT VS. TEMPERATURE



5. SPECTRAL RESPONSE



6. TYPICAL RADIATION PATTERN

#### **F5G1**

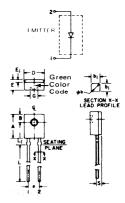
## **Infrared Emitter Gallium Aluminum Arsenide Infrared Emitting Diode**

The F5G1 is a Gallium-Aluminum-Arsenide, infrared emitting diode which emits non-coherent, infrared energy with a peak wavelength of 880 nanometers. This device will provide a significant increase in system efficiency, when used with silicon detectors, compared to GaAs infrared emitting diodes. It is encapsulated in a clear side looking, epoxy package with an integral recessed lens.

#### absolute maximum ratings: (25°C) unless otherwise specified

VOLTAGES Reverse Voltage	SYMBOL V <sub>R</sub>	6	UNITS V
CURRENT Forward Current (continuous) Forward Current (Peak, pw = 1 μs, PRR ≤ 300 pps)	$I_{\mathrm{F}}$	50 2	mA A
DISSIPATION Power Dissipation*	$P_{\mathrm{T}}$	100	mW
TEMPERATURES Junction Temperature Storage Temperature Lead Soldering Temperature (5 seconds maximum, 1.6mm from case)	T <sub>J</sub> T <sub>STG</sub> T <sub>L</sub>	-55 to +100 -55 to +100 260	°C °C °C

<sup>\*</sup>Derate 1.33mW/°C above 25°C ambient



SYM		MILLI- METERS		HES	NOTES
	MIN	MAX	MIN	MAX	
A	5.59	5.80	.220	.228	
8	1.78	NOM.	.070	NOM.	2
øb	.60	.75	.024	.030	1
ь, .	.51	NOM.	.020	NOM.	1
D	4.45	4.70	.175	.185	
E	2.41	2.67	.095	.105	
E <sub>1</sub>	.58	.69	.023	.027	
•	2.41	2.67	.095	.105	3
G	1.98	NOM.	.078	NOM.	
L	12.7	-	.500	-	
L <sub>1</sub>	1.40	1.65	.055	.065	
S	83	.94	.033	.037	3

- Two leads. Lead cross section dimensions unco trolled within 1.27 MM (.050") of seating plan
- Centerline of active element located within .25 MM (.010") of true position.
- Inch dimensions derived from millimeters

#### electrical characteristics: (25°C)

	SYMBOL	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage (I <sub>R</sub> = 10 μA)	V <sub>(BR)R</sub>	6			V
Forward Voltage, I <sub>F</sub> = 60mA (pulsed)	$V_{\mathrm{F}}$		1.5	1.85	V
$I_{\rm F} = 20 {\rm mA}$	$V_{\rm F}$	_		1.7	V
Reverse Leakage Current, V <sub>R</sub> = 5V	$I_{R}$			10	μΑ
Capacitance, $V = 0$ , $f = 1MHz$	C <sub>i</sub>	_	30	_	pF

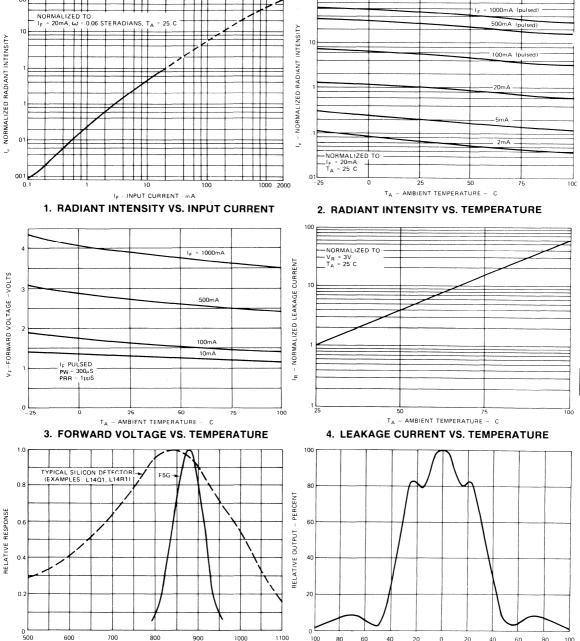
#### optical characteristics:

Radiant Intensity, $I_F = 20 \text{mA}$ , $\omega = 0.06 \text{sr}$	l <sub>e</sub>	0.6	_	_	mW/sr
Peak Emission Wavelength, I <sub>F</sub> = 20mA	$\lambda_{\rm p}$		880		nm
Spectral Bandwidth — 50%	Δλ		50		nm
Half Intensity Beam Angle	$ heta_{ m HI}$		35		deg.

<sup>†1,</sup> measured with a 0.45cm aperture placed 1.6cm from the tip of the lens, on the lens center line perpendicular to the plane of the leads.

# **F5G1**

### TYPICAL CHARACTERISTICS



800

> - WAVE LENGTH - NANOMETERS

5. SPECTRAL RESPONSE

900

1000

1100

100

179

DEGREES

DISPLACEMENT FROM OPTICAL AXIS

6. TYPICAL RADIATION PATTERN

# LED55B, LED55C, LED56, LED55BF, LED55CF, LED56F

# Infrared Emitter Gallium Arsenide Infrared Emitting Diode

The LED55B-LED55C-LED56 Series are gallium arsenide, light emitting diodes which emit non-coherent, infrared energy with a peak wave length of 940 nanometers. They are ideally suited for use with silicon detectors. The LED55B, LED55C and LED56 devices have a lens which provides a narrow beam angle while the "F" versions have a flat window for a wide beam angle which is useful with external lensing.

absolute maximum ratings: (25°C unless otherwise specified)

Voltage: Reverse Voltage	$V_{\mathbf{p}}$	3	volts
	· K		
Currents: Forward Current Continuous	T	100	m A
	$l_{\mathrm{F}}$		
Forward Current (pw 1 µsec 200 Hz)	$I_{\mathbf{F}}$	10	· A
Dissipations:		1	
Power Dissipation $(T_A = 25^{\circ}C)^*$	$P_{T}$	170	mW
Power Dissipation (T <sub>C</sub> = 25°C)**	$P_{T}$	1.3	W
Temperatures:			
Junction Temperature	$T_{I}$	-65°C to +	150°C
Storage Temperature		-65°C to +	
<b>U</b> .	181G	seconds at	260°C
Lead Soldering Time	. 10	seconds at	200 C
*Derate 1.36 mW/°C above 25°C ambient. **Derate 10.4 mW/°C above 25°C case.			

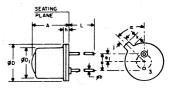
electrical characteristics: (25°C unless otherwise specified)

	MIIN.	IYP.	MAX.	UNITE
Reverse Leakage Current				
$(V_R = 3V)$	$I_{\mathbf{R}}$		10	$\mu$ A
Forward Voltage				
$(I_F = 100mA)$	$V_{\mathrm{F}}$	1.4	1.7	V

optical characteristics: (25°C unless otherwise specified)

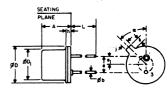
Total Power Output (note 1)		
$(I_F = 100 \text{mA})$		
LED55B-LED55BF	P <sub>O</sub> 3.5	mW
LED55C-LED55CF	5.4	mW
LED56 -LED56F	1.5	mW
Peak Emission Wavelength		
$(I_F = 100mA)$	940	nm
Spectral Shift with Temperature	.28	nm/°C
Spectral Bandwidth 50%	60	nm
Rise Time 0-90% of Output	1.0	μsec
Fall Time 100-10% of Output	1.0	μsec

Note 1: Total power output,  $P_O$ , is the total power radiated by the device into a solid angle of 2  $\pi$  steradians.



LED55B , LED55C , LED56

SYMBOL	INC MIN.	HES MAX	MILLIN	ETERS	NOTES
	MIN.	MAX.	MIN.	MAA.	MUIES
Α .		.255		6.47	
ga l	.016	021	.407	.533	1.
<b>#</b> D	.209	230	5.31	5.84	
øD:	.180	.188	4.57	4.77	
•	.10	ONOM.	2.54	NOM.	?
•1	. 05	O NOM.	1.27	NOM.	2
, I	- 1	.030	ł	.76	
i. l	.031	.044	.79	1.11	
	.036	.046	.92	1.16	- 1
L	1.00	1	25.4	Į.	
ā l	4	50		45*	3



LED55BF, LED55CF, LED56F

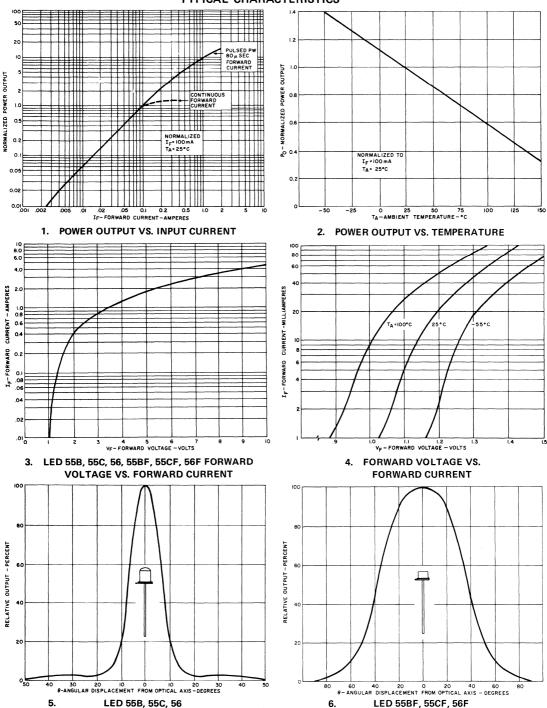
SYMBOL	INCI MIN.	HES MAX	MILLII MIN.	METERS	NOTES
· A		.155		3.93	
øb	.016	.021	.407	.533	
#0	.209	.230	5,31	584	
øD,	.180	.188	4.57	4.77	
	. 10	ONOM.	2.54	NOM.	2
•.	05	ONOM.	1.27	NOM	2
h l		.030	l	.76	
i l	.031	.044	70	1.11	
k	.036	.046	.79 .92	1.16	
L	1.00		25.4	1	
a	4	•	۱ ،	15*	3



- Measured from maximum diameter of device.
- Leads having max. diameter .021" (.533mm) measured in gaging plane .054" + .001" - .000 (137 + 025 -000mm) below the reference plane of the device shall be within .007" (.778mm) their true position relative to a maximum width tab.
- 3. From centerline tab.

# LED55B, LED55C, LED56, LED55BF, LED55CF, LED56F

#### TYPICAL CHARACTERISTICS



TYPICAL RADIATION PATTERN

**TYPICAL RADIATION PATTERN** 

# L14C1, L14C2

# **Light Detector Planar Silicon Phototransistor**

The L14C1 and L14C2 are NPN Silicon Phototransistors in a TO-18 style hermetically sealed package. The device has a top-looking flat lens which is thus ideally suited to optoelectronic sensing applications where external optics are being used. Generally only the collector and emitter leads are used; a base lead is provided, however, to control sensitivity and gain of the device.



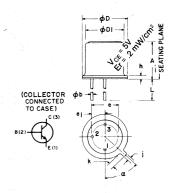
Voltages — Dark Characteristics Collector to Emitter Voltage	$V_{CEO}$	L14C1 50	<b>L14C2</b> 50	volts
Collector to Base Voltage	$V_{CEO}$	50	50	volts
Emitter to Base Voltage	$V_{EBO}$	7	7	volts
Currents				
Light Current	$\mathbf{I}_{L}$		50	mA
Dissipations				
Power Dissipation $(T_A = 25^{\circ}C)^*$	$P_T$	3	00	mW
Power Dissipation $(T_C = 25^{\circ}C)^{**}$	$P_{T}$	6	000	mW
Temperatures				
Junction Temperature	$T_J$	-65	to 150	°C
Storage Temperature	$T_{STG}$	-65	to 150	°C
Lead Soldering Time	$T_{L}$	10 5	Seconds at 2	260°C
*Derate 2.4 mW/°C above 25°C ambient	**Derate 4.8 mW	°C above 25°	C case	

electrical characteristics: (25°C) unless otherwise specified

		L14	4C1	L14	4C2	
STATIC CHARACTERISTICS		MIN.	MAX.	MIN.	MAX.	
Light Current						
$(V_{CE} = 5V, E_e = 10 \text{mW/cm}^2)$	$I_{L}$	1.0		0.5	_	mA
$(V_{CE} = 5V, E_e = 20mW/cm^2)$		_	_	1.0		mA
Dark Current						
$(V_{CE} = 20V, E_c \approx 0)$	$I_D$		100	_	100	nΑ
Emitter-Base Breakdown Voltage						
$(I_E = 100\mu A, I_C = 0, E_e \approx 0)$	$V_{(BR)EBO}$	7		7		V
Collector-Base Breakdown Voltage						
$(I_C = 100\mu A, I_E = 0, E_e \approx 0)$	$V_{(BR)CBO}$	50		50		V
Collector-Emitter Breakdown Voltage						
$(I_C = 10 \text{mA}, E_e \approx 0$	$V_{(BR)CEO}$	50		50		V
Pulse Width $\leq 300\mu \text{sec}$ ,						
Duty Cycle ≤ 1%)						
Saturation Voltage	V		0.2		0.2	V
$(I_C = 0.4 \text{mA}, E_e = 20 \text{mW/cm}^2)$	V <sub>CE(SAT)</sub>		0.2	<b>T</b> \/D	0.2	•
SWITCHING CHARACTERISTICS				TYP.		
Switching Speeds						
$(V_{CC} = 10V, I_L = 2mA, R_L = 100\Omega)$						
Turn-On Time	t <sub>on(=</sub>	$t_d + t_r$		5		μsec
Turn-Off Time	t <sub>off(=</sub>	t <sub>s</sub> + t <sub>f</sub> )		5		μsec
E <sub>e</sub> = Radiation Flux Density. Radiation source is an unf	iltered tungster	n filament	bulb at 2870	°K color t	emperatur	e.

Note: A GaAs source of 3.0mW/cm2 is approxiamately equivalent to a tungsten source, at 2870°K, of 10mW/cm2.





SYMBOL		HES	MILLIN	MAY	NOTES
STINDOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	-	210	-	5.34	
ФЬ	.016	.021	406	.534	
ΦD	.209	.230	5.30	5.85	
ΦDı	.178	.195	4.52	4.96	
e	.100	NOM		NOM	2
e <sub>1</sub>	.050	NOM	1.27	NOM	2
h	-	.030	-	.76	
	.036	.046	.91	1.17	
k	.028	.048	.71	1.22	1
L	.500		12.7	-	
a	45°	45°	45°	45°	3

- NOTES:

  1. Measured from maximum diameter of device.

  2. Leads having maximum diameter. O2!"

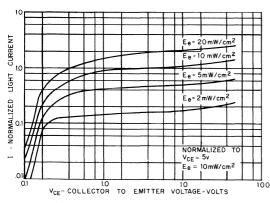
  (.533 mm) measured in gauging plane.054"

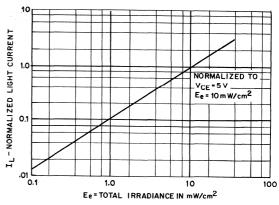
  +.00!"-.000(137 +.025-.000mm) below the reference plane of the device shall be within .007"(.778mm) their true position relative to maximum width tab.

  3. From centerline tab.

# L14C1, L14C2

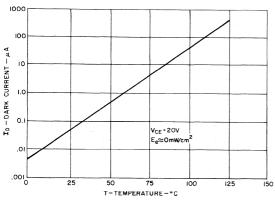
## TYPICAL ELECTRICAL CHARACTERISTICS

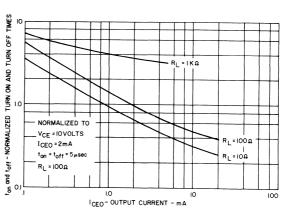




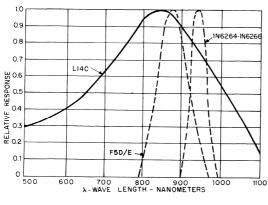
# LIGHT CURRENT VS COLLECTOR TO EMITTER VOLTAGE

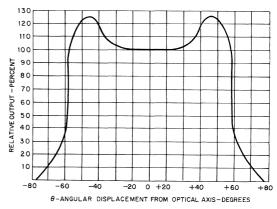
NORMALIZED LIGHT CURRENT VS RADIATION





**DARK CURRENT VS TEMPERATURE** 





**SPECTRAL RESPONSE** 

**ANGULAR RESPONSE CURVE** 

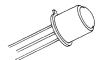
11

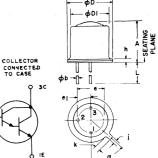
\*Derate 2.4 mW/°C above 25°C ambient. \*\*Derate 4.8 mW/°C above 25°C case.

# L14F1, L14F2

# **Light Detector Planar Silicon Photo-Darlington Amplifier**

The L14F1 and L14F2 are supersensitive NPN Planar Silicon Photo-Darlington Amplifiers. For many applications, only the collector and emitter leads are used; however, a base lead is provided to control sensitivity and the gain of the device. The L14F1 and L14F2 are mounted in a TO-18 style hermetically sealed packaged with lens cap and are designed to be used in optoelectronic sensing applications requiring very high sensitivity.





absolute maximum ratings	: (25°C) (unless otherwise specified)
VOLTAGES - DARK CHARACTERISTICS	

VOLTAGES - DARK CHARACTERISTICS			
Collector to Emitter Voltage	$V_{CEO}$	25	volts
Collector to Base Voltage	$V_{CBO}$	25	volts
Emitter to Base Voltage	$V_{EBO}$	12	volts
CURRENTS			
Light Current	$I_L$	200	mA
DISSIPATIONS			
Power Dissipation $(T_A = 25^{\circ}C)^*$	$P_{T}$	300	mW
Power Dissipation $(T_C = 25^{\circ}C)^{**}$	$\mathbf{P_T}$	600	$\mathbf{m}_{\mathbf{w}}^{\mathbf{w}}$
TEMPERATURES			
Junction Temperature	$T_{I}$	-55 to 150	°C
Storage Temperature	$T_{STG}$	-65 to 150	°C
Lead Soldering Time	Τ.	10 Seconds at 2	260°C

-	_	_		_	_	_		_		-	_		_		_				_	_	_	_	-	-		_		_	-
	ءاد	2	tr	ic	a۱	^	h	a r	20	to	ri	ct	ic	٥.	- (	21	50	C	10	un	ecc	: 01	the	r137	ise	sn	eci	fie	d)

 $T_{I}$ 

STATIC CHARACTERISTICS MIN. MAX. MIN. MAX. LIGHT CURRENT ( $V_{CE} = 5V, Ee\dagger = 0.2mW/cm^2$ ) $I_L$ 3 $-$ 1 $-$ mA DARK CURRENT ( $V_{CE} = 12V, I_B = 0$ ) $I_D$ $-$ 100 $-$ 100 nA EMITTER-BASE BREAKDOWN VOLTAGE ( $I_E = 100~\mu A$ ) $V_{(BR)EBO}$ 12 $-$ 12 $-$ V
$\begin{array}{cccccccccccccccccccccccccccccccccccc$
Dark current $(V_{CE}=12V,I_B=0) \hspace{1cm} I_D \hspace{1cm} -\hspace{1cm} 100 \hspace{1cm} -\hspace{1cm} 100 \hspace{1cm} nA$ emitter-base breakdown voltage
$ (V_{CE} = 12V, I_B = 0) \\ \text{EMITTER-BASE BREAKDOWN VOLTAGE} $ $ I_D \qquad - \qquad 100 \qquad - \qquad 100 \qquad nA $
EMITTER-BASE BREAKDOWN VOLTAGE
$(I_E = 100 \mu\text{A})$ $V_{(BR)EBO} 12 - 12 - V$
COLLECTOR-BASE BREAKDOWN VOLTAGE
$(I_C = 100 \mu\text{A})$ $V_{(BR)CBO} 25 - 25 - V$
COLLECTOR-EMITTER BREAKDOWN VOLTAGE
$(I_C = 10 \text{ mA})$ $V_{(BR)CEO} 25 - 25 - V$
SWITCHING CHARACTERISTICS (see Switching Circuit)
SWITCHING SPEEDS
$(V_{CC} = 10V, I_L = 10 \text{ mA}, R_L = 100 \Omega)$
DELAY TIME $t_d - 50 - 50 \mu sec$
RISE TIME $t_r - 300 - 300 \mu sec$
STORAGE TIME $t_s = 10 - 10 \mu sec$
FALL TIME $t_{\mathrm{f}}$ – 250 – 250 $\mu \mathrm{sec}$

<sup>†</sup>Ee = Radiation Flux Density. Radiation source is an unfiltered tungsten filament bulb at 2870° K color temperature.

NOTE: The 2870°K radiation is 25% effective on the photodarlington; i.e., a GaAs source of 0.05 mW/cm<sup>2</sup> is equivalent to this 0.2 mW/cm2 tungsten source.

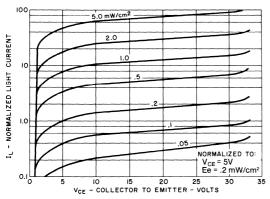
SYMBOL	INC	HES	MILLIN	ETERS	NOTE
3 I WIDOL	MIN.	MAX.	MIN.	MAX.	IVOIL
Α	.225	.255	5.71	6.47	
ΦЬ	.016	.021	407	533	
φD	.209	.230	5.31	5.84	
ΦDı	.178	.195	4.52	4.96	
e	.100	NOM		NOM	2
e <sub>1</sub>	.050	NOM	1,27	NOM	2
h		.030	_	.76	
]	.036	.046	.92	1.16	
k	.028	.048	.71	1.22	1
L	.500	-	12.7	_	
a	45°	45°	45°	45°	3

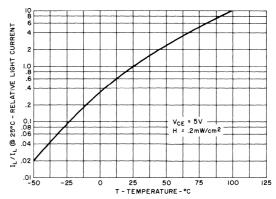
IOTES: Measured from maximum diameter of device. 1. Measured from maximum diameter, O2!"
2. Leads having maximum diameter, O2!"
(.533 mm) measured in gauging plane.054"
+.00!" -.000(137 +.025 -.000mm) below

1. Measured from maximum diameter, O2!"

he reference plane of the device shall be within .007"(.778mm) their true position relative to maximum width tab.

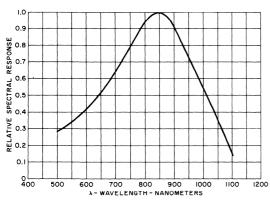


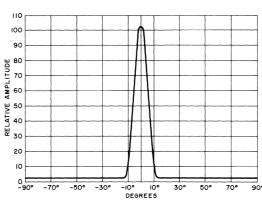




# 1. LIGHT CURRENT VS. COLLECTOR TO EMITTER VOLTAGE

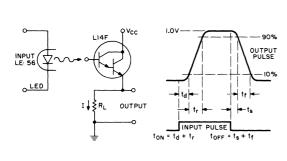
2. RELATIVE LIGHT CURRENT VS.
AMBIENT TEMPERATURE

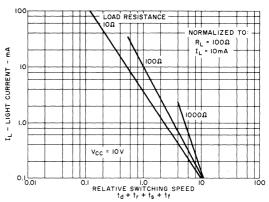




3. SPECTRAL RESPONSE CURVE

4. ANGULAR RESPONSE





5. TEST CIRCUIT AND VOLTAGE WAVEFORMS

6. LIGHT CURRENT VS. RELATIVE SWITCHING SPEED

11

# L14G1, L14G2, L14G3

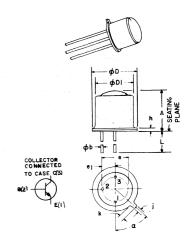
# **Light Detector Planar Silicon Phototransistor**

The L14G1 through L14G3 are highly sensitive NPN Planar Silicon Phototransistors. They are housed in a TO-18 style hermetically sealed package with lens cap. The L14G series is ideal for use in optoelectronic sensing applications where both high sensitivity and fast switching speeds are important parameters. Generally only the collector and emitter leads are used; a base lead is provided, however, to control sensitivity and gain of the device.

# absolute maximum ratings: (25°C unless otherwise specified)

Voltages — Dark Characteristics			
Collector to Emitter Voltage	$V_{CEO}$	45	volts
Collector to Base Voltage	$V_{CBO}$	45	volts
Emitter to Base Voltage	$V_{EBO}$	5	volts
Currents			
Light Current	IL	50	mA
Dissipations			
Power Dissipation $(T_A = 25^{\circ}C)^*$	$P_{T}$	300	mW
Power Dissipation (T <sub>C</sub> = 25°C)**	$P_{T}$	600	mW
Temperatures			_
Junction Temperature	$T_{J}$	-55 to 150	°C
Storage Temperature	T <sub>STG</sub>	- 65 to 150	°C
Lead Soldering Time	$T_L$	10 Seconds a	t 260°C

<sup>\*</sup>Derate 2.4 mW/OC above 25OC ambient



SYMBOL	INC	HES	MILLIN	NOTES	
31 MDUL	MIN.	MAX.	MIN.	MAY.	10.23
Α	.225	.255	5.71	6.47	
ΦЬ	.016	.021	407	533	
ΦD	.209	.230	5.31	5.84	
φDı	178	.195	4.52	4.96	
е	.100	NOM		NOM	2
e <sub>1</sub>	.050	NOM	1.27	NOM	2
h	-	.030	-	.76	
1	.036	.046	.92	1.16	
k	.028	.048	.71	1.22	1_1_
L	.500	-	12.7		L
a	450	45°	45°	45°	3

NOTES:

1. Measured from maximum diameter of device. (.533 mm) measured in gauging plane.054" +.001" -.000(137 +.025 -.000 mm) below the reference plane of the device shall be within .007"(.778 mm) their true position relative to maximum width tab.

3. From centerline tab.

# electrical characteristics: (25°C unless otherwise specified)

		L14	IG1	L14	G2	L14	G3
STATIC CHARACTERISTICS		MIN.	MAX.	MIN.	MAX.	MIN.	MAX.
Light Current							
$(V_{CE} = 5V, Ee^{\dagger} = 10mW/cm^2)$	IL	6		3		12	mA
Dark Current							
$(V_{CE} = 10V, Ee \approx 0)$	$I_D$		100		100		100nA
Emitter-Base Breakdown Voltage							
$(I_E = 100\mu A, I_C = 0, Ee \approx 0)$	$V_{(BR)EBO}$	5	5		5		V
Collector-Base Breakdown Voltage							
$(I_C = 100\mu A, I_E = 0, Ee \approx 0)$	$V_{(BR)CBO}$	45	45		45		V
Collector-Emitter Breakdown Voltage							
$(I_c = 10 \text{mA}, Ee \approx 0)$	$V_{(BR)CEO}$	45	45		45		V
Saturation Voltage							
$(I_C = 10\text{mA}, I_B = 1\text{mA})$	$V_{CE(SAT)}$		0.4		0.4		0.4
DYNAMIC CHARACTERISTICS			TYP.		TYP.		TYP.
Turn-On Time ( $V_{CE} = 10V$ , $I_C = 2mA$ ,	ton		8		8		8µsec
Turn-Off Time ( $R_L = 100\Omega$ )	t <sub>off</sub>		7		7		7µsec

<sup>†</sup>Ee = Radiation Flux Density. Radiation source is an unfiltered tungsten filament bulb at 2870°K color temperature.

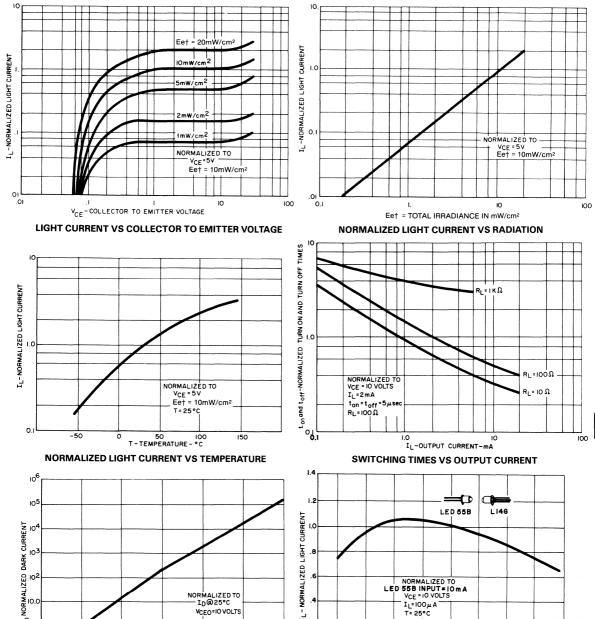
NOTE: A GaAs source of 3.0 mW/cm<sup>2</sup> is approximately equivalent to a tungsten source, at 2870° K, of 10 mW/cm<sup>2</sup>

<sup>\*\*</sup>Derate 4.8 mW/°C above 25°C case

# 11

# L14G1, L14G2, L14G3

#### TYPICAL ELECTRICAL CHARACTERISTICS



25 50 75 100
T-TEMPERATURE - °C

DARK CURRENT VS TEMPERATURE

125

150

1.0

NORMALIZED LIGHT CURRENT VS TEMPERATURE

Both Emitter (LED55B) and Detector

(L14G) at Same Temperature

5 25 45 T-TEMPERATURE-°C Ю5

## L14N1, L14N2

# **Light Detector High Sensitivity Phototransistor**

The L14N1 and L14N2 are NPN Silicon Phototransistors in a TO-18 style hermetically sealed package. The device has a top-looking flat lens cap and is ideally suited for applications requiring high sensitivity in the industrial control and alarm/detection markets. For phototransistor applications, the collector and emitter leads are used. The base lead is provided to control phototransistor sensitivity. For application flexibility, the device can also be used as a photodiode by using the collector and base leads.

# absolute maximum ratings: (25°C) unless otherwise specified

Voltages — Dark Characteristics			
Collector to Emitter Voltage	$v_{ceo}$	30	volts
Collector to Base Voltage	$V_{CBO}$	40	volts
Emitter to Base Voltage	$V_{EBO}$	5	volts
Currents			
Collector Current	$I_C$	50	mA
Emitter Current	IE	50	mA
Dissipations			
Power Dissipation (TA = 25°C)*	$P_{T}$	300	mW
Power Dissipation (T <sub>C</sub> = 25°C)**	$P_{T}$	600	mW
Temperatures			
Junction Temperature	$T_{I}$	-55 to 150	°C
Storage Temperature	$T_{STG}$	-65 to 150	°C
Lead Soldering Temperature	$T_{L}$	260	°C
(1/16" from case for 10 sec.)	<del>-</del>		

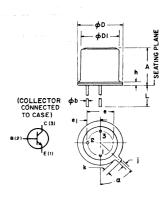
<sup>\*</sup>Derate 2.4 mW/°C above 25°C ambient \*\*Derate 4.8 mW/°C above 25°C ambient

# electrical characteristics: (25°C) unless otherwise specified

			L14N	1	- (	L14N	2	
STATIC CHARACTERISTICS		MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	
Photo Current								
$(V_{CE} = 5V, E_e = 5mW/cm^2)$ Phototransistor	$I_{L}$	3.0	6.0		6.0	10.0		mΑ
$(V_{CB} = 5V, E_e = 5mW/cm^2)$ Photodiode	$I_L$		5.0			5.0		$\mu A$
Dark Current								
$(V_{CE} = 10V, E_e \approx 0)$	$I_{CEO}$		6.0	100		10	100	nΑ
$(V_{CB} = 25V, E_e \approx 0)$	$I_{CBO}$		0.1	25		0.1	25	n <b>A</b>
Emitter-Base Breakdown Voltage								
$(I_E = 100 \mu A, I_C = 0, E_c \approx 0)$	V(BR)EBO	5	10		5	10		V
Collector-Base Breakdown Voltage								
$(I_C = 100 \mu A, I_E = 0, E_e \approx 0)$	V(BR)CBO	40	65		40	50		V
Collector-Emitter Breakdown Voltage								
$(I_C = 1 \text{ mA}, E_e \approx 0)$	V(BR)CEO	30	55		30	45		V
Pulse Width $\leq 300\mu sec$ ,								
Duty Cycle ≤ 1%)								
Beam Angle								
Beam Angle at 50% Amplitude	$\theta$		35			35		degrees
Saturation Voltage								-
$(I_C = 0.8 \text{ mA}, E_e = 10 \text{mW/cm}^2)$	V <sub>CE(SAT)</sub>		0.30	0.40				V
$(I_C = 1.6 \text{ mA}, E_e = 10 \text{mW/cm}^2)$	V <sub>CE(SAT)</sub>					0.25	0.40	v
SWITCHING CHARACTERISTICS								
Switching Speeds (Phototransistor)								
$(V_{CC} = 5V, I_C = 10 \text{ mA}, R_L = 100\Omega)$								
Rise Time	tr		10			14		μsec
Fall Time	t <sub>f</sub>		12			16		μsec
Tun Tine	, I		12			.0		µ3CC

E<sub>e</sub> = Radiation Flux Density. Radiation source is an unfiltered tungsten filament bulb at 2870°K color temperature. Note: A GaAs source of 3.0 mW/cm<sup>2</sup> is approximately equivalent to a tungsten source, at 2870°K, of 10 mW/cm<sup>2</sup>.





SYMBOL	INC	HES	MILLIA	NOTES	
3 I MOUL	MIN.	MAX.	MIN.	MAX.	VOICS
Α	-	210	-	5.34	
φь	.016	.021	406	.534	
φD	.209	.230	5.30	5.85	
ΦD1	.178	.195	4.52	4.96	
e	.100	NOM	2.54	NOM	2
e <sub>1</sub>	.050	NOM	1.27	NOM	2
h	-	.030	-	.76	
J	<b>£</b> 36	.046	.91	1.17	
k	.028	.048	.71	1.22	1
L	.500	_	12.7	-	
a	45°	450	45°	45°	3

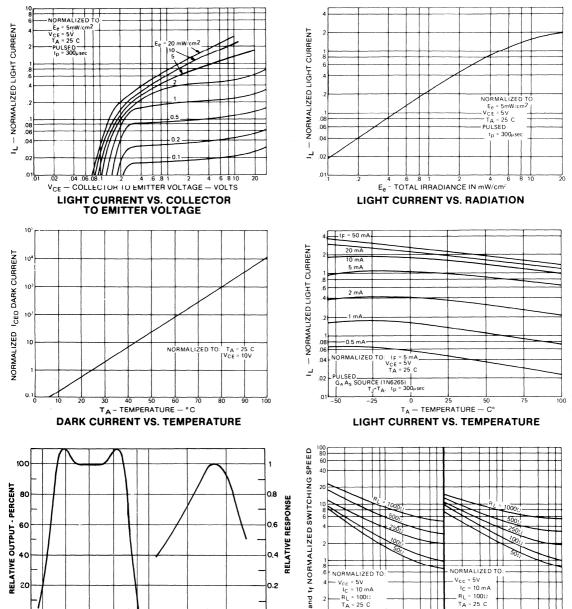
3. From centerline tab.

Measured from maximum diameter of device (.533 mm) measured in gauging plane.054' +.00!" -.000(137 + 025 -.000 mm) below the reference plane of the device shall be within .007"(,778mm) their true position relative to maximum width tab.

# L14N1, L14N2

#### TYPICAL ELECTRICAL CHARACTERISTICS

(Normalized to Specification Bias Points)



l٥

1100

**ANGULAR AND SPECTRAL RESPONSE** 

θ - ANGULAR DISPLACEMENT FROM OPTICAL AXIS

700

λ - WAVE LENGTH NANOMETERS

900

6 8 10

RL = 100Ω

TA = 25 C

**FALL TIME** 

ICE - OUTPUT CURRENT - mA

**SWITCHING SPEED VS. BIAS** 

TA = 25 C

**RISE TIME** 

\*Derate 2.4 mW/°C above 25°C ambient

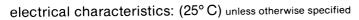
# L14P1, L14P2

# **Light Detector High Sensitivity Phototransistor**

The L14P1 and L14P2 are NPN Silicon Phototransistors in a TO-18 style hermetically sealed package. The device has a top-looking lens cap and is ideally suited for applications requiring high sensitivity in the industrial control and alarm/detection markets. For phototransistor applications, the collector and emitter leads are used. The base lead is provided to control phototransistor sensitivity. For application flexibility, the device can also be used as a photodiode by using the collector and base leads.

# absolute maximum ratings: (25°C) unless otherwise specified

Voltages — Dark Characteristics			
Collector to Emitter Voltage	$V_{CEO}$	30	volts
Collector to Base Voltage	$V_{CBO}$	40	volts
Emitter to Base Voltage	$V_{EBO}$	5	volts
Currents			
Collector Current	$I_{\mathbb{C}}$	50	mA
Emitter Current	$I_{E}$	50	mA
Dissipations			
Power Dissipation (T <sub>A</sub> = 25°C)*	$P_{T}$	300	mW
Power Dissipation (T <sub>C</sub> = 25°C)**	$P_{T}$	600	mW
Temperatures			
Junction Temperature	$T_{I}$	-55 to 150	°C
Storage Temperature	$T'_{STG}$	-65 to 150	°C
Lead Soldering Temperature	$T_L$	260	°C

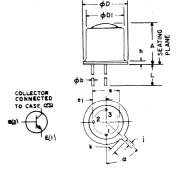


\*\*Derate 4.8 mW/°C above 25°C ambient

			L14P			L14P		
STATIC CHARACTERISTICS		MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	
Photo Current								
$(V_{CE} = 5V, E_e = 1mW/cm^2)$ Phototransistor	I <sub>1.</sub>	4.0	8.0		8.0	11.0		mA.
$(V_{CB} = 5V, E_e = 1mW/cm^2)$ Photodiode	${ m I}_{ m L}$		6.0			6.0		μΑ
Dark Current								
$(V_{CE} = 10V, E_e \approx 0)$	$I_{CEO}$		6.0	100		10.0		nΑ
$(V_{CB} = 25V, E_c \approx 0)$	$I_{CBO}$		0.1	25		0.1	25	nΑ
Emitter-Base Breakdown Voltage								
$(I_E = 100\mu A, I_C = 0, E_e \approx 0)$	$V_{(BR)EBO}$	. 5	10		5	10		V
Collector-Base Breakdown Voltage								2.0
$(I_C = 100 \mu A, I_E = 0, E_e \approx 0)$	V <sub>(BR)CBO</sub>	40	65		40	50		V
Collector-Emitter Breakdown Voltage								
$(I_C = 1 \text{ mA}, E_e \approx 0$	V <sub>(BR)CEC</sub>	30	55		30	45		V
Beam Angle								
Beam Angle at 50% Amplitude	$\theta$		12			12		degrees
Saturation Voltage								
$(I_C = 0.8 \text{ mA}, E_c = 2\text{mW/cm}^2)$	V <sub>CE(SAT)</sub>		0.30	0.40				V
$(I_C = 1.6 \text{ mA}, E_e = 2\text{mW/cm}^2)$	V <sub>CE(SAT)</sub>					0.25	0.40	V
SWITCHING CHARACTERISTICS								
Switching Speeds (Phototransistor)								
$(V_{CC} = 5V, I_C = 10 \text{ mA}, R_L = 100\Omega)$								
Rise Time	t <sub>r</sub>		10			14		μsec
Fall Time	tf		12			16		μsec

 $E_e$  = Radiation Flux Density. Radiation source is an unfiltered tungsten filament bulb at  $2870^{\circ}$  K color temperature. Note: A GaAs source of 3.0 mW/cm<sup>2</sup> is approximately equivalent to a tungsten source, at 2870°K, of 10 mW/cm<sup>2</sup>.





SYMBOL	INC	HES	MILLIN	METERS	NOTES
SIMBUL	MIN.	MAX.	MIN.	MIMA.	10123
Α	.225	.255	5.71	6.47	
ΦЬ	.016	.021	407	533	
ΦD	.209	.230	5.31	5.84	
<b>₫</b> D₁	.178	.195	4.52	4:96	
e	.100	NOM	2.54	NOM	2
e,	.050	NOM	1,27	NOM	2
h	-	.030	-	.76	
)	.036	.046	92	1.16	
k	.028	.048	.71	1.22	1 1
L	.500	_	12.7	_	
a	450	450	45°	45°	3

NOTES.

1. Meosured from maximum diameter of device

2. Leads having maximum diameter. 02!"

(.533 mm) measured in gauging plane.054"

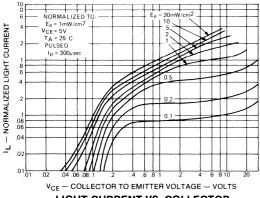
+.00!"-000(137 + 025 - 000mm) below the reference plane of the device shall be within .007"(.778 mm) their true position relative to maximum width tab.

<sup>3.</sup> From centerline tab.

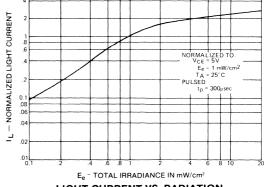
# L14P1, L14P2

### TYPICAL ELECTRICAL CHARACTERISTICS

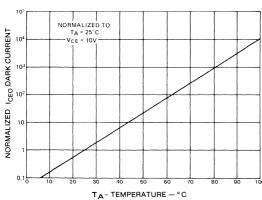
(Normalized to Specification Bias Points)



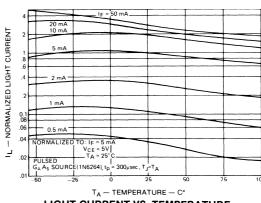
LIGHT CURRENT VS. COLLECTOR TO EMITTER VOLTAGE



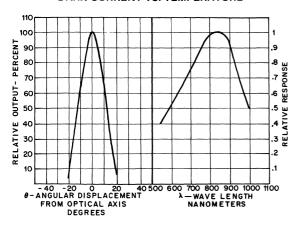
LIGHT CURRENT VS. RADIATION



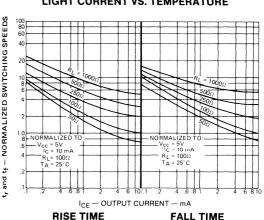
**DARK CURRENT VS. TEMPERATURE** 



LIGHT CURRENT VS. TEMPERATURE



ANGULAR AND SPECTRAL RESPONSE

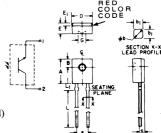


**RISE TIME FALL TIME SWITCHING SPEED VS. BIAS** 

### L14Q1

# **Light Detector Planar Silicon Phototransistor**

The L14Q1 Light Detector is an NPN planar silicon phototransistor. It is packaged in a side-looking clear epoxy encapsulant.



# absolute maximum ratings: (25°C) (unless otherwise specified)

VOLTAGES - Dark Characteristics Collector to Emitter Voltage	$V_{CEO}$	30	v
Emitter to Collector Voltage	V <sub>ECO</sub>	6	V
CURRENT Light Current (continuous)	I <sub>I</sub>	100	mA
<b>DISSIPATION</b> Power Dissipation $(T_A = 25^{\circ}C)^*$	$P_{T}$	150	mW
TEMPERATURES	•		
Junction Temperature	$T_J$	-55  to  + 100	°C
Storage Temperature	$T_{STG}$	-55  to  + 100	°C
Lead Soldering Temperature	$T_L$	260	°C
(5 seconds maximum, 1.6mm from	case)		

<sup>\*</sup>Derate 2.0mW/°C above 25°C ambient

SYM	MET	MILLI- METERS		INCHES		
	MIN	MAX	MIN	MAX		
A	5.59	5.80	.220	.228		
В	1.78	NOM.	.070	NOM.	2	
ρb	.60	.75	.024	.030	. 1	
b <sub>1</sub>	.51	NOM.	.020	NOM.	,	
D	4.45	4.70	.175	.185		
E	2.41	2.67	.095	.105		
Εı	.58	.69	.023	.027		
e	2.41	2.67	.095	.105	3	
G	1.98	NOM.	.078	NOM.	Į	
L	12.7		.500		1	
L <sub>1</sub>	1 40	1.65	055	.065	1	
s	.83	.94	033	.037	3	

- Two leads. Lead cross section dimensions uncon-trolled within 1.27 MM (.050") of seating plane. Centerline of active element located within .25 MM (.010") of true position.
- As measured at the seating plane Inch dimensions derived from millimeters

# electrical characteristics: (25°C)

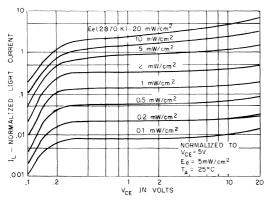
DETECTOR ONLY	SYMBOL	MIN.	TYP.	MAX.	UNITS
Light Current					
$(V_{CE} = 5V, E_e^{\dagger} = 5mW/cm^2 @ 2870^{\circ}K)$	$I_L$	1.0	4	_	mA
Dark Current					
$(V_{CE} = 25V, E_e = 0)$	$I_D$	-		100	nA
Beam Angle at Half Power Point					_
(Half angle)	$ heta_{ extsf{H}}$		30		Deg.
Saturation Voltage				0.4	• •
$(I_C = 0.5 \text{mA}, E_e = 2 \text{mW/cm}^2 @ 2870^{\circ} \text{K})$	$V_{CE(sat)}$		0.2	0.4	V
Collector-Emitter Breakdown Voltage					
$(I_C = 1mA)$	$V_{(BR)CEO}$	30		-	V
Emitter-Collector Breakdown Voltage					* 7
$(I_{\rm E} = 100\mu A)$	$V_{(BR)ECO}$	6	-	-	V
Collector-Emitter Capacitance				_	_
$(V_{CE} = 5V, f = 1MHz)$	$C_{ceo}$		3.3	5	pF
coupled characteristics					
Light Current					
$(V_{CE} = 5V, I_F = 20mA)$	$I_L$	***************************************	4	-	mA
Turn On Time					
$(V_{CC} = 5V, I_F = 30mA, R_L = 2.5k\Omega)$	t <sub>on</sub>		8		μs
Turn Off Time					
$(V_{CC} = 5V, I_F = 30mA, R_L = 2.5K\Omega)$	t <sub>off</sub>		50		μs

NOTE: Coupled electrical characteristics are measured using an F5F1 GaAs IRED at a separation distance of 4.0mm (.155 in.) with the lenses of the emitter and detector on a common axis within 0.1mm and parallel within 5°.

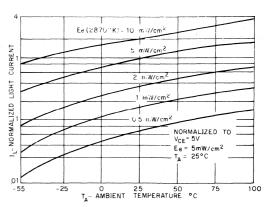
Ee = Radiation flux density. Radiation source is an unfiltered tungsten filament bulb at 2870° K color temperature.

The F5F940nm radiation is approximately 3 times more efficient than the 2870°K tungsten irradiance on this device. This means 1.5mW/cm² from the F5F is equivalent to the 5mW/cm² at 2870° K.

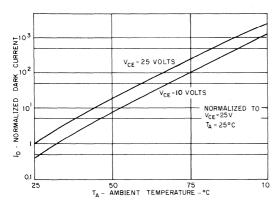
#### L14Q1



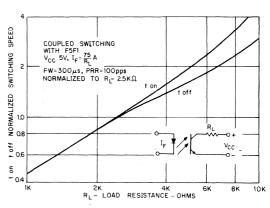
1. LIGHT CURRENT VS. COLLECTOR TO EMITTER VOLTAGE



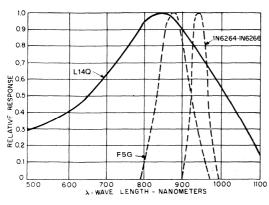
2. LIGHT CURRENT VS. AMBIENT TEMPERATURE



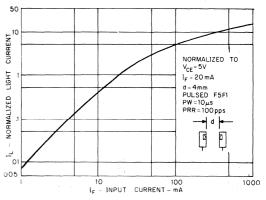
3. LEAKAGE CURRENT VS. TEMPERATURE



4. SWITCHING TIME VS. LOAD RESISTANCE



**5. SPECTRAL RESPONSE** 



6. COUPLED LIGHT CURRENT VS. F5F1 INPUT CURRENT

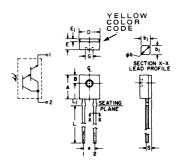
#### L14R1

# **Light Detector Planar Silicon Photo-Darlington Amplifier**

The L14R1 Light Detector is a planar silicon Darlington-connected Phototransistor. It is mounted in a side-looking clear epoxy encapsulated package.

# absolute maximum ratings: (25°C) (unless otherwise specified)

VOLTAGE (Dark characteristics) Collector to Emitter Voltage Emitter to Collector Voltage	$\begin{array}{c} \textbf{SYMBOL} \\ \textbf{V}_{\text{CEO}} \\ \textbf{V}_{\text{ECO}} \end{array}$	30 7	UNITS V V
CURRENT Light Current (continuous)	$I_{L}$	100	mA
<b>Dissipation</b> Power Dissipation $(T_A = 25^{\circ}C)^*$	$P_{T}$	150	mW
TEMPERATURES Junction Temperature Storage Temperature Lead Soldering Temperature (5 seconds maximum 1 6mm from ca	$T_{J}$ $T_{STG}$ $T_{L}$	-55 to +100 -55 to +100 260	°C °C



SYM	ME	LLI- TERS	INC	HES	NOTES
	MIN	MAX	MIN	MAX	
A	5.59	5.80	.220	.228	
В	1.78	NOM.	.070	NOM.	2
φb	.60	.75	.024	.030	1
b1	.51	NOM.	.020	NOM.	1
D	4.45	4.70	.175	.185	
E	2.41	2.67	.095	.105	
E <sub>1</sub>	.58	.69	.023	.027	
	2.41	2.67	.095	.105	3
G	1.98	NOM.	.078	NOM.	
L	12.7		.500		
L1	1.40	1.65	.065	.065	
S	.83	.94	.033	.037	3

- Two leads. Lead cross section dimensions uncontrolled within 1,27 MM (.050") of seating plane
- easured at the seating plane.

# electrical characteristics: (25°C)

DETECTOR ONLY	SYMBOL	MIN.	TYP.	MAX.	UNITS
Light Current					
$(V_{CE} = 1.5V, E_e^{\dagger} = 1 \text{mW/cm}^2 @ 2870^{\circ} \text{K})$	$I_L$	5	18		mA
Dark Current					
$(V_{CE} = 25V, E_e = 0)$	$I_{D}$	_	-	100	nA
Beam Angle at Half Power Point					
(Half Angle)	$\theta_{ m H}$	_	30		Deg.
Saturation Voltage					
$(I_C = 20 \text{mA}, E_e = 2 \text{mW/cm}^2 @ 2870 ^{\circ} \text{K})$	$V_{CE(sat)}$	-	.9	1.2	V
Collector-Emitter Breakdown Voltage					
$(\mathbf{I}_{\mathbf{C}} = 1  \mathbf{m} \mathbf{A})$	$V_{(BR)CEO}$	30		-	V
Emitter-Collector Breakdown Voltage					
$(I_{\rm E}=100\mu{\rm A})$	$V_{(BR)ECO}$	7	-		V
Collector-Emitter Capacitance					
$(V_{CE} = 5V, f = 1MHz)$	$C_{ceo}$		5	8	pF
coupled characteristics:					
Light Current					
$(V_{CE} = 1.5V, I_E = 5mA)$	$I_{I}$	-	18		mA
Turn On Time	-L				
$(V_{CC} = 5V, I_F = 10mA, R_I = 750\Omega)$	ton		45	_	μs
Turn Off Time	-01				F***
$(V_{CC} = 5V, I_F = 10mA, R_L = 750\Omega)$	t <sub>off</sub>	- :	250		μs

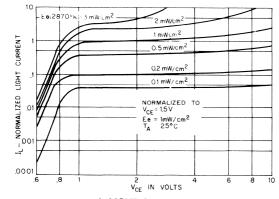
NOTE: Coupled electrical characteristics are measured using an F5F1 GaAs IRED at a separation distance of 4.0mm (.155 in.) with the lenses of the emitter and detector on a common axis within 0.1mm and parallel within 5°.

Ee = Radiation flux density. Radiation source is an unfiltered tungsten filament bulb at 2870° K color temperature.

The F5F940nm radiation is approximately 3 times more efficient than the 2870° K tungsten irradiance on this device. This means 0.3mW/cm<sup>2</sup> from the F5F is equivalent to the 1mW/cm<sup>2</sup> at 2870° K.

<sup>\*</sup>Derate 2.0mW/°C above 25°C ambient

### L14R1

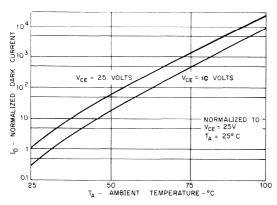


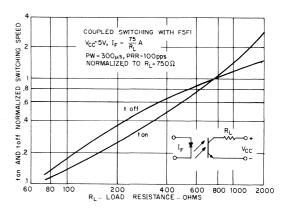
2 mW/cm<sup>2</sup> CURRECT 1 mWcm<sup>2</sup> LIGHT 0.5 mW/cm2 NORMALIZED 0.2 mW/cm<sup>2</sup> '0.1 mW/ cm<sup>2</sup> NORMALIZED TO VCE = 1.5 V Ee = 1mW/cm<sup>2</sup> T<sub>A</sub> = 25°C 01 ك .003 O 25 50 - AMBIENT TEMPERATURE - °C 75 100

Ee(2870°K)=3 mW/cm2

1. LIGHT CURRENT VS. COLLECTOR-EMITTER VOLTAGE

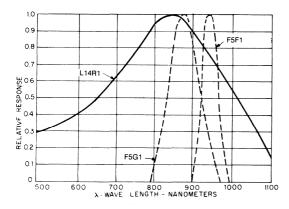
2. LIGHT CURRENT VS. AMBIENT TEMPERATURE

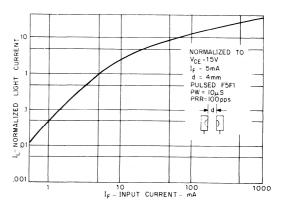




3. LEAKAGE CURRENT VS. TEMPERATURE

4. SWITCHING TIME VS. LOAD RESISTANCE





5. SPECTRAL RESPONSE

6. COUPLED LIGHT CURRENT VS. F5F1 INPUT CURRENT

# 4N25, 4N25A, 4N26, 4N27, 4N28

# **Optoisolator**

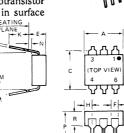
# GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The 4N25, 4N25A, 4N26, 4N27, 4N28 devices consist of a gallium arsenide infrared emitting diode coupled with a silicon phototransistor in a dual-in-line package. These devices are also available in surface mount packaging.

#### **FEATURES:**

- · Fast switching speeds
- · High DC current transfer ratio
- High isolation resistance
- Meets or exceeds all JEDEC registered specifications
- I/O compatible with integrated circuits

†Parameters are JEDEC registered values.



	SYMBOL	MILLIM	MILLIMETERS		INCHES		
	STIVIBUL	MIN.	MAX.	MIN.	MAX.	NOTES	
	А	8.38	8.89	.330	.350		
	8	7.62	REF.	.300	REF.	1 1	
	С		8.64		.340	2	
	D	.406	.508	.016	.020		
	. E	-	5.08		.200	3	
	F	1.01	1.78	.040	.070		
	G	2.28	2.80	.090	.110		
	_ H		2.16	-	.085	4	
	J	.203	.305	.008	.012		
	K	2.54	-	.100	-		
	м	-	15		15		
	N	.381	-	.015			
. †	Р	-	9.53	-	.375		
s	R	2.92	3.43	.115	.135		
Ĭ	S	6.10	6.86	.240	.270		
t							

- NOTES:
- 1. INSTALLED POSITION LEAD CENTERS
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE
- 4. FOUR PLACES.

# absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE			PHOTO TRANSISTOR		
†Power Dissipation	*150	milliwatts	†Power Dissipation	**150	milliwatts
†Forward Current (Continuous)	80	milliamps	†VCEO	30	volts
†Forward Current (Peak)	3	ampere	†VCBO	70	volts
(Pulse width 300 usec 2% duty cycle)		•	†VECO	7	volts
†Reverse Voltage	3	volts	Collector Current (Continuous)	100	milliamps
*Derate 2.0mW/°C above 25°C a	ambient		**Derate 2.0mW/°C above 25°	C ambient	

TOTAL DEVICE	
Storage Temperature -55 to 150°C  Operating Temperature -55 to 100°C  Lead Soldering Time (at 260°C) 10 seconds  Power Dissipation @ TA = 25°C. PD 250mW  Derate 3.3mW,°C above 25°C ambient	Surge Isolation Voltage (Input to Output) 3535V(peak) 2500V(RMS) Steady-State Isolation Voltage (Input to Output) 3180V(peak) 2250V(RMS)

# individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS	PHOTO TRANSISTOR	MIN.	TYP.	MAX.	UNITS
†Forward Voltage - VF	1.1	1.5	volts	†Breakdown Voltage – V <sub>(BR)</sub> CEO	30	-	-	volts
$(I_F = 10\text{mA})$				$(I_C = 1 \text{mA}, I_F = 0)$ †Breakdown Voltage – $V(BR)CBO$ $(I_C = 100 \mu A, I_F = 0)$	70	-	-	volts
†Reverse current - IR	-	100	microamps	†Breakdown Voltage - V <sub>(BR)ECO</sub>	7	-	-	volts
$(V_R = 3V)$				$(I_E = 100 \mu A, I_F = 0)$ †Collector Dark Current $I_{CEO}$ 4N25-27 $(V_{CE} = 10V, I_F = 0)$ 4N28	-	5 -	50 100	nanoamps nanoamps
Capacitance - C <sub>J</sub> (V = O, f = 1MHz)	50	-	picofarads	†Collector Dark Current – I <sub>CBO</sub> (V <sub>CB</sub> = 10V, I <sub>F</sub> = 0)	-	2	20	nanoamps

# coupled electrical characteristics (25°C)

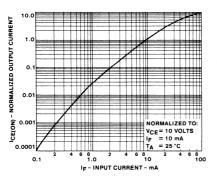
		MIN.	TYP.	MAX.	UNITS
†DC Current Transfer Ratio (IF = 10mA, VCE = 10V)	4N25, 4N25A, 4N26	20		-	%
	4N27, 4N28	10	-	-	%
†Saturation Voltage - Collector - Emitter (IF = 50mA, IC = 2mA)		-	0.1	0.5	volts
Resistance - IRED to Photo-Transistor (@ 500 volts)		-	100	-	gigaohms
Capacitance - IRED to Photo-Transistor (@ 0 volts, f = 1MHz)		-	1	-	picofarad
Rise/Fall Time ( $V_{CE} = 10V$ , $I_{CE} = 2mA$ , $R_{L} = 100\Omega$ )		-	2	-	microseconds
Rise/Fall Time ( $V_{CB} = 10V$ , $I_{CB} = 50\mu A$ , $R_{L} = 100\Omega$ )		- '	300	-	nanoseconds

N Covered under U.L. component recognition program, reference file E51868

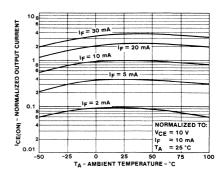
VDE Approved to 0883/6.80 0110b Certificate #35025, except type 4N28

## 4N25-4N28

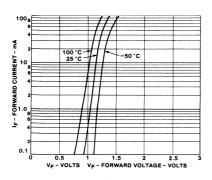
#### TYPICAL CHARACTERISTICS



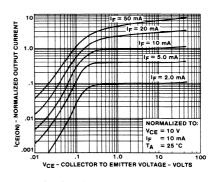
**OUTPUT CURRENT VS INPUT CURRENT** 



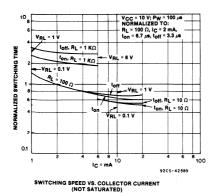
**OUTPUT CURRENT VS TEMPERATURE** 



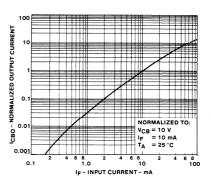
INPUT CHARACTERISTICS



**OUTPUT CHARACTERISTICS** 



**SWITCHING TIMES VS OUTPUT CURRENT** 



OUTPUT CURRENT (I<sub>CBO</sub>) VS INPUT CURRENT

# 4N29, 4N29A, 4N30, 4N31, 4N32, 4N32A, 4N33

# **Optoisolator**

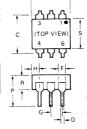
GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier

The 4N29 through 4N33 devices consist of a gallium arsenide infrared emitting diode coupled with a silicon photo-Darlington amplifier in a dual-in-line package. These devices are also available in surface mount packaging.

#### **FEATURES:**

- High DC current transfer ratio
- High isolation resistance
- · Meets or exceeds all JEDEC registered specifications
- I/O compatible with integrated circuits

†Parameters are JEDEC registered values.



	SYMBOL	MIN.	MAX.	MIN.	MAX.	
	А	8.38	8.89	.330	.350	
	В	7.62	REF.	.300	REF.	1
	С	m.s	8.64	_	.340	- 2
	D	.406	.508	.016	.020	
	E	-	5.08	-	.200	3
_	F	1.01	1.78	.040	.070	
	G	2.28	2.80	.090	.110	
	н		2.16	-	.085	4
	J	.203	.305	.008	.012	
_	К	2.54		.100		
	м		15		15	
	N	.381		.015		
	Р	-	9.53		.375	
	R	2.92	3.43	.115	.135	
	s	6.10	6.86	.240	.270	
	MOTEC.					

INCHES

NOTES:

- . INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.

MILLIMETERS

 THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE. 1 4, FOUR PLACES.

# absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE			PHOTO TRANSISTOR		
†Power Dissipation	*150	milliwatts	†Power Dissipation	**150	milliwatts
†Forward Current (Continuous)	80	milliamps	†VCEO	30	volts
†Forward Current (Peak)	3	ampere	†V <sub>CBO</sub>	30	volts
(Pulse width 300µsec 2% duty cycle)			†VEBO	5	volts
†Reverse Voltage	3	volts	Collector Current (Continuous)	100	milliamps
*Derate 2.0mW/°C above 25°C a	ambient		**Derate 2.0mW/°C above 25	°C ambient	

TOTAL DEVICE	
Storage Temperature -55 to 150°C	Surge Isolation Voltage (Input to Output)
Operating Temperature -55 to 100°C	3535V(peak) 2500V(RMS)
Lead Soldering Time (at 260°C) 10 seconds	Steady-State Isolation Voltage (Input to Output)
Power Dissipation @ T <sub>A</sub> = 25°C. PD 250mW	3180V <sub>(peak)</sub> 2250V <sub>(RMS)</sub>
Derate 3.3mW/°C above 25°C ambient	(Fully) (Tulle)

# individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS	PHOTO DARLINGTON	MIN.	TYP.	MAX.	UNITS
†Forward Voltage - VF (IF = 10mA)	1.2	1.5	volts	†Breakdown Voltage – $V_{(BR)}$ CBO (IC = 100µA, IF = 0)	30	-	-	volts
†Reverse current – Ip	_	100	microamps	†Breakdown Voltage – V(BR)CEO (IC = 1mA, IF = 0)	30	-	-	volts
$(V_R = 3V)$			pc	†Breakdown Voltage - V(BR)EBO (IE = 100µA, IF = 0)	5	-	-	volts
Capacitance - C <sub>J</sub> (V = O, f = 1MHz)	50	-	picofarads	†Collector Dark Current - I <sub>CEO</sub> (V <sub>CE</sub> = 10V, I <sub>F</sub> = O)	-	-	100	nanoamps

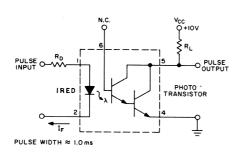
# coupled electrical characteristics (25°C)

		MIN.	TYP.	MAX.	UNITS
†Collector Output Current (IF = 10mA, VCE = 10V)	4N32, 4N32A, 4N33	50	_	-	mA
· · ·	4N29, 4N29A, 4N30	10	-	-	mA
	4N31	5	-	l -	mA
†Saturation Voltage - Collector - Emitter	4N29, 29A, 30, 32, 32A, 33	~	-	0.1	volts
$(I_F = 50 \text{mA}, I_C = 2 \text{mA})$	4N31	~	-	1.2	volts
Resistance - IRED to Photo-Transistor (@ 500 volts)		-	100	-	gigaohms
Capacitance - IRED to Photo-Transistor (@ 0 volts, f = 1M	Hz)	~	1	-	picofarad
†Switching Speeds (IC = 50mA, IF = 200mA					
Turn-On Time - ton			-	5	microseconds
Turn-Off Time - toff	4N29, 4N29A, 4N30, 4N31	-	-	40	microseconds
Turn-Off Time - toff	4N32, 4N32A, 4N33		-	100	microseconds

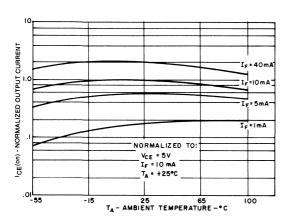
Na Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate #35025

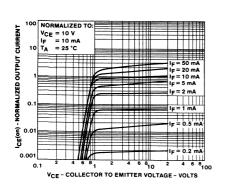
# 12



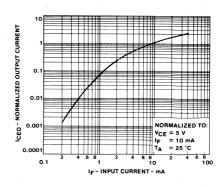
#### SWITCHING TIME TEST CIRCUIT



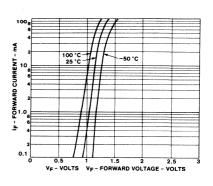
**OUTPUT CURRENT VS TEMPERATURE** 



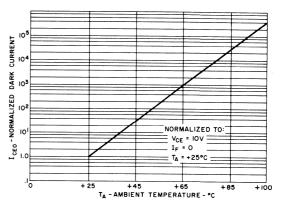
**OUTPUT CHARACTERISTICS** 



**OUTPUT CURRENT VS INPUT CURRENT** 



INPUT CHARACTERISTICS



NORMALIZED DARK CURRENT VS TEMPERATURE

# 4N35, 4N36, 4N37

# **Optoisolator**

# **GaAs Infrared Emitting Diode and NPN Silicon Phototransistor**

The 4N35, 4N36, 4N37 are gallium arsenide infrared emitting diodes coupled with a silicon phototransistor in a dual in-line package. These devices are also available in surface-mount packaging.

#### **FEATURES:**

- · Fast switching speeds
- · High DC current transfer ratio
- · High isolation resistance
- · Meets or exceeds all JEDEC registered specifications
- I/O compatible with integrated circuits

# absolute maximum ratings: (25°C) (unless otherwise specified)

#### INFRARED EMITTING DIODE

	Power Dissipation	$T_A = 25$ °C	<b>100</b>	milliwatts
*	Power Dissipation	$T_C = 25$ °C	<b>☆100</b>	milliwatts
	(T <sub>C</sub> indicates coll-	ector lead temper	ature 1/32" fr	om case)
*	Forward Current (Co	ntinuous)	60	milliamps
*	Forward Current (Pea	ık)	3	ampere
	(Pulse width 1 use	c, 300 pps)		
٠	Reverse Voltage		6	volts

☆Derate 1.33mW/°C above 25°C

#### PHOTO-TRANSISTOR

<ul> <li>Power Dissipation</li> </ul>	$T_A = 25$ °C	☆☆3 <b>0</b> 0	milliwatts
<ul> <li>Power Dissipation</li> </ul>	$T_C = 25$ °C	ቱሱሱ500	milliwatts
(T <sub>C</sub> indicates coll	ector lead tempe	erature 1/32" f	rom case)
<ul> <li>V<sub>CEO</sub></li> </ul>		30	volts
<ul> <li>V<sub>CBO</sub></li> </ul>		70	volts
<ul> <li>v<sub>ECO</sub></li> </ul>		7	volts
* Collector Current (Co	ontinuous)	100	milliamps
		0-	

☆ Derate 4.0mW/°C above 25°C ফার্ম Derate 6.7mW/°C above 25°C

#### **TOTAL DEVICE**

- \* Storage Temperature -55 to 150°C
- \* Operating Temperature -55 to 100°C
- \* Lead Soldering Time (at 260°C) 10 seconds
- Relative Humidity 85% @ 85°C

Surge Isolation Voltage (Input to Output) 3535V(peak) 2500V(RMS)

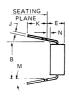
Steady-State Isolation Voltage (Input to Output) 2250V(RMS)

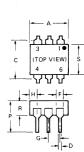
3180V(peak)

\* Indicates JEDEC registered values

Na Covered under U.L. component recognition program, reference file E51868 VDE Approved to 0883/6.80 0110b Certificate #35025, except type 4N37







SYMBOL	MILLIN	IETERS	INC	HES	NOTES
STIVIBUL	MIN.	MAX.	MIN.	MAX.	NO.ES
Α	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
С		8.64	-	.340	2
D	.406	.508	.016	.020	
E	-	5.08	-	.200	3
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
н	-	2.16		.085	4
J	.203	.305	.008	.012	
K	2.54	-	.100	-	
M:	- 1	15		15	
N	.381	-	.015		
Ρ	-	9.53	-	.375	
R .	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	

- NOTES: 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE
- 4. FOUR PLACES



#### 4N35-4N37

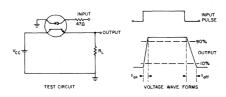
# individual electrical characteristics (25°C) (unless otherwise specified)

INFRARED EMITTING	SYMBOL	MIN.	MAX.	UNITS	PHOTO-TRANSISTOR	SYMBOL	MIN.	TYP.	MAX.	UNITS
* Forward Voltage (I <sub>F</sub> = 10 mA)	$v_{\rm F}$	.8	1.5	volts	* Breakdown Voltage (I <sub>C</sub> = 10 mA, I <sub>F</sub> = 0)	V <sub>(BR)</sub> CEO	30	-	-	volts
* Forward Voltage (IF = 10 mA)	v <sub>F</sub>	.9	1.7	volts	* Breakdown Voltage (I <sub>C</sub> = 100uA, I <sub>F</sub> = O)	V(BR) CBO	70	-	-	volts
T <sub>A</sub> = -55°C  * Forward Voltage	$v_{\mathrm{F}}$	.7	1.4	volts	* Breakdown Voltage (I <sub>E</sub> = 100uA, I <sub>F</sub> = O)	V(BR) ECO	7	-	-	volts
$(I_F = 10 \text{ mA})$ $T_A = +100^{\circ}\text{C}$					Collector Dark Current (V <sub>CE</sub> = 10V, I <sub>F</sub> = O)	ICEO	-	5	50	nanoamps
* Reverse Current (V <sub>R</sub> = 6V)	IR	-	10	microamps	* Collector Dark Current (VCF = 30V, IF = 0)	ICEO	_	1.	500	microamps
Capacitance (V=O, f=1 MHz)	СЈ		100	picofarads	$T_{A} = 100^{\circ} C$ Capacitance $(V_{CE} = 10V, f = 1MHz)$	$c_{CE}$	_	2	-	picofarads

# coupled electrical characteristics (25°C) (unless otherwise specified)

	MIN.	TYP.	MAX.	UNITS
* DC Current Transfer Ratio (I <sub>F</sub> = 10mA, V <sub>CE</sub> = 10V)	100	-	-	%
* DC Current Transfer Ratio (I <sub>F</sub> = 10mA, V <sub>CE</sub> = 10V) T <sub>A</sub> = -55°C	40	-	-	%
* DC Current Transfer Ratio (I <sub>F</sub> = 10mA, V <sub>CE</sub> = 10V) T <sub>A</sub> = +100°C	40	-	-	%
* Saturation Voltage-Collector To Emitter (I <sub>F</sub> = 10mA, I <sub>C</sub> = 0.5mA)	_	-	0.3	volts
* Input to Output Isolation Current (Pulse Width = 8 msec)				
(See Note 1) Input to Output Voltage = 3550 V <sub>(peak)</sub> 4N35	-	-	100	microamps
Input to Output Voltage = 2500 V <sub>(peak)</sub> 4N36	-	-	100	microamps
Input to Output Voltage = 1500 V <sub>(peak)</sub> 4N37	-		100	microamps
<ul> <li>Input to Output Resistance (Input to Output Voltage = 500V - See Note 1)</li> </ul>	100	-	-	gigaohms
* Input to Output Capacitance (Input to Output Voltage = 0, f = 1MHz - See Note 1)	-	-	2	picofarads
* Turn on Time $t_{on}$ (V <sub>CC</sub> = 10V, $I_{C}$ = 2MA, $R_{L}$ = 100 $\Omega$ ) (See Figure 1)	_	5	10	microseconds
* Turn off Time – $t_{off}$ (V <sub>CC</sub> = 10V, I <sub>C</sub> = 2MA, R <sub>L</sub> = 100 $\Omega$ ) (See Figure 1)		. 5	10	microseconds

Note 1: Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together

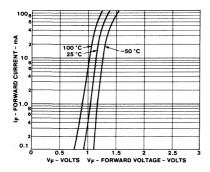


Adjust Amplitude of Input Pulse for Output (I<sub>C</sub>) of 2 mA

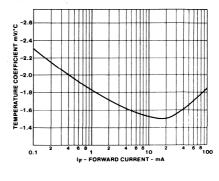
FIGURE 1

<sup>\*</sup> Indicates JEDEC registered values.

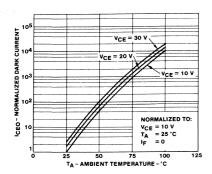
#### 4N35-4N37



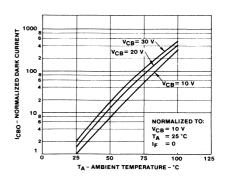
1. INPUT CHARACTERISTICS



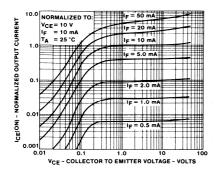
2. FORWARD VOLTAGE TEMPERATURE COEFFICIENT



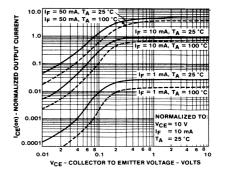
3. DARK ICEO CURRENT VS TEMPERATURE



4. ICBO VS TEMPERATURE



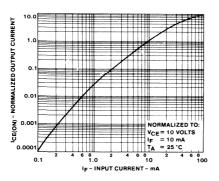
5. OUTPUT CHARACTERISTICS



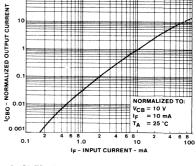
6. OUTPUT CHARACTERISTICS

# 12

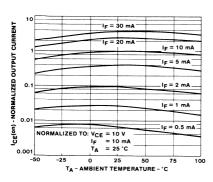
#### TYPICAL CHARACTERISTICS



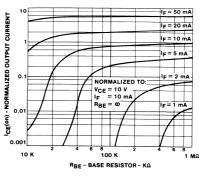
7. OUTPUT CURRENT VS INPUT CURRENT



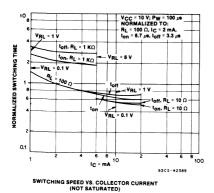
8. OUTPUT CURRENT — COLLECTOR TO BASE VS INPUT CURRENT



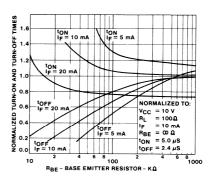
9. OUTPUT CURRENT VS TEMPERATURE



10. OUTPUT CURRENT VS BASE EMITTER RESISTANCE



11. SWITCHING TIMES VS OUTPUT CURRENT



12. SWITCHING TIME VS RBE

# 4N38, 4N38A

# **Optoisolator**

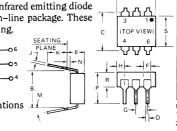
# GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The 4N38 and 4N38A consist of a gallium arsenide infrared emitting diode coupled with a silicon phototransistor in a dual-in-line package. These devices are also available in surface mount packaging.

#### **FEATURES:**

- · Fast switching speeds
- High DC current transfer ratio
- · High isolation resistance
- Meets or exceeds all JEDEC registered specifications
- I/O compatible with integrated circuits

†Parameters are JEDEC registered values.



	STIVIBUL	MIN.	MAX.	MIN.	MAX.	NOTES
	A	8.38	8.89	.330	.350	
	В	7.62	REF.	.300	REF.	1
	С		8.64	_	.340	2
	D	.406	.508	.016	.020	
-	E	-	5.08		.200	3
	F	1.01	1.78	.040	.070	
3	G	2.28	2.80	.090	.110	
L	н	-	2.16	-	.085	4
	J	.203	.305	.008	.012	
	K	2.54	-	.100	-	
	M		15		15	
	N	.381	-	.015	-	
	P	-	9.53	-	.375	
	R	2.92	3.43	.115	.135	
	S	6.10	6.86	.240	.270	

INCHES

MILLIMETERS

- NOTES:
- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES.

# absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE			PHOTO TRANSISTOR		
†Power Dissipation	*150	milliwatts	†Power Dissipation	**150	milliwatts
†Forward Current (Continuous)	80	milliamps	†V <sub>CEO</sub>	80	volts
†Forward Current (Peak)	3	ampere	†VCBO	80	volts
(Pulse width 300µsec 2% duty cycle)			†VECO	7	volts
†Reverse Voltage	3	volts	Collector Current (Continuous)	100	milliamps
*Derate 2.0mW/°C above 25°C ambient			**Derate 2.0mW/°C above 25°	C ambient	

TOTAL DEVICE	
Storage Temperature -55 to 150°C Operating Temperature -55 to 100°C Lead Soldering Time (at 260°C) 10 seconds Power Dissipation @ TA = 25°C. PD 250mW Derate 3.3mW/°C above 25°C ambient	Surge Isolation Voltage (Input to Output) 3535V(peak) 2500V(RMS) Steady-State Isolation Voltage (Input to Output) 3180V(peak) 2250V(RMS)

# individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS	PHOTO TRANSISTOR	MIN.	TYP.	MAX.	UNITS
†Forward Voltage - VF (IF = 10mA)	1.2	1.5	volts	†Breakdown Voltage – V <sub>(BR)</sub> CEO (I <sub>C</sub> = 1mA, I <sub>F</sub> = 0)	80	-	-	volts
(IF - IONIA)				tBreakdown Voltage - $V(BR)CBO$ (IC = 1 $\mu$ A, IF = 0)	80	-	-	volts
†Reverse current – I <sub>R</sub> (V <sub>R</sub> = 3V)	-	100	microamps	†Breakdown Voltage – V <sub>(BR)ECO</sub> (I <sub>E</sub> = 100 µA, I <sub>F</sub> = 0)	7	-		volts
			-	†Collector Dark Current - ICEO (VCE = 10V, IF = 0)	-	-	50	nanoamps
Capacitance - C <sub>J</sub> (V = O, f = 1MHz)	50	-	picofarads	†Collector Dark Current - I <sub>CBO</sub> (V <sub>CB</sub> = 60V, I <sub>F</sub> = O)	-	-	20	nanoamps

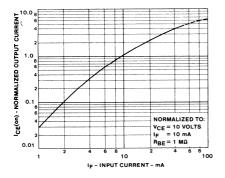
# coupled electrical characteristics (25°C)

	MIN.	TYP.	MAX.	UNITS
†Saturation Voltage - Collector - Emitter (IF = 20mA, IC = 4mA)	-	-	1.0	volts
Resistance - IRED to Photo-Transistor (@ 500 volts)	-	100	-	gigaohms
Capacitance - IRED to Photo-Transistor (@ 0 volts, f = 1MHz)	-	1	-	picofarad
DC Current Transfer Ratio (IF = $10$ mA, $V_{CE} = 100\Omega$ )	10		-	%
Switching Speeds $V_{CE} = 10V$ , $I_{C}$ , $= 2mA$ , $R_{L} = 100\Omega$ )				
Turn-On Time - ton	-	5	-	microseconds
Turn-Off Time - t <sub>off</sub>	-	5	-	microseconds

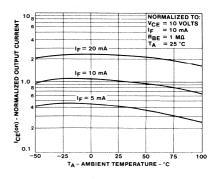
Na Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate #35025, except type 4N38A

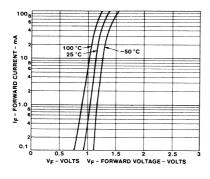
#### TYPICAL CHARACTERISTICS



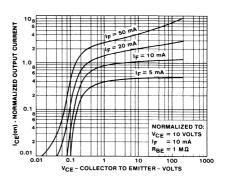
#### 1. OUTPUT CURRENT VS INPUT CURRENT



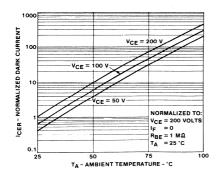
#### 2. OUTPUT CURRENT VS TEMPERATURE



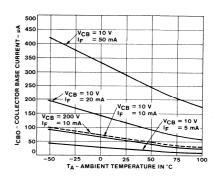
3. INPUT CHARACTERISTICS



### 4. OUTPUT CHARACTERISTICS



5. NORMALIZED DARK CURRENT VS TEMPERATURE



6. COLLECTOR BASE CURRENT VS TEMPERATURE

# 4N39, 4N40 **Optoisolator**

# **GaAs Infrared Emitting Diode and Light Activated SCR**

The 4N39 and 4N40 consist of a gallium arsenide, infrared emitting diode coupled with a light activated silicon controlled rectifier in a dual-in-line package. These devices are also available in surface mount packaging. Meets or exceeds all JEDEC registered specifications.

# absolute maximum ratings

INFRARED EMITTING DIODE		
†Power Dissipation (-55°C to 50°C)	*100	milliwatts
†Forward Current (Continuous)	60	milliamps
(-55°C to 50°C) †Forward Current (Peak) (-55°C to 50°C)	1	
(100 µsec 1% duty cycle)	1	ampere
†Reverse Voltage (-55°C to 50°C)	6	volts
*Derate 2.0mW/°C above 50°C.		

PHOTO-SCR			
†Off-State and Reverse Voltage	4N39	200	volts
(-55°C to +100°C)	4N40	400	volts
†Peak Reverse Gate Voltage (-55	°C to 50°C)	6	volts
†Direct On-State Current (-55°C	to 50°C)	300	milliamps
†Surge (non-rep) On-State Curre	nt (100µsec)	10	amps
(-55°C to 50°C)			-
†Peak Gate Current (-55°C to 50	°C)	10	milliamps
†Output Power Dissipation (-55°		*400	milliwatts
**Doroto 8mW/°C abo	110 50°C		

SYMBOL	MILLIM	ETERS	INC	INCHES	
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
А	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
c		8.64		.340	2
D	.406	.508	.016	.020	
E	-	5.08	-	.200	3
F	1.01	1.78	.040	.070	1
G	2.28	2.80	.090	.110	
н	-	2.16	-	.085	4
J	203	.305	.008	.012	
к	2.54		.100	-	
M		15		15	
N	.381		.015	-	
Р		9.53		.375	
R	2.92	3.43	.115	.135	
s	6.10	6.86	.240	.270	

1. INSTALLED POSITION LEAD CENTERS

- 2 OVERALL INSTALLED DIMENSION.
- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES.

#### **TOTAL DEVICE**

†Storage Temperature Range -55°C to 150°C

†Operating Temperature Range -55°C to 100°C †Normal Temperature Range (No Derating) -55°C to 50°C

†Soldering Temperature (1/16" from case, 10 seconds) 260°C

†Total Device Dissipation (-55°C to 50°C), 450 milliwatts

†Linear Derating Factor (above 50°C), 9.0mW/°C

†† Surge Isolation Voltage (Input to Output).

3535V(peak) 2500V(RMS)

†† Steady-State Isolation Voltage (Input to Output).

3180V(peak) 2250V(RMS)

### individual electrical characteristics (25°C) (unless otherwise specified)

INFRARED EMITTIN	G DIODE	TYP.	MAX.	UNITS
†Forward Voltage (I <sub>F</sub> = 10mA)	$V_{\mathbf{F}}$	1.1	1.5	volts
†Reverse Current (V <sub>R</sub> = 3V)	I <sub>R</sub>	_	10	microamps
Capacitance (V = O,f = 1 MHz)	$C_{J}$	50	-	picofarads

PHOTO-SCR		MIN.	MAX.	UNITS
†Peak Off-State Voltage - VD	M 4N39	200	_	volts
$(R_{GK} = 10K\Omega, T_A = 100^{\circ}C)$	) 4N40	400	_	volts
†Peak Reverse Voltage - VRM	4N39	200	-	volts
$(T_A = 100^{\circ}C)$	4N40	400	-	volts
†On-State Voltage - V <sub>T</sub>		l –	1.3	volts
$(I_T = 300 \text{mA})$		1	1	
†Off-State Current - ID	4N39	-	50	microamps
$(V_D=200V,T_A=100^{\circ}C,I_F=O,R_C$	(K=10K)		l	
†Off-State Current - ID	4N40	l –	150	microamps
$(V_D=400V,T_A=100^{\circ}C,\tilde{I}_F=O,R_0$	<sub>3K</sub> =10K)	l		_
†Reverse Current - IR	4N39	_	50	microamps
$(V_R = 200V, T_A = 100^{\circ}C, I_F$	= O)	1		•
†Reverse Current - IR	4N40	_	150	microamps
$(V_R = 400V, T_A = 100^{\circ}C, I_F$	= O)	1		•
†Holding Current - IH		_	1.0	milliamps
$(V_{FX} = 50V, R_{GK} = 27K\Omega)$				

# coupled electrical characteristics (25°C)

FT		30	milliamps
FT		14	milliamps
io	100	_	gigaohms
on		50	microseconds
	500	-	volts/microsec.
-		2	picofarads
	FT io	FT - 100 on -	FT   -   14   14   100   -   50   -

†Indicates JEDEC Registered Values. Nu Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate # 35025

†† Exceeds JEDEC registered values

# 4N39, 4N40

#### TYPICAL CHARACTERISTICS

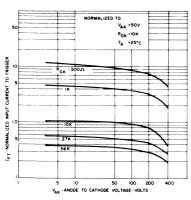


FIGURE 1. INPUT CURRENT TO TRIGGER VS. ANODE-CATHODE VOLTAGE

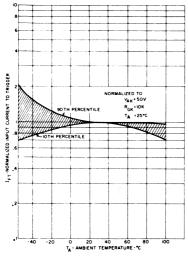


FIGURE 3. INPUT CURRENT TO TRIGGER DISTRIBUTION VS. TEMPERATURE

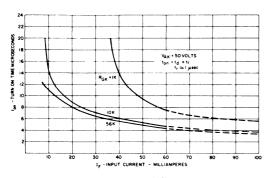


FIGURE 5. TURN-ON TIME VS. INPUT CURRENT

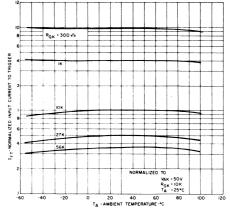


FIGURE 2. INPUT CURRENT TO TRIGGER VS. TEMPERATURE

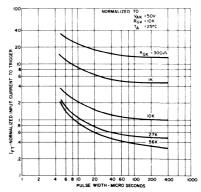


FIGURE 4. INPUT CURRENT TO TRIGGER VS. PULSE WIDTH

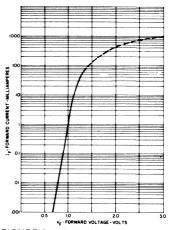


FIGURE 6. INPUT CHARACTERISTICS  $I_F$  VS.  $V_F$ 

## 4N39, 4N40

#### TYPICAL CHARACTERISTICS OF OUTPUT (SCR)

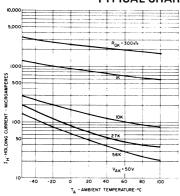


FIGURE 7. HOLDING CURRENT VS. TEMPERATURE

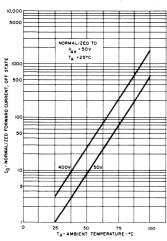


FIGURE 9. OFF-STATE FORWARD CURRENT VS. TEMPERATURE

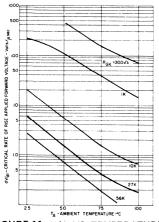


FIGURE 11. dv/dt VS. TEMPERATURE

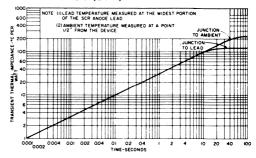


FIGURE 8. MAXIMUM TRANSIENT THERMAL IMPEDANCE

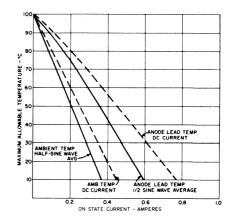


FIGURE 10. ON-STATE CURRENT VS. MAXIMUM ALLOWABLE TEMPERATURE

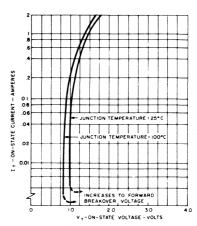


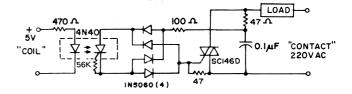
FIGURE 12. ON-STATE CHARACTERISTICS

# 12

#### TYPICAL APPLICATIONS

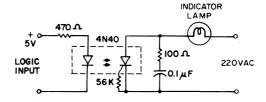
#### 10A, T2L COMPATIBLE, SOLID STATE RELAY

Use of the 4N40 for high sensitivity, 2500V isolation capability, provides this highly reliable solid state relay design. This design is compatible with 74, 74S and 74H series T<sup>2</sup>L logic systems inputs and 220V AC loads up to 10A.



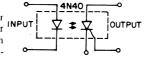
#### 25W LOGIC INDICATOR LAMP DRIVER

The high surge capability and non-reactive input characteristics of the 4N40 allow it to directly couple, without buffers,  $T^2L$  and DTL logic to indicator and alarm devices, without danger of introducing noise and logic glitches.

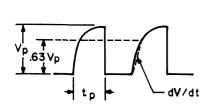


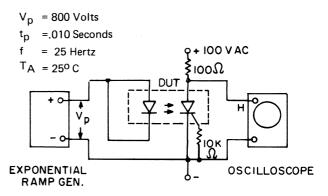
#### 400V SYMMETRICAL TRANSISTOR COUPLER

Use of the high voltage PNP portion of the 4N40 provides a 400V transistor capable of conducting positive and negative signals with current transfer ratios of over 1%. This function is useful in remote instrumentation, high voltage power supplies and test equipment. Care should be taken not to exceed the 400 mW power dissipation rating when used at high voltages.



# FIGURE 13 COUPLED dv/dt — TEST CIRCUIT



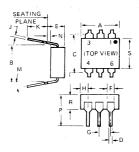


# H11A1, H11A2, H11A3, H11A4, H11A5

# Optoisolator GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The H11A1 through H11A5 consist of a gallium arsenide infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. These devices are also available in surface-mount packaging.





# absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1 µsec 300 P Ps)		
Reverse Voltage	3	volts
*Derate 1.33mW/°C above	25°C ambient	

PHOTO-TRANSISTOR		
Power Dissipation	**150	milliwatts
$V_{CEO}$	30	volts
$V_{CBO}$	70	volts
$V_{ECO}$	7	volts
Collector Current (Continuous)	100	milliamps
**Derate 2.0mW/°C above 2	5°C ambient	•

SYMBOL	MILLIM	ETERS	INC	HES	NOTES
SYMBOL	MIN.	MAX.	MIN.	MAX.	INCIES
Α	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
С	-	8.64		.340	2
D	.406	.508	.016	.020	
Е		5.08	-	.200	3
F	1.01	1.78	.040	.070	ĺ
G	2.28	2.80	.090	.110	
н	-	2.16		.085	. 4
J	.203	.305	.008	.012	l
К	2.54		.100	-	
M		15		15	
N	.381	-	.015		
Р	-	9.53		.375	
R	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	

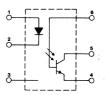
#### NOTES

- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE. 4, FOUR PLACES.

#### TOTAL DEVICE

Storage Temperature -55 to 150°C
Operating Temperature -55 to 100°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output).
3535V<sub>(peak)</sub> 2500V<sub>(RMS)</sub>
Steady-State Isolation Voltage (Input to Output).
3180V<sub>(peak)</sub> 2250V<sub>(RMS)</sub>





# 12

# H11A1, H11A2, H11A3, H11A4, H11A5

# individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage $-V_F$ ( $I_F = 10 \text{ mA}$ )	1.1	1.5	volts
Reverse Current $-I_R$ $(V_R = 3 V)$	-	10	microamps
Capacitance - C <sub>J</sub> (V = O,f = 1 MHz)	50	-	picofarads

PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage- $V_{(BR)CEO}$ ( $I_C = 10$ mA, $I_F = 0$ )	30		-	volts
Breakdown Voltage- $V_{(BR)CBO}$ ( $I_C = 100\mu A, I_F = 0$ )	70			volts
Breakdown Voltage- $V_{(BR)ECO}$ ( $I_E = 100\mu A, I_F = O$ )	7	-	_	volts
Collector Dark Current $-I_{CEO}$ ( $V_{CE} = 10V, I_{E} = 0$ )	-	5	50	nanoamps
Capacitance $(V_{CE} = 10V, f = 1MHz)$	-	2	MARINA	picofarads

# coupled electrical characteristics (25°C)

		MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio (I <sub>E</sub> = 10mA, V <sub>CE</sub> = 10V)	HIIAL	50		-	%
	H11A2	20	-		%
	H11A3	20	-	_	%
	H11A4	10	_	_	%
	H11A5	30	_	_	%
Saturation Voltage – Collector to Emitter ( $I_F = 10\text{mA}$ , $I_C = 0.5\text{mA}$ )		_	0.1	0.4	volts
Isolation Resistance (Input to Output Voltage = $500V_{DC}$ )		100	_	-	gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1MHz)		-		2	picofarads
Switching Speeds:					
Rise/Fall Time ( $V_{CE} = 10V$ , $I_{CE} = 2mA$ , $R_L = 100\Omega$ )		_	2	_	microseconds
Rise/Fall Time ( $V_{CB} = 10V$ , $I_{CB} = 50\mu A$ , $R_L = 100\Omega$ )		_	300	_	nanoseconds

#### **†DETAILS OF VDE 0884 APPROVAL**

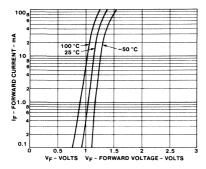
Class: DIN VDE 0109/12.83 Table 1

OPERATING VOLTAGE	CLASSIFICATION
V <sub>LINE</sub> < 300V <sub>RMS</sub>	Class I – IV
V <sub>LINE</sub> < 600V <sub>RMS</sub>	Class I – III
Max. operating voltage = 630 <sub>RMS</sub>	
Max. transient overvoltage = 6000V	
Partial discharge test voltage = 1000V	
Partial discharge max value at test voltage = 5 picocoulomb	

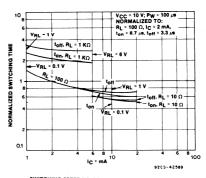
The optoisolator provides safe electrical isolation only when used within its maximum ratings. To guarantee safe operation, external circuitry must provide safe limits to the energy applied to the optoisolator. (Refer to Chapter 6: Safety.)

# H11A1, H11A2, H11A3, H11A4, H11A5

#### TYPICAL CHARACTERISTICS

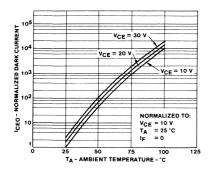


1. INPUT CHARACTERISTICS

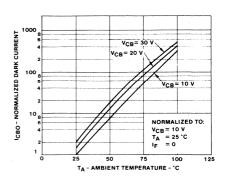


SWITCHING SPEED VS. COLLECTOR CURRENT (NOT SATURATED)

# 2. SWITCHING SPEED VS. COLLECTOR CURRENT (NOT SATURATED)



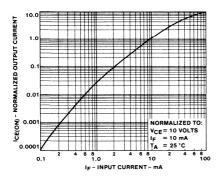
3. DARK ICEO CURRENT VS TEMPERATURE



4. I<sub>CBO</sub> VS TEMPERATURE

# H11A1, H11A2, H11A3, H11A4, H11A5

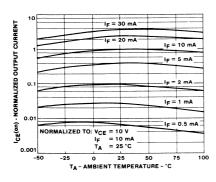
### TYPICAL CHARACTERISTICS

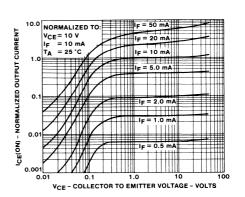


0.001 2 4 6 8 2 4 6 8 2 4 6 8 100 Ip- INPUT CURRENT - MA

#### 5. OUTPUT CURRENT VS INPUT CURRENT

6. OUTPUT CURRENT — COLLECTOR TO BASE VS INPUT CURRENT





7. OUTPUT CURRENT VS TEMPERATURE

8. OUTPUT CHARACTERISTICS

#### H11A10

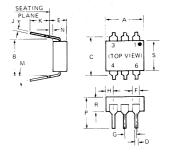
# Optoisolator GaAs Infrared Emitting Diode and NPN Silicon Phototransistor Current Threshold Switch



The H11A10 is a gallium arsenide infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. It is characterized and specified with two resistors, one on the input and one on the output. This configuration provides a circuit which will detect a doubling of the input current level by registering more than a twenty-to-one difference in the output current over a wide temperature range. This device is also available in surface-mount packaging.

#### **FEATURES:**

- Programmable Threshold "off" to "on" with a 2/1 change in input current
- Glass Dielectric Isolation
- Fast Switching Speeds
- Operation over wide temperature range
- High Noise Immunity



INCHES

340

15

375

MIN. MAX

.330 .350 .300 REF.

.016 .020

1.78 .040 .070 2.80 .090 .110 2.16 ~ .085 .305 .008 .012

.115 .135

MILLIMETERS

8.89

8.64

15 -9.53

INSTALLED POSITION LEAD CENTERS.
 OVERALL INSTALLED DIMENSION.

.508

MIN MAX

8.38

406

1.01

2.92

Ď

# absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE		,	
Power Dissipation	$T_A = 25^{\circ}C$	*100	milliwatts
Power Dissipation	$T_{\rm C} = 25^{\rm o}{\rm C}$	*100	milliwatts
Forward Current (Continuous)	_	50	milliamps
Forward Current (Peak)			•
(Pulse width 1 µsec, 300 pps)		3	ampere
Reverse Voltage		6	volts
*Derate 1.33mW/°C above 25°C			

PHOTO-TRANSISTOR	-	
Power Dissipation Power Dissipation (T <sub>C</sub> indicates collector lead	$T_A = 25^{\circ}C$ **300 $T_C = 25^{\circ}C$ ***500 temperature 1/32" from	milliwatts
VCEO VCBO VEBO Collector Current (Continuous)	30 70 7	volts volts volts milliamps
**Derate 4.0mW/°C above 25°C  ***Perate 6.7mW/°C above 25°C	100	mmamps

SEA	ESE MEASUREMENTS ATING PLANE. JR PLACES.	ARE MADE FR	ОМ ТНЕ
2 - 1		6	
R <sub>1</sub> 2	字	5	}
3		4	

THRESHOLD SWITCH BIAS CIRCUIT ILLUSTRATION

#### TOTAL DEVICE

Storage Temperature -55 to 150°C
Operating Temperature -55 to 100°C
Lead Soldering Time (at 260°C) 10 seconds
Input to Output Isolation Voltage
Surge Isolation (Input to Output)
3535V (peak) 2500V (RMS)

Steady-State Isolation Voltage (Input to Output)

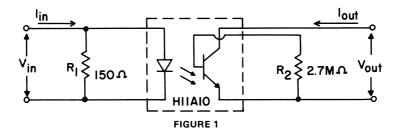
3180V<sub>(peak)</sub> 2250V<sub>(RMS)</sub>

Nu Covered under U.L. Component Recognition Program, reference file E51868

### H11A10

## individual electrical characteristics (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE	SYMBOL	MIN.	MAX.	UNITS	PHOTO-TRANSISTOR	SYMBOL	MIN.	TYP.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> =10mA)	$V_{\mathrm{F}}$		1.5	volts	Breakdown Voltage (I <sub>C</sub> =10mA, I <sub>F</sub> =0)	V <sub>(BR)CEO</sub>	30	-		volts
Reverse Current (V <sub>R</sub> =6V)	I <sub>R</sub>	-	10	microamps	Breakdown Voltage (I <sub>C</sub> =100μA, I <sub>F</sub> =0)	V <sub>(BR)CBO</sub>	70	_	-	volts
Capacitance (V=0, f=1 MHz)	CJ		100	picofarads	Breakdown Voltage (I <sub>E</sub> =100μA, I <sub>F</sub> =0)	V <sub>(BR)EBO</sub>	7	_		volts



### THRESHOLD CIRCUIT CHARACTERISTICS - BIAS PER FIGURE 1

(-55°C to 100°C Unless Otherwise Specified)

SYMBOL	PARAMETER/CONDITIONS	MIN.	TYP.	MAX.	UNITS
I <sub>out</sub>	Output Current ( $V_{out}=10V$ , $I_{in} \le 5mA$ , $T_A=25^{\circ}C$ )		1	50	nanoamperes
I <sub>out</sub>	Output Current ( $V_{out}$ =10V, $I_{in} \le 5mA$ , $T_A$ =100°C)		1	50	microamperes
I <sub>out</sub> I <sub>in</sub> V <sub>out</sub>	D.C. Current Transfer Ratio $(V_{out}=10V, I_{in} \ge 10mA)$ Output Saturation Voltage $(I_{in}=10mA, I_{out}=0.5mA)$	10	30 0.2	0.4	percent volts
R <sub>io</sub>	Input to Output Resistance (V <sub>io</sub> =500V) Note 1	100	-		gigaohms
t <sub>on</sub>	Turn-On Time (Vcc = 10V, $I_{in}$ =20 mA, $R_L$ =100 $\Omega$ ) Figure 2		5		microseconds
t <sub>off</sub>	Turn-Off Time (Vcc = 10V, $I_{in}$ =20mA, $R_L$ =100 $\Omega$ ) Figure 2		5		microseconds

Note 1: Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together

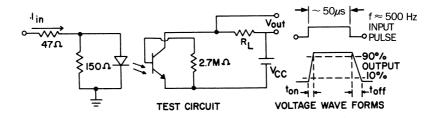
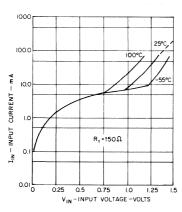
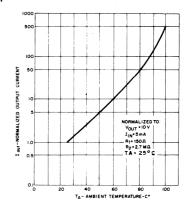


FIGURE 2 - TEST CIRCUIT AND VOLTAGE WAVEFORMS

### H11A10

### TYPICAL CHARACTERISTICS BIASED PER FIGURE 1

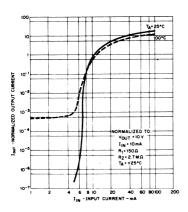


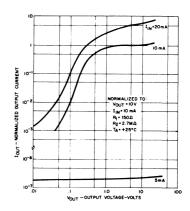


3. INPUT

4. LEAKAGE

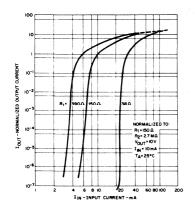
### PROGRAMMING AND TRANSFER CHARACTERISTICS

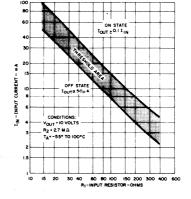




### 5. TEMPERATURE

### 6. INPUT CURRENT





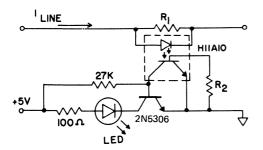
#### 7. THRESHOLDING

### 8. PROGRAMMING

H11A10

#### THRESHOLD COUPLER APPLICATIONS

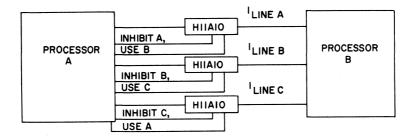
## LINE CURRENT MONITORS LINE DROPOUT ALARM LIGHT

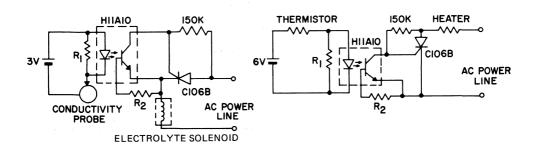


When remote line current ( $I_{\rm LINE}$ ) falls below the programmed threshold value the LED turns on, indicating loss of power to critical, isolated circuit function. Phase inversion, accomplished by replacing the 2N5306 with a D41K1 PNP and interchanging the collector and emitter connections, provides an over-current alarm light.

#### INFORMATION FLOW DIRECTOR

To minimize lines needed to communicate between A and B, a queue system is set up using H11A10's to monitor line use and set up the queue procedures.





In many process control applications such as solution mixing, resistor trimming, light control and temperature control, it is advantageous to monitor conductivity with isolated low voltages and transmit this information to a power control or logic system. Low voltages are often preferred for safety, convenience or self heating considerations or to prevent ground loops and provide noise immunity. Until the advent of the H11A10 such systems were complex and costly. Using the H11A10 allows the use of simple low power circuits such as illustrated here to provide these functions. In battery operated systems, the low current thresholds of the H11A10 can considerably enhance battery life.

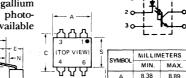
## **Optoisolator**

## **GaAs Infrared Emitting Diode and NPN Silicon Phototransistor**

The H11A520, H11A550 and H11A5100 consist of a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual-in-line package. These devices are also available in surface-mount packaging. PLANE K



- High isolation voltage, 5000V minimum.
- · Unique patented glass isolation construction.
- High efficiency liquid epitaxial IRED.
- · High humidiy resistant silicone encapsulation.
- · Fast switching speeds.





SYMBOL	MILLIMETERS INCHES		HES	NOTES	
STIVIDUL	MIN.	MAX.	MIN.	MAX.	WOTES
А	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
С	-	8.64		.340	2
D	.406	.508	.016	.020	1 1
E	-	5.08		.200	3
· F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
· H	-	2.16	-	.085	4
J	.203	.305	.008	.012	
К	2.54	-	.100	-	
M	-	15		15	
N	.381		.015		
P	-	9.53	-	.375	
R.	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	

## absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE		
Power Dissipation $-T_A = 25^{\circ}C$	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	amperes
(Pulse width 1 µsec, 300 pps)		
Reverse Voltage	6	volts
*Derate 1.33mW/°C above 2	25°C.	

### PHOTO-TRANSISTOR

Power Dissipation $-T_A = 25^{\circ}C$	**300	milliwatts
$V_{CEO}$	30	volts
$V_{CBO}$	70	volts
$V_{ m EBO}$	7	volts
Collector Current (Continuous)	100	milliamps
**Derate 4.0mW/°C above		

- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE
- SEATING PLANE. 4. FOUR PLACES

### TOTAL DEVICE

Storage Temperature -55 to 150°C. Operating Temperature -55 to 100°C. Lead Soldering Time (at 260°C) 10 seconds. Surge Isolation Voltage (Input to Output). 5656V<sub>(peak)</sub> 4000V(RMS)

Steady-State Isolation Voltage (Input to Output). 5300V<sub>(DC)</sub> 3750V<sub>(RMS)</sub>

## individual electrical characteristics (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE	MIN.	MAX.	UNITS
Forward Voltage – V <sub>F</sub>	.8	1.5	volts
$(I_F = 10 \text{mA})$ Forward Voltage $-V_F$	.9	17	volts
$(I_F = 10\text{mA})$		1/	TOILS
$T_A = -55^{\circ}C$			
Forward Voltage $-V_F$ $(I_F = 10\text{mA})$	.7	1.4	volts
$T_A = +100^{\circ}C$		1	
Reverse Current – I <sub>R</sub>	-	10	microamps
$(V_R = 6V)$			
Capacitance $-C_J$ (V = O,f = 1 MHz)	-	100	picofarads
( , ,,, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1	i	

PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - V <sub>(BR)CEO</sub>	30	-	_	volts
$(I_C = 10 \text{mA}, I_F = 0)$ Breakdown Voltage $-V_{(BR)CBO}$	70	_	_	volts
$(I_C = 100\mu A, I_F = O)$ Breakdown Voltage $-V_{(BR)EBO}$	7	-	_	volts
$(I_E = 100\mu A, I_F = O)$ Collector Dark Current $-I_{CEO}$ $(V_{CE} = 10V, I_F = O)$	- ,	5	50	nano-
$(V_{CE} = 10V, I_F = 0)$ Collector Dark Current $-I_{CEO}$ $(V_{CE} = 10V, I_F = 0)$	_	-	500	amps micro- amps
$T_A = 100^{\circ}C$ Capacitance $-C_{CE}$ $(V_{CF} = 10V, f = 1MHz)$	_	2		pico- farads

No Covered under U.L. component recognition program, reference file E51868

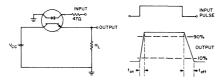
VDE Approved to 0883/6.80 0110b Certificate #35025

## coupled electrical characteristics (25°C) (unless otherwise specified)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_F = 10\text{mA}$ , $V_{CE} = 10\text{V}$ ) H11A510	100		_	%
H11A550	50		_	%
H11A520	20	-	-	%
Saturation Voltage — Collector to Emitter (I <sub>F</sub> = 20mA, I <sub>C</sub> = 2mA)	-	-	0.4	volts
Isolation Resistance (Input to Output Voltage = 500V <sub>DC</sub> . See Note 1)	100	-	_	gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1 MHz. See Note 1)	-		2.0	picofarads
Turn-On Time $-t_{on}$ ( $V_{CC} = 10V$ , $I_{C} = 2mA$ , $R_{L} = 100\Omega$ ). (See Figure 1)	-	5	10	microseconds
Turn-Off Time $-t_{off}$ ( $V_{CC} = 10V$ , $I_C = 2mA$ , $R_L = 100\Omega$ ). (See Figure 1)	_   -	5	10	microseconds

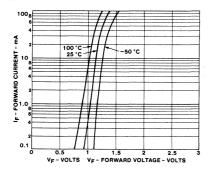
### NOTE 1:

Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together.

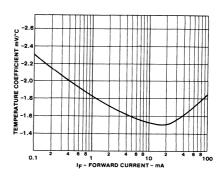


Adjust Amplitude of Input Pulse for Output ( $I_C$ ) of 2mA

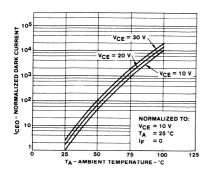
### TYPICAL CHARACTERISTICS



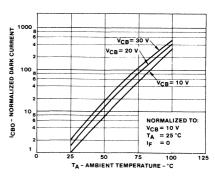
1. INPUT CHARACTERISTICS



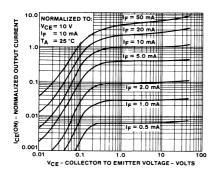
2. FORWARD VOLTAGE TEMPERATURE COEFFICIENT



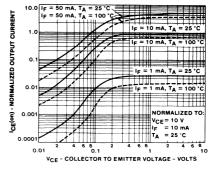
3. DARK ICEO CURRENT VS TEMPERATURE



4. OUTPUT CURRENT VS TEMPERATURE

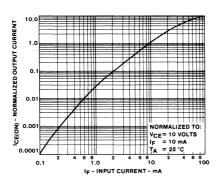


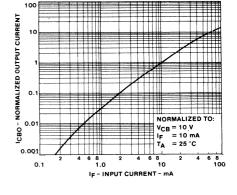
5. OUTPUT CHARACTERISTICS



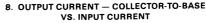
6. OUTPUT CURRENT VS BASE EMITTER RESISTANCE

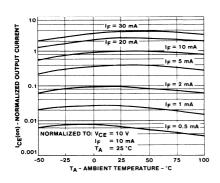
### TYPICAL CHARACTERISTICS

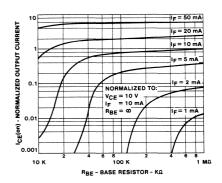




### 7. OUTPUT CURRENT VS. INPUT CURRENT

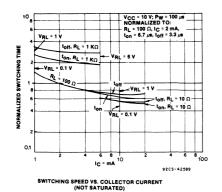


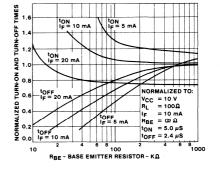




### 9. OUTPUT CURRENT VS. TEMPERATURE

10. OUTPUT CURRENT VS. BASE EMITTER RESISTANCE





11. SWITCHING SPEED VS. COLLECTOR CURRENT (NOT SATURATED)

12. SWITCHING TIME VS.  $R_{BE}$ 

# Optoisolator AC Input GaAs Infrared Emitting Diodes and NPN Silicon Phototransistor



The H11AA1 through H11AA4 consist of two gallium arsenide infrared emitting diodes connected in inverse parallel and coupled with a silicon phototransistor in a dual in-line package. These devices are also available in surface-mount packaging.

#### **FEATURES:**

- AC or polarity insensitive inputs
- Fast switching speeds
- Built-in reverse polarity input protection
- High isolation voltage
- High isolation resistance
- I/O compatible with integrated circuits

## absolute maximum ratings: (25°C) (unless otherwise specified)

### **INFRARED EMITTING DIODE**

Power Dissipation  $T_A = 25^{\circ}\text{C}$  \*100 milliwatts Power Dissipation  $T_C = 25^{\circ}\text{C}$  \*100 milliwatts  $(T_C \text{ indicates collector lead temperature } 1/32^{\circ}\text{ from case})$  Input Current (RMS) 60 milliamps Input Current (Peak)  $\pm$  1 ampere (Pulse width  $1\mu\text{sec}$ , 300 pps)

\*Derate 1.33mW/oC above 25oC

#### **PHOTO-TRANSISTOR**

Power Dissipation Power Dissipation	$T_A = 25^{\circ}C$ **300 $T_C = 25^{\circ}C$ ***500	milliwatts milliwatts
(T <sub>C</sub> indicates collector lead		
$V_{CEO}$	30	volts
$V_{CBO}$	70	volts
$V_{ m EBO}$	5	volts
Collector Current (Continuous)	) 100	milliamps

\*\*Derate 4.0mW/°C above 25°C \*\*\*Derate 6.7mW/°C above 25°C

SYMBOL	MILLIMETERS		INC	NOTES	
STIVIBUL	MIN.	MAX.	MIN.	MAX.	NOTES
А	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
С	-	8.64	-	.340	2
D	.406	.508	.016	.020	
E	- 1	5.08	144	.200	3
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
н	-	2.16		.085	4
J	.203	.305	.008	.012	
K	2.54		.100	100	
M	-	15		15	
N	.381	-	.015		]
Ρ	-	9.53		.375	1
R	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	

#### NOTES:

- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION:
- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES

### TOTAL DEVICE

Storage Temperature -55 to 150°C
Operating Temperature -55 to 100°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output)
2500V<sub>(peak)</sub> 1770V<sub>(RMS)</sub>
Steady-State Isolation Voltage (Input to Output)
1500V<sub>(peak)</sub> 1060V<sub>(RMS)</sub>

Na Covered under U.L. component recognition program, reference file E51868

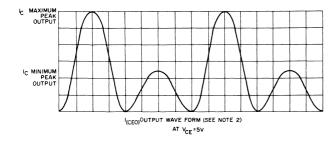
## individual electrical characteristics (25°C) (unless otherwise specified)

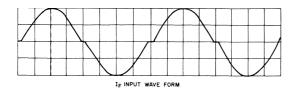
INFRARED EMITTING DIODE	SYMBOL	MAX.	UNITS	PHOTO-TRANSISTOR	SYMBOL	MIN.	MAX.	UNITS
Input Voltage (I <sub>F</sub> = ± 10 mA)	$V_{\mathrm{F}}$		·	Breakdown Voltage $(I_C = 10 \text{mA}, I_F = 0)$	V <sub>(BR)CEO</sub>	30		volts
H11AA1,3,4 H11AA2		1.5 1.8	volts volts	Breakdown Voltage (I <sub>C</sub> = 100μA, I <sub>F</sub> = 0)	V <sub>(BR)CBO</sub>	70		volts
Capacitance (V = 0, F = 1 MHz)	$C_{J}$	100	picofarads	Breakdown Voltage $(I_E = 100\mu A, I_F = 0)$	V <sub>(BR)EBO</sub>	5		volts
				Collector Dark Current (V <sub>CE</sub> = 10V, I <sub>F</sub> = 0)	I <sub>CEO</sub>		·	
				H11AA1, 3, 4 H11AA2			100 200	nanoamps nanoamps

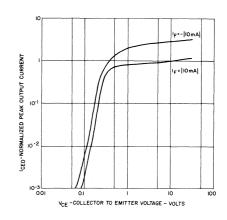
## coupled electrical characteristics (25°C) (unless otherwise specified)

	MIN.	MAX.	UNITS
Current Transfer Ratio (V <sub>CE</sub> = 10V, I <sub>F</sub> = ± 10mA) H11AA4 H11AA3 H11AA1	100 50 20		percent percent percent
H11AA2	10		percent
Saturation Voltage - Collector to Emitter (I <sub>CEO</sub> =0.5mA, I <sub>F</sub> = ±10mA)		0.4	volts
Current Transfer Ratio Symmetry: $\frac{I_{CEO}(V_{CE}=10V, I_F=10\text{mA})}{I_{CEO}(V_{CE}=10V, I_F=-10\text{mA})}$ Note 2		* .	
H11AA1, 3, 4	0.33	3.0	
Isolation Resistance (Input to Output Voltage = 500V <sub>DC</sub> . See Note 1)	100		gigaohms

Note 1: Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together

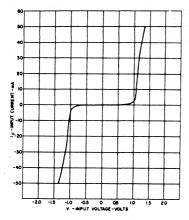




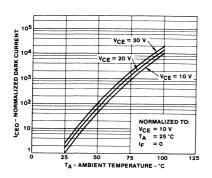


Note 2: The H11AA1 specification guarantees the maximum peak output current will be no more than three times the minimum peak output current at I<sub>F</sub> = 10 mA

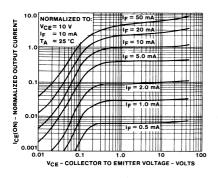
### TYPICAL CHARACTERISTICS



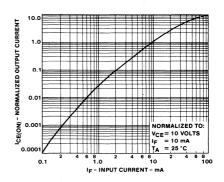
1. INPUT CHARACTERISTICS



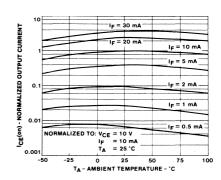
3. DARK I<sub>CEO</sub> CURRENT VS TEMPERATURE



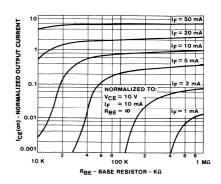
5. OUTPUT CHARACTERISTICS



#### 2. OUTPUT CURRENT VS INPUT CURRENT



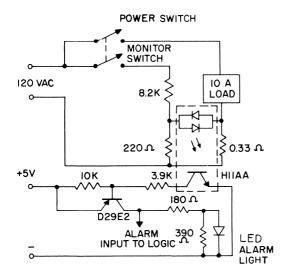
4. OUTPUT CURRENT VS TEMPERATURE



6. OUTPUT CURRENT VS BASE EMITTER RESISTANCE

#### H11AA APPLICATIONS

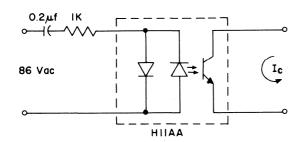
### LOAD MONITOR AND ALARM



In many computer controlled systems where AC power is controlled, load dropout due to filament burnout, fusing, etc. or the opposite situation - load power when uncalled for due to switch failure can cause serious systems or safety problems. This circuit provides a simple AC power monitor which lights an alarm lamp and provides a "1" input to the computer control in either of these situations while maintaining complete electrical isolation between the logic and the power system.

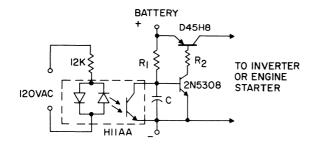
Note that for other than resistive loads, phase angle correction of the monitoring voltage divider is required.

#### RING DETECTOR



In many telecommunications applications it is desirable to detect the presence of a ring signal in a system without any direct electrical contact with the system. When the 86 Vac ring signal is applied, the output transistor of the H11AA is turned on indicating the presence of a ring signal in the isolated telecommunications system.

### **UPS SOLID STATE TURN-ON SWITCH**



Interruption of the 120 VAC power line turns off the H11AA, allowing C to charge and turn on the 2N5308-D45H8 combination which activates the auxiliary power supply. This system features low standby drain, isolation to prevent ground loop problems and the capability of ignoring a fixed number of "dropped cycles" by choice of the value of C.

### H11AG1, H11AG2, H11AG3

## **Optoisolator**

# **GaAlAs Infrared Emitting Diode and**

**NPN Silicon Phototransistor** 

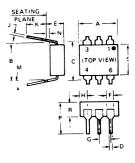
The H11AG series consists of a gallium aluminum arsenide infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. This photon coupled isolator provides the unique feature of high current transfer ratio at both low output voltage and low input current. This makes it ideal for use in low power logic circuits, telecommunications equipment and portable electronics isolation applications. These devices are also available in surface-mount packaging.





### **FEATURES**

- High isolation voltage, 3750 V<sub>(RMS)</sub> minimum (steady state)
- Unique high performance glass dielectric construction
- High efficiency low degradation liquid epitaxial IRED
- Logic level compatible, input and output currents, with CMOS and LS/TTL
- High DC current transfer ratio at low input currents



## absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE							
Power Dissipation - T <sub>A</sub> = 25°C Forward Current (Continuous)	*75 50	milliwatts milliamps					
Reverse Voltage	6	volts					
*Derate 1.0 mW/°C above 25°C.							

PHOTO-TRANSISTOR						
Power Dissipation - $T_A = 25^{\circ}C$	**150	milliwatts				
$V_{CEO}$	30	volts				
$V_{CBO}$	70	volts				
$V_{ECO}$	7	volts				
Collector Current (Continuous)	50	milliamps				
**Derate 2.0 mW/°C above 25°C						

	MILLIMETERS		INC	HES	
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Λ	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
C	- 1	8.64	1	.340	2
D	.406	.508	0.16	.020	
E	1	5.08	1 1	.200	3
F	1.01	1.78	.040	.070	I
G	2.28	2.80	.090	.110	I
н		2.16		.085	4
J }	.203	.305	.008	.012	1
K	2.54		.100		
M		15°		15°	1
N P	.381		.015		1
P		9.53	1	.375	1
R	2.92	3.43	.115	.135	1
S	6.10	6.86	.240	.270	1

- 1. INSTALLED POSITION LEAD CENTERS.
  2. OVERALL INSTALLED DIMENSION.
  3. THESE MEASUREMENTS ARE MADE FROM THE SEATING
- PLANE. 4. FOUR PLACES

#### **TOTAL DEVICE**

Storage Temperature -50°C to 150°C

Operating Temperature -50 to 100°C

Lead Soldering Time (at 260°C) 10 seconds

Surge Isolation Voltage (Input to Output)

H11AG1-H11AG2 5656 V<sub>(neak)</sub> 4000 V<sub>(RMS)</sub> 2500 V<sub>(RMS)</sub> 3535 V<sub>(peak)</sub>

Steady-State Isolation Voltage (Input to Output) H11AG1-H11AG2 5300 V<sub>(peak)</sub> 3750 V(RMS)

3180 V<sub>(peak)</sub> 2250 V<sub>(RMS)</sub> H11AG3



N Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate #35035, except type H11AG3

## individual electrical characteristics (0-70°C)

INFRARED EMITTER DIODE	MIN.	MAX.	UNITS
Forward Voltage - V <sub>F</sub> (l <sub>F</sub> = 1 mA)		1.5	volts
Reverse Current - $I_R$ $T_A = 25^{\circ}$ C $(V_R = 5V)$ $T_A = 70^{\circ}$ C		100	microamps microamp
Capacitance - $C_J$ (V = O, f = 1 MHz)		100	picofarads

PHOTO-TRANSISTOR	MIN.	TYP.	мах.	UNITS
Breakdown Voltage - $V_{(BR)CFO}$ ( $I_C = 1.0 \text{ mA}, I_F = O$ )	30	No. of the last of		volts
Breakdown Voltage $V_{(BR)CBO}$ ( $I_C = 100 \mu A, I_F = O$ )	70		- desirabilitation	volts
Breakdown Voltage $V_{(BR)ECO}$ ( $I_F = 100 \mu A, I_F = O$ )	7			volts
Collector Dark Current $I_{CEO}$ ( $V_{CE} = 10 \text{ V}, I_F = O$ )		5	10	micro- amps
Capacitance $C_{CF}$ ( $V_{CF} = 10 \text{ V}, f = 1 \text{MHz}$ )		2		pico- farads

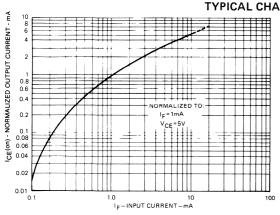
## Coupled electrical characteristics (0-70°C)

1.7	H11AG1		H11AG1 H11AG2		H11AG3		LINUTE	
	MIN.	MAX.	MIN.	MAX.	MIN.	MAX.	UNITS	
DC Current Transfer Ratio								
$(I_E = 1.0 \text{ mA}, V_{CE} = 5 \text{ V})$	300	_	200		100		%	
$(I_E = 1.0 \text{ mA}, V_{CE} = 0.6 \text{ V})$	100		50		20		%	
$(I_F = 0.2 \text{ mA}, V_{CF} = 1.5 \text{ V})$	100	_	50	-			%	
Saturation Voltage — Collector to Emitter								
$(I_F = 2.0 \text{ mA}, I_C = 0.5 \text{ mA})$		0.4	_	0.4		0.4	volts	

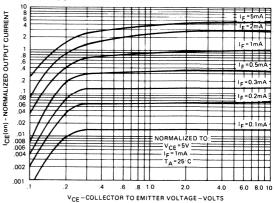
## coupled electrical characteristics (25°C)

	MIN.	TYP.	MAX.	UNITS
Isolation Resistance (Input to Output Voltage = 500 V <sub>DC</sub> ) Input to Output Capacitance (Input to Output Voltage = O, f = 1 MHz)	100		2	gigaohms picofarads
Turn-On Time $-t_{on}$ ( $V_{CC}$ = 5 V, $I_F$ = 1 mA, $R_L$ = 100)		5	_	microseconds
Turn-Off Time $-t_{\text{off}}$ ( $V_{CC}$ = 5 V, $I_F$ = 1 mA, $R_I$ = 100)		5		microseconds

## H11AG1, H11AG2, H11AG3

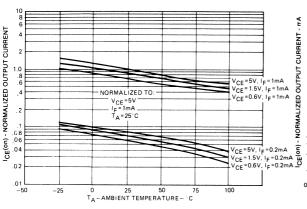


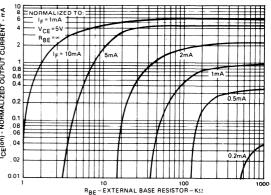
TYPICAL CHARACTERISTICS



**OUTPUT CURRENT VS. INPUT CURRENT** 

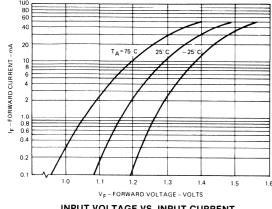
OUTPUT CURRENT VS. COLLECTOR-EMITTER VOLTAGE

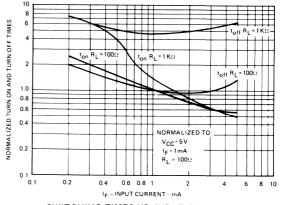




**OUTPUT CURRENT VS. TEMPERATURE** 

**OUTPUT CURRENT VS. BASE EMITTER** RESISTANCE



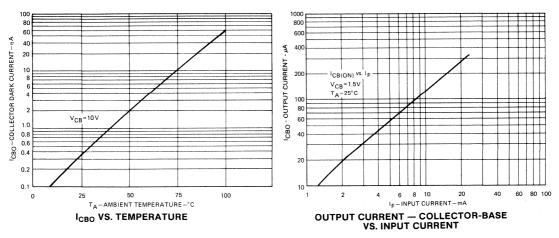


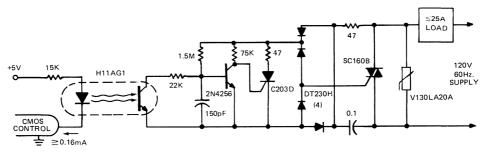
INPUT VOLTAGE VS. INPUT CURRENT

**SWITCHING TIMES VS. INPUT CURRENT** 

### H11AG1, H11AG2, H11AG3

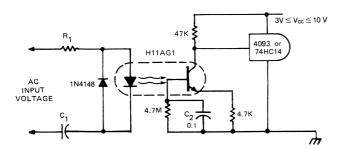
#### TYPICAL CHARACTERISTICS





### CMOS INPUT, 3KW, ZERO VOLTAGE SWITCHING SOLID STATE RELAY

The H11AG1 superior performance at low input currents allows standard CMOS logic circuits to directly operate a 25A solid state relay. Circuit operation is as follows: power switching is provided by the SC160B, 25A triac. Its gate is controlled by the C203B via the DT230H rectifier bridge. The C203B turn-on is inhibited by the 2N4256 when line voltage is above 12V and/or the H11AG1 is off. False trigger and dv/dt protection are provided by the combination of a GE-MOV® varistor and RC snubber network.



INPUT	R <sub>1</sub>	C <sub>1</sub>	z
40-90 VRMS	75K	0.1 μF	109K
20 Hz.	1/ <sub>10</sub> W	100 V	
95-135 VRMS	180K	12 ηF	285K
60 Hz.	1/ <sub>10</sub> W	200 V	
200-280 VRMS	390K	6.80 ηF	550K
50/60 Hz.	¼ W	400 V	

DC component of input voltage is ignored due to C1

### TELEPHONE RING DETECTOR/A.C. LINE CMOS INPUT ISOLATOR

The H11AG1 uses less input power than the neon bulb traditionally used to monitor telephone and line voltages. Additionally, response time can be tailored to ignore telephone dial tap, switching transients and other undesired signals by modifying the value of C2. The high impedance to line voltage also can simplify board layout spacing requirements.

## H11AV1, H11AV2, H11AV3, H11AV1A, H11AV2A, H11AV3A

## **Optoisolator**

## **GaAs Infrared Emitting Diode and NPN Silicon Phototransistor**

The H11AV series consists of a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. The construction provides guaranteed internal distance for VDE creep and clearance requirements, for business machine applications per VDE standard 0730-2P. The H11AV1A, H11AV2A and H11AV3A are lead-formed versions of the H11AV1, H11AV2 and H11AV3. These devices are also available in surface-mount packaging.

#### **FEATURES**

- High isolation voltage, 3750  $V_{(RMS)}$  minimum (steady state).
- Unique high performance dielectric construction
- High efficiency low degradation liquid epitaxial IRED
- High humidity resistant silicone encapsulation
- Internal conductive part separation 2mm minimum
- Creepage distance 8.2mm minimum (before mounting)
- Low isolation capacitance 0.5pf (max.)

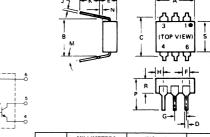
### absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE						
Power Dissipation - $T_A = 25^{\circ}C$	*100	milliwatts				
Forward Current (Continuous)	60	milliamps				
Forward Current (Peak) (Pulse width 1 µsec, 300 pps)	3	amperes				
Reverse Voltage	6	volts				
*Derate 1.33 mW/°C above 25°C ambient						

PHOTO-TRANSISTOR						
Power Dissipation - $T_A = 25^{\circ}C$	**300	milliwatts				
V <sub>CFO</sub>	70	volts				
V <sub>CBO</sub>	70	volts				
V <sub>EBO</sub>	7	volts				
Collector Current (Continuous)	100	milliamps				
**Derate 4.0 mW/°C above 25°C						

### Storage Temperature -55°C to 150°C Operating Temperature -55 to 100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output) 5656 V<sub>(peak)</sub> 4000 V(RMS) Steady-State Isolation Voltage (Input to Output). 3750 V<sub>(RMS)</sub> 5304 V<sub>(DC)</sub> Nominal Voltage 500 V<sub>(RMS)</sub>/600 V<sub>DC</sub> Isolation Group C

**TOTAL DEVICE** 



	MILLIMETERS		INCHES		
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Λ .	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
С	- 1	8.64	i	.340	2
D	.406	.508	0.16	.020	
E		5.08	1	.200	3
F	1.01	1.78	.040	.070	1
G	2.28	2.80	.090	.110	1
н		2.16	l	.085	4
J	.203	.305	.008	.012	
K	2.54		.100		1
M		15°		15°	1
N	.381		.015		I
P		9.53		.375	1
R	2.92	3.43	.115	.135	1
S	6.10	6.86	.240	.270	I

- NOTES
- NOTES

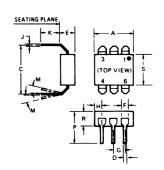
  1. INSTALLED POSITION LEAD CENTERS.

  2. OVERALL INSTALLED DIMENSION.

  3. THESE MEASUREMENTS ARE MADE FROM THE SEATING
- PLANE. 4. FOUR PLACES.

UI. RECOGNIZED FILE # E51868 VDE APPROVED TO VDE 0883/6.80 VDE 0860/8.81 VDE 0806/8.81 VDE 0804/1.83 VDE 0750T1/5.82 VDE 0110/11.72 IEC 601T1 IEC 380 CERTIFICATE # 30440 VDE 0884 CERTIFICATE # 63724†

### H11AV1, H11AV2, H11AV3



	MILLIMETERS		INCHES		
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Λ	8.38	8.89	.330	350	
l c l	10.16	REF.		REF.	1
D	.406	.508	.016	.020	1
E		4.32		.170	1
F	1.01	1.78	.040	.070	1
6	2.28	2.80	.090	.110	
н		2.16		.085	1 1
J	.203	.305	.008	.012	
K	2.54	l	.100		1
М		10%		10°	ł
P	6.20	REF.	.244	REF.	1
R	2.92	3.43	.115	.135	1
S .	6.10	6.86	.240	.270	1
NOTES				<u> </u>	

DIMENSION APPLIES FOUR PLACES.

H11AV1A, H11AV2A, H11AV3A

# 12

## H11AV1, H11AV2, H11AV3, H11AV1A, H11AV2A, H11AV3A

## individual electrical characteristics (25°C) (unless otherwise indicated)

INFRARED EMITTER DIODE	MIN.	MAX.	UNITS
Forward Voltage - V <sub>F</sub> (I <sub>F</sub> = 10 mA)	.8	1.5	volts
Forward Voltage - $V_F$ ( $I_F = 10 \text{ mA}$ ) $T_A = 55^{\circ}\text{C}$	.9	1.7	volts
Forward Voltage - $V_F$ ( $I_F = 10 \text{ mA}$ ) $T_A = 100^{\circ}\text{C}$	.7	1.4	volts
Reverse Current - $I_R$ ( $V_R = 6V$ )	_	10	microamps
Capacitance - $C_J$ (V = O, f = 1 MHz)		100	picofarads

PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - $V_{(BR)CEO}$ ( $I_C = 1.0 \text{ mA}, I_F = O$ )	70	and the same of th		volts
Breakdown Voltage - $V_{(BR)CBO}$ ( $I_C = 100 \mu A, I_F = O$ )	70	Sept. Sec.		volts
Breakdown Voltage - $V_{(BR)EBO}$ $(I_F = 100 \mu A, I_F = O)$	7			volts
Collector Dark Current - $I_{CEO}$ ( $V_{CE} = 10 \text{ V}, I_F = O$ )		5	50	nano- amps
Capacitance $C_{CE}$ ( $V_{CE} = 10 \text{ V}, f = 1 \text{ MHz}$ )	_	2		pico- farads

## coupled electrical characteristics (25°C) (unless otherwise specified)

	MIN.	MAX.	UNITS
DC Current Transfer Ratio (I <sub>E</sub> = 10 mA, V <sub>CE</sub> = 10 V) H11A	V1 100	300	%
HIIA	V2 50	_	%
HIIA	V3 20		%
Saturation Voltage - Collector to Emitter (I <sub>F</sub> = 20 mA, I <sub>C</sub> = 2 mA)	_	0.4	volts
Isolation Resistance (Input to Output Voltage = 500 V <sub>DC</sub> See Note 1)	100		gigaohms
Input to Output Capacitance (Input to Output Voltage = O, f = 1 MHz, See Note 1)	-	0.5	picofarads
Turn-On Time — $t_{on}$ ( $V_{CC}$ = 10 V, $I_{C}$ = 2 mA, $R_{L}$ = 100 $\Omega$ ). (See Figure 1)	_	15	microseconds
Turn-Off Time — $t_{off}$ ( $V_{CC}$ = 10 V, $I_C$ = 2 mA, $R_L$ = 100 $\Omega$ ). (See Figure 1)	: <u></u>	15	microseconds

### Resistance to Creepage

• EXTERNAL K<sub>B</sub> 100 • INTERNAL K<sub>B</sub> 600

#### NOTE 1:

Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together.

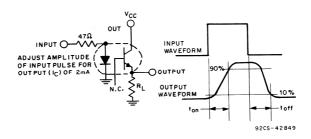
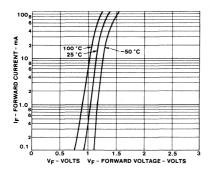


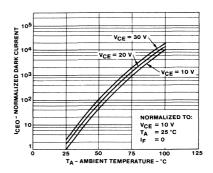
FIGURE 1. SWITCHING TIME TEST CIRCUIT

### H11AV1, H11AV2, H11AV3, H11AV1A, H11AV2A, H11AV3A

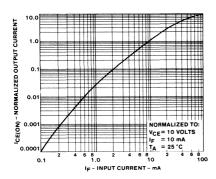
### **TYPICAL CHARACTERISTICS**



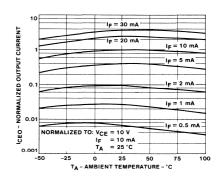
#### 2. INPUT CHARACTERISTICS



### 3. DARK I<sub>CEO</sub> CURRENT VS TEMPERATURE



4. OUTPUT CURRENT VS INPUT CURRENT



### 5. OUTPUT CURRENT VS TEMPERATURE

### **†DETAILS OF VDE 0884 APPROVAL**

Class: DIN VDE 0109/12.83 Table 1

OPERATING VOLTAGE	CLASSIFICATION
V <sub>LINE</sub> < 300V <sub>RMS</sub>	Class I – IV
V <sub>LINE</sub> < 600V <sub>RMS</sub>	Class I – III
Max. operating voltage = 630 <sub>RMS</sub>	
Max. transient overvoltage = 6000V	
Partial discharge test voltage = 1000V	
Partial discharge max value at test voltage = 5 picocoulomb	

The optoisolator provides safe electrical isolation only when used within its maximum ratings. To guarantee safe operation, external circuitry must provide safe limits to the energy applied to the optoisolator. (Refer to Chapter 6: Safety.)

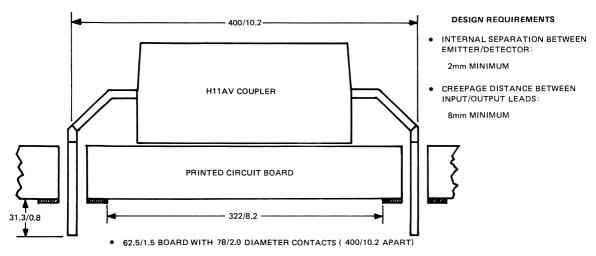
### H11AV1, H11AV2, H11AV3, H11AV1A, H11AV2A, H11AV3A

#### MOUNTING THE H11AV

CURRENT INDUSTRIAL STANDARD VDE 0883/6.80 OF THE FEDERAL REPUBLIC OF GERMANY CONCERNING OPTOCOUPLERS CALLS FOR A MINIMUM CREEPAGE DISTANCE (I.E... ACROSS THE SURFACE OF THE CIRCUIT BOARD IN WHICH THE DEVICE IS

MOUNTED) OF 8mm (0.315 IN.) BETWEEN INPUT AND OUTPUT TERMINALS. THE FOLLOWING DIAGRAM ILLUSTRATES ONE WAY TO FORM THE LEADS TO MEET THIS DIMENSIONAL REQUIREMENT.

#### TYPICAL H11AV COUPLER MOUNTING (DIMENSIONS IN MILLINCHES/MILLIMETERS UNLESS NOTED)



31.3/0.8 PROTRUDING FROM BOARD FOR SOLDERING

### IMPORTANT NOTICE

CONFORMITY WITH VDE STANDARDS IS DETERMINED BY VDE ALTHOUGH THE ABOVE DRAWING ILLUSTRATES ONE SUGGESTED MOUNTING TECHNIQUE, IT SHOULD NOT BE UNDERSTOOD AS HAVING RECEIVED ADVANCE APPROVAL FROM VDE.

IN RESPECT TO VDE STANDARDS, HARRIS GUARANTEES THAT THE DIMENSIONS OF THE H11AV

OPTOCOUPLERS MANUFACTURED BY IT CONFORM TO THOSE DIMENSIONS LISTED ON THE H11AV SPECIFICATION SHEET #40.8, BUT ASSUMES NO RESPONSIBILITY OR LIABILITY FOR THE MEETING OF THE 8mm (0.315") CREEPAGE DISTANCE REQUIREMENT BY ANY CUSTOMER MOUNTED PRODUCT.

## H11B1, H11B2, H11B3

## **Optoisolator**

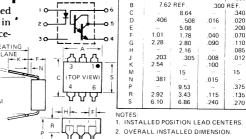
**GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier** 

The H11B1, H11B2 and H11B3 are gallium arsenide, infrared emitting diodes coupled with a silicon photo-Darlington amplifier in a dual in-line package. These devices are also available in surfacemount packaging.

### absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1 µsec 300 P Ps)		
Reverse Voltage	3	volts
*Derate 1.33mW/°C above 25	5°C ambient.	

PHOTO-DARLINGTON		
Power Dissipation	**150	milliwatts
$V_{CEO}$	25	volts
$V_{CBO}$	30	volts
$V_{ m EBO}$	7	volts
Collector Current (Continuous)	100	milliamps
**Derate 2.0mW/°C above		



MILLIMETERS

MAX.

8.89

MIN.

INCHES

MIN MAX

.330 350 NOTES

- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES

3750V<sub>(RMS)</sub>

#### **TOTAL DEVICE**

5300V<sub>(peak)</sub>

Storage Temperature -55 to 150°C Operating Temperature -55 to 100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output).  $5656V_{(peak)}$  $4000V_{(RMS)}$ Steady-State Isolation Voltage (Input to Output).

### individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage - V <sub>F</sub>			
$H11B1, B2 (I_F = 10mA)$	1.1	1.5 1.5	volts
H11B3 $(I_F = 50mA)$	1.1	1.5	volts
Reverse Current $-I_R$ $(V_R = 3V)$	. some	10	microamps
Capacitance $-C_J$ $(V = O, f = 1 MHz)$	50		picofarads

PHOTO-DARLINGTON	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - V <sub>(BR)CEO</sub>	25	_	_	volts
$(I_C = 10 \text{mA}, I_F = 0)$				
Breakdown Voltage – V <sub>(BR)CBO</sub>	30		-	volts
$(I_C = 100\mu A, I_F = 0)$				
Breakdown Voltage — V <sub>(BR)EBO</sub>	7	_		volts
$(I_{\rm E} = 100\mu A, I_{\rm F} = O)$				
Collector Dark Current – I <sub>CEO</sub>	-	5	100	nanoamps
$(V_{CE} = 10V, I_F = 0)$			,	
Capacitance	-	6	-	picofarads
$(V_{CE} = 10V, f = 1MHz)$				4.5

## coupled electrical characteristics (25°C)

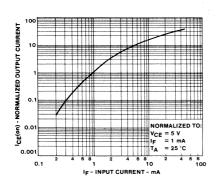
		MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio (I <sub>F</sub> = 1mA, V <sub>CE</sub> = 5V)	H11B1	500	_	_	%
	H11B2	200			%
	H11B3	100	_		%
Saturation Voltage – Collector to Emitter ( $I_F = 1 \text{mA}$ , $I_C = 1 \text{mA}$ )		-	0.7	1.0	volts
Isolation Resistance (Input to Output Voltage = 500V <sub>DC</sub> )		100	_	_	gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1MHz)		-		2	picofarads
Switching Speeds: $(V_{CE} = 10V, I_C = 10mA, R_L = 100\Omega)$	On-Time	-	125	_	microseconds
	Off-Time	· —	100		microseconds

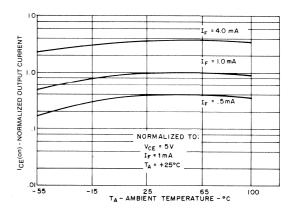
Nu Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate # 35025

### H11B1, H11B2, H11B3

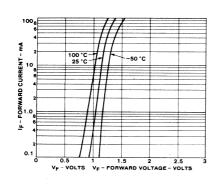
### TYPICAL CHARACTERISTICS

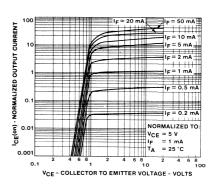




#### **OUTPUT CURRENT VS INPUT CURRENT**

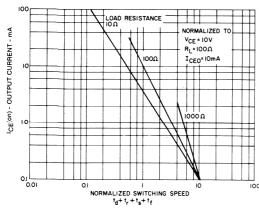
**OUTPUT CURRENT VS TEMPERATURE** 

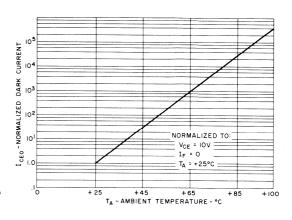




### INPUT CHARACTERISTICS

OUTPUT CHARACTERISTICS





SWITCHING SPEED VS OUTPUT CURRENT

NORMALIZED DARK CURRENT VS TEMPERATURE

### H11B255

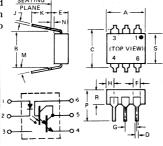
## **Optoisolator**

# GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier

The H11B255 consists of a gallium arsenide infrared emitting diode coupled with a silicon photo-Darlington amplifier in a dual in-line package. This device is also available in surface-mount packaging.

### absolute maximum ratings: (25°C)

INFRARED EMITTING DIODES								
Power Dissipation	*90	milliwatts						
Forward Current (Continuous)	60	milliamps						
Forward Current (Peak)	3	ampere						
(Pulse width 1µsec. 300 P Ps)								
Reverse Voltage	3	volts						
*Derate 1.2mW/°C above 25°C ambient.								



SYMBOL	MILLIM	ETERS	INC	HES	NOTES
STIVIBUL	MIN.	MAX.	MIN.	MAX.	10123
A	8.38	8.89	.330 .350		
В	7.62	REF.	.300	REF.	1
C	-	8.64		.340	2
D	.406	.508	.016	.020	3
E	-	5.08	_	200	
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
н	-	2.16		.085	4
J	.203	.305	.008	.012	
K	2.54	-	.100		
М	-	15		15	1
. N	.381	-	.015 -		
P	-	9.53	-	.375	
R	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	

- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES.

F	ч	Ю	T	O.	D	Α	R	L	IN	G	то	N

Power Dissipation	**210	milliwatts			
$V_{CEO}$	55	volts			
$V_{CBO}$	55	volts			
$V_{EBO}$	8	volts			
Collector Current (Continuous)	100	milliamps			
**Derate 2.8mW/°C above 25°C ambient.					

### TOTAL DEVICE

Storage Temperature -55 to 150°C
Operating Temperature -55 to 100°C
Lead Soldering Time (at 260°C) 10 seconds.
Surge Isolation Voltage (Input to Output).
3535V<sub>(peak)</sub> 2500V<sub>(RMS)</sub>
Steady-State Isolation Voltage (Input to Output).
3180V<sub>(peak)</sub> 2250V<sub>(RMS)</sub>

### individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage - VF	1.1	1.5	volts
$(I_F = 20 \text{mA})$			
Reverse Current - I <sub>R</sub>	_	10	microamps
$(V_R = 3V)$			
Capacitance $-C_J$ (V = O, f = 1 MHz)	50	water	picofarads
( , , , , , , , , , , , , , , , , , , ,		1	

PHOTO-DARLINGTON	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage – V <sub>(BR)CEO</sub>	55	_	_	volts
$(I_C = 100 \mu A, I_F = O)$				
Breakdown Voltage – V <sub>(BR)CBO</sub>	55	-	-	volts
$(I_C = 100 \mu A, I_F = O)$				
Breakdown Voltage – V <sub>(BR)EBO</sub>	8		-	volts
$(I_E = 100 \mu A, I_F = O)$				
Collector Dark Current - I <sub>CEO</sub>	-	-	100	nanoamps
$(V_{CE} = 10V, I_F = 0)$				
Capacitance	-	2	- 1	picofarads
$(V_{CE} = 10V, f = 1 MHz)$				

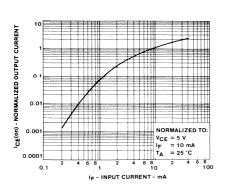
## coupled electrical characteristics (25°C)

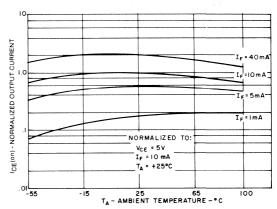
	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio (I <sub>F</sub> = 10mA, V <sub>CE</sub> = 5V)	100			%
Saturation Voltage – Collector to Emitter (I <sub>F</sub> = 50mA, I <sub>C</sub> = 50mA)	100	_	1.0	volts
Isolation Resistance (Input to Output Voltage = 500V <sub>DC</sub> )	100			gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1 MHz)			2	picofarads
Switching Speeds: On-Time $-(V_{CE} = 10V, I_{C} = 10mA, R_{L} = 100\Omega)$		125	-	microseconds
Off-Time – $(V_{CE} = 10V, I_C = 10mA, R_L = 100\Omega)$	_	100	-	microseconds

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## 12

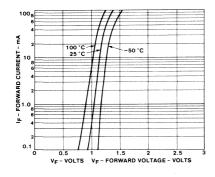
### TYPICAL CHARACTERISTICS

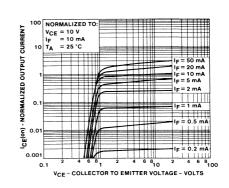




### 1. OUTPUT CURRENT VS. INPUT CURRENT

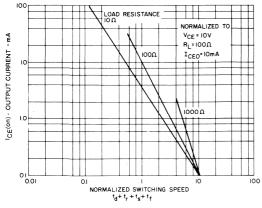
2. OUTPUT CURRENT VS. TEMPERATURE

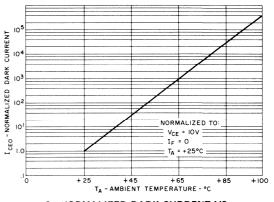




### 3. INPUT CHARACTERISTICS

4. OUTPUT CHARACTERISTICS





5. SWITCHING SPEED VS. OUTPUT CURRENT

6. NORMALIZED DARK CURRENT VS. TEMPERATURE

## H11C1, H11C2, H11C3

## **Optoisolator**

## **GaAs Infrared Emitting Diode and**

**Light Activated SCR** The H11C1, H11C2 and H11C3 are gallium arsenide, infrared emitting diodes coupled with light activated silicon controlled rectifiers in a dual in-line package. These devices are also

available in surface-mount packaging. absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1 µsec 300 P Ps)		
Reverse Voltage	6	volts
*Derate 1.33 mW/°C above 2	5°C ambient.	

SEATING PLANE		SYMBOL.	MIN.	MAX.	MIN.	MAX.	NOTES
J 7 1+ K + 1+ E+	A	А	8.38	8.89	.330	.350	
t II-NI		В	7.62	REF.	.300	REF.	1
		С		8.64		.340	2
1	3 1 1	D	.406	508	.016	.020	
1 1	C ITOP VIEW) S	E		5.08		.200	3
В	C (TOP VIEW) S	F	1.01	1.78	.040	.070	
M	4 6	G	2.28	2.80	.090	.110	
	+ 575757	н		2.16		.085	4
	0 0 0	J	.203	.305	.008	.012	
1	I→IHI← →IEI←	K	2.54		.100		
		M		15		15	
1		N	.381		.015		
10°6	$i \leftarrow \forall \mathcal{A} \mathcal{A} \mathcal{A}$	P	-	9.53		.375	
[ <del>                                     </del>	1 1 N M B	R	2.92	3.43	.115	.135	
᠈╃┦ <sup>╻</sup> ┸	<u>+                                    </u>	5	6.10	6.86	240	.270	
304		NOTES: 1. INSTAI	LED PO	SITION L	EAD CEN	TERS.	

- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES.

MILLIMETERS

INCHES

NOTE

PHOTO-SCR		
Peak Forward Voltage	200	volts
RMS Forward Current	300	milliamps
Forward Current (Peak)	10	amperes
(100µsec 1% duty cycle)		
Surge Current (10m sec)	5	amperes
Reverse Gate Voltage	6	volts
Power Dissipation (25°C Ambient)	** 400	milliwatts
Power Dissipation (25°C Case)	***1000	milliwatts
**Derate 5.3mW/°C above ***Derate 13.3mW/°C above	25°C ambient. 25°C case.	

### **TOTAL DEVICE**

Storage Temperature -55 to 150°C Operating Temperature -55 to 100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output).

4000V<sub>(RMS)</sub> H11C1 5656V<sub>(peak)</sub>

H11C2-H11C3 3535V<sub>(peak)</sub> 2500V<sub>(RMS)</sub> Steady-State Isolation Voltage (Input to Output).

H11C1 5300V<sub>(peak)</sub> 3750V<sub>(RMS)</sub> H11C2-H11C3 3180V<sub>(peak)</sub>

2250V(RMS)

## individual electrical characteristics (25°C)

INFRARED EMITTIN	G DIODE	TYP.	MAX.	UNITS
Forward Voltage $(I_F = 10mA)$	$V_{\mathrm{F}}$	1.2	1.5	volts
Reverse Current (V <sub>R</sub> = 3V)	$I_R$	<del>-</del>	10	microamps
Capacitance (V = O,f = 1MHz)	C <sub>J</sub>	50	-	picofarads

PHOTO-SCR	MIN.	TYP.	MAX.	UNITS
Off-State Voltage — V <sub>DM</sub> (R <sub>GK</sub>	200	_	_	volts
= $10K\Omega$ , $100^{\circ}$ C, $I_D = 50\mu$ A)				
Reverse Voltage — V <sub>RM</sub> (R <sub>GK</sub>	200	-	-	volts
= $10K\Omega$ , $100^{\circ}$ C, $I_R = 50\mu$ A)				
On-State Voltage — V <sub>TM</sub>		1.1	1.3	volts
$(I_{TM} = .3 \text{ amp})$				
Off-state Current $-I_{DM}$ ( $V_{DM} =$	-	-	50	microamps
$200V, T_A = 100^{\circ}C, R_{GK} = 10K)$				
Reverse Current $-I_{RM}$ ( $V_{RM} =$	-		50	microamps
$200V, T_A = 100^{\circ}C, R_{GK} = 10K)$				
Capacitance (Anode-Gate)	-	20	-	picofarads
V=0V,f=1MHz(Gate-Cathode)	_	350		picofarads

## coupled electrical characteristics (25°C)

		MIN.	TYP.	MAX.	UNITS
Input Current to Trigger ( $V_{AK} = 50V$ , $R_{GK} = 10K\Omega$ )	H11C1, C2	_	_	20	milliamps
	H11C3	-		30	milliamps
Input Current to Trigger ( $V_{AK}$ = 100V, $R_{GK}$ = 27K $\Omega$ )	H11C1, C2	-	-	11	milliamps
	H11C3			14	milliamps
Isolation Resistance (Input to Output Voltage = $500V_{DC}$ )		100	-	-	gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1MHz)		-		2	picofarads
Coupled dV/dt, Input to Output (See Figure 13)		500			volts/µsec

No Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate # 35025

## H11C1, H11C2, H11C3

### TYPICAL CHARACTERISTICS

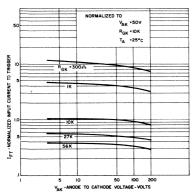


FIGURE 1. INPUT CURRENT TO TRIGGER VS ANODE-CATHODE VOLTAGE

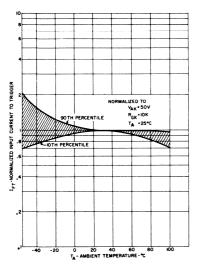


FIGURE 3. INPUT CURRENT TO TRIGGER DISTRIBUTION VS TEMPERATURE

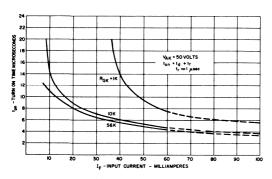


FIGURE 5. TURN ON TIME VS INPUT CURRENT

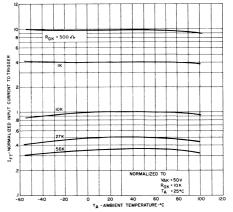


FIGURE 2. INPUT CURRENT TO TRIGGER VS TEMPERATURE

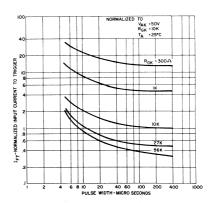


FIGURE 4. INPUT CURRENT TO TRIGGER VS PULSE WIDTH

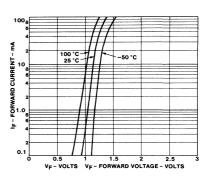


FIGURE 6. INPUT CHARACTERISTICS  $I_F$  VS  $V_F$ 

### H11C1, H11C2, H11C3

### TYPICAL CHARACTERISTICS OF OUTPUT (SCR)

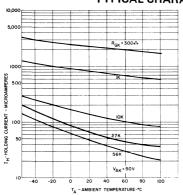


FIGURE 7. HOLDING CURRENT VS TEMPERATURE

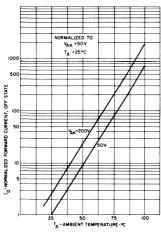


FIGURE 9. OFF STATE FORWARD CURRENT VS TEMPERATURE

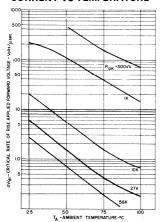


FIGURE 11. dV/dt VS TEMPERATURE

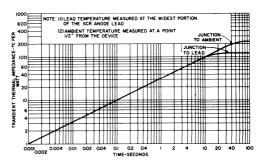


FIGURE 8. MAXIMUM TRANSIENT THERMAL IMPEDANCE

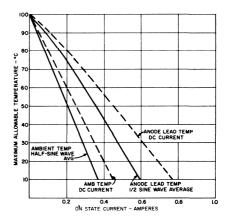


FIGURE 10. ON STATE CURRENT VS MAXIMUM ALLOWABLE TEMPERATURE

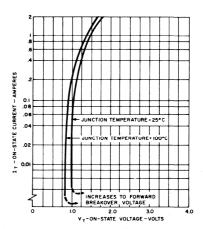
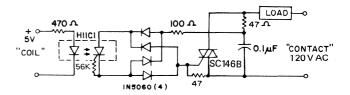


FIGURE 12. ON-STATE CHARACTERISTICS

### TYPICAL APPLICATIONS

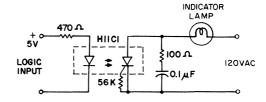
### 10A, T2L COMPATABLE, SOLID STATE RELAY

Use of the H11C1 for high sensitivity, 2500 v isolation capability, provides this highly reliable solid state relay design. This design is compatable with 74, 74S and 74H series T<sup>2</sup>L logic systems inputs and 120VAC loads up to 10 A.



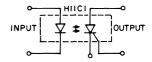
### 25W LOGIC INDICATOR LAMP DRIVER

The high surge capability and non-reactive input characteristics of the H11C allow it to directly couple, without buffers,  $T^2L$  and DTL logic to indicator and alarm devices, without danger of introducing noise and logic glitches.

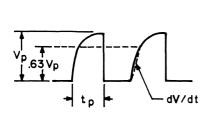


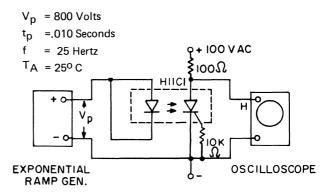
#### 200V SYMMETRICAL TRANSISTOR COUPLER

Use of the high voltage PNP portion of the H11C provides a 200V transistor capable of conducting positive and negative signals with current transfer ratios of over 1%. This function is useful in remote instrumentation, high voltage power supplys and test equipment. Care should be taken not to exceed the H11C 400 mW power dissipation rating when used at high voltages.



## FIGURE 13 COUPLED dV/dt - TEST CIRCUIT





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### H11C4, H11C5, H11C6

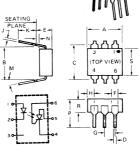
## **Optoisolator**

# GaAs Infrared Emitting Diode and Light Activated SCR

The H11C4, H11C5 and H11C6 are gallium arsenide, infrared emitting diodes coupled with light activated silicon controlled rectifiers in a dual in-line package. These devices are also available in surface-mount packaging.

### absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1µsec 300 P Ps)		
Reverse Voltage	6	volts
*Derate 1.33mW/°C above 25	°C ambient.	



0.000	MILLIM	ETERS	INCHES		NOTES
SYMBOL	MIN.	MAX.	MIN.	MAX.	INOTES
А	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1 1
C.		8.64		.340	2
D	.406	.508	.016	.020	
E	1 14	5.08	-	.200	3
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
н	-	2.16		.085	4
J	.203	.305	.008	.012	
К	2.54	- '	.100		
M	~	15		15	
N	.381	-	.015		1
Р	-	9.53		:375	
R	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	1

- INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE
- 4. FOUR PLACES.

PHOTO - SCR		
Peak Forward Voltage	400	volts
RMS Forward Current	300	milliamps
Forward Current (Peak)	10	amperes
(100µsec 1% duty cycle)		
Surge Current (10m sec)	5	amperes
Reverse Gate Voltage	6	volts
Power Dissipation (25°C Ambient)	** 400	milliwatts
Power Dissipation (25°C Case)	***1000	milliwatts
**Derate 5.3mW/°C above		
***Derate 13.3mW/°C above	25°C case.	

### TOTAL DEVICE

Storage Temperature -55 to 150°C Operating Temperature -55 to 100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output).

 $\begin{array}{ccc} H11C4 & 5656V_{(peak)} & 4000V_{(RMS)} \\ H11C5\text{-}H11C6 & 3535V_{(peak)} & 2500V_{(RMS)} \end{array}$ 

$$\label{eq:Steady-State Isolation Voltage (Input to Output)} \begin{split} & \text{H11C4} & 5300 V_{\text{(peak)}} & 3750 V_{\text{(RMS)}} \\ & \text{H11C5-H11C6} & 3180 V_{\text{(peak)}} & 2250 V_{\text{(RMS)}} \end{split}$$

## individual electrical characteristics (25°C)

INFRARED EMITTING	TYP.	MAX.	UNITS	
Forward Voltage (I <sub>F</sub> = 10mA)	$V_{\mathrm{F}}$	1.2	1.5	volts
Reverse Current (V <sub>R</sub> = 3V)	$I_R$	_	10	microamps
Capacitance (V = O,f = 1MHz)	C <sub>J</sub>	50		picofarads

PHOTO - SCR	MIN.	TYP.	MAX.	UNITS
Off-State Voltage — V <sub>DM</sub> (R <sub>GK</sub>	400		-	volts
= $10$ KΩ, $100$ °C, $I_D$ = $150\mu$ A) Reverse Voltage — $V_{RM}$ ( $R_{GK}$ = $10$ KΩ, $100$ °C, $I_D$ = $150\mu$ A)	400	_	-	volts
On-State Voltage — V <sub>TM</sub>	_	1.1	1.3	volts
$ (I_{TM} = .3 \text{ amp}) $ Off-state Current — $I_{DM}$ ( $V_{DM} = 400V$ , $T_A = 100$ °C, $R_{GK} = 10K$ )	_	-	150	microamps
Reverse Current – $I_{RM}$ ( $V_{RM} = 400V$ , $T_A = 100^{\circ}$ C, $R_{GK} = 10K$ )			150	microamps
Capacitance (Anode-Gate) V=0V,f=1MHz (Gate-Cathode)	_	20 350	_	picofarads picofarads
v - 0 v,1 - 1 will 2 (Gate-Cathode)		550		Picoraraus

## coupled electrical characteristics (25°C)

		MIN.	TYP.	MAX.	UNITS
Input Current to Trigger ( $V_{AK} = 50V$ , $R_{GK} = 10K\Omega$ )	H11C4, C5	_	_	20	milliamps
I AR J OR J	H11C6		-	30	milliamps
Input Current to Trigger ( $V_{AK} = 100 \text{ V}, R_{GK} = 27 \text{K}\Omega$ )	H11C4, C5		_	11	milliamps
CO (AR	H11C6	-	_	14	milliamps
Isolation Resistance (Input to Output Voltage = $500V_{DC}$ )		100	-	-	gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1MHz)		_		2	picofarads
Coupled dv/dt, Input to Output (See Figure 13)		500		_	volts/µsec

Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate # 35025

## 12

## H11C4, H11C5, H11C6

### TYPICAL CHARACTERISTICS

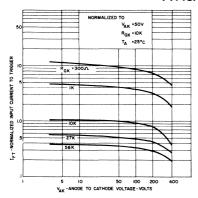


FIGURE 1. INPUT CURRENT TO TRIGGER VS. ANODE-CATHODE VOLTAGE

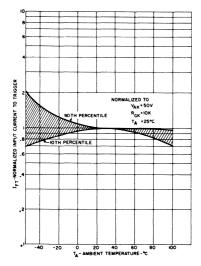


FIGURE 3. INPUT CURRENT TO TRIGGER DISTRIBUTION VS. TEMPERATURE

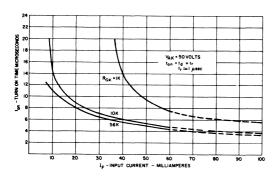


FIGURE 5. TURN-ON TIME VS. INPUT CURRENT

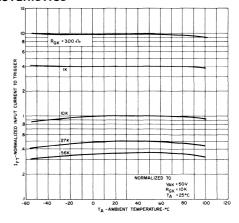


FIGURE 2. INPUT CURRENT TO TRIGGER VS. TEMPERATURE

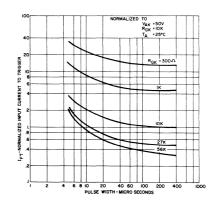


FIGURE 4. INPUT CURRENT TO TRIGGER VS. PULSE WIDTH

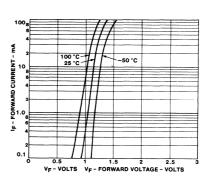


FIGURE 6. INPUT CHARACTERISTICS

I<sub>F</sub> VS. V<sub>F</sub>

## H11C4, H11C5, H11C6

### TYPICAL CHARACTERISTICS OF OUTPUT (SCR)

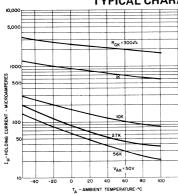


FIGURE 7. HOLDING CURRENT VS. TEMPERATURE

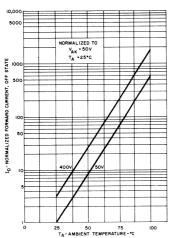


FIGURE 9. OFF-STATE FORWARD CURRENT VS. TEMPERATURE

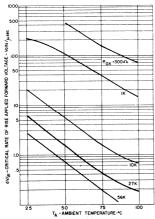


FIGURE 11. dv/dt VS. TEMPERATURE

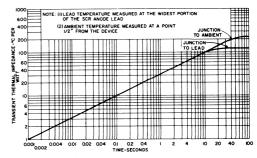


FIGURE 8. MAXIMUM TRANSIENT THERMAL IMPEDANCE

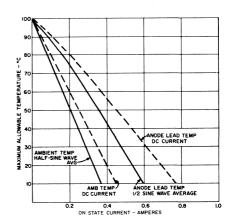


FIGURE 10. ON-STATE CURRENT VS. MAXIMUM ALLOWABLE TEMPERATURE

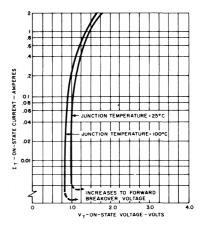
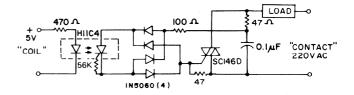


FIGURE 12. ON-STATE CHARACTERISTICS

### TYPICAL APPLICATIONS

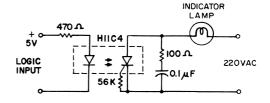
### 10A, T2L COMPATIBLE, SOLID STATE RELAY

Use of the H11C4 for high sensitivity, 2500V isolation capability, provides this highly reliable solid state relay design. This design is compatible with 74, 74S and 74H series  $T^2L$  logic systems inputs and 220V AC loads up to 10A.



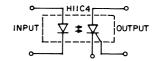
### 25W LOGIC INDICATOR LAMP DRIVER

The high surge capability and non-reactive input characteristics of the H11C allow it to directly couple, without buffers, T<sup>2</sup>L and DTL logic to indicator and alarm devices, without danger of introducing noise and logic glitches.

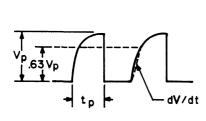


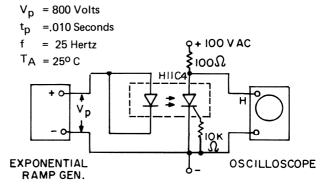
#### 400V SYMMETRICAL TRANSISTOR COUPLER

Use of the high voltage PNP portion of the H11C provides a 400V transistor capable of conducting positive and negative signals with current transfer ratios of over 1%. This function is useful in remote instrumentation, high voltage power supplies and test equipment. Care should be taken not to exceed the H11C 400 mW power dissipation rating when used at high voltages.



## FIGURE 13 COUPLED dv/dt — TEST CIRCUIT



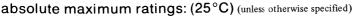


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# H74A1 Optoisolator

# GaAs Infrared Emitting Diode and NPN Silicon Phototransistor TTL Interface

The H74A1 provides logic-to-logic optical interfacing of TTL gates with guaranteed level compatibility in practical specified circuits. The H74A1 is a transistor output photo-coupled isolator specifically designed to eliminate ground loop crosstalk and reflection problems when two distinct logic systems are coupled. It is guaranteed to couple 7400, 74H00 and 74S00 logic gates over the full TTL temperature and voltage ranges. This device is mounted in a dual in-line plastic package. This device is also available in surface-mount packaging.





 $T_A = 25^{\circ}C$  \*100 milliwatts  $T_C = 25^{\circ}C$  \*100 milliwatts

(T<sub>C</sub> indicates collector lead temperature 1/32" from case)
Forward Current (Continuous) 60 milliamps
Forward Current (Peak) 3 ampere

Forward Current (Peak) (Pulse width 1µsec 300 pps)

Reverse Voltage 6 volts

\*Derate 2.2mW/°C above 25°C.

#### PHOTO-TRANSISTOR

Power Dissipation	$T_A = 25^{\circ}C$	**300	milliwatts
Power Dissipation	$T_C = 25^{\circ}C$	***500	milliwatts
(T <sub>C</sub> indicates collector lead	l temperatur	e 1/32" from	n case)
$V_{CEO}$		15	volts
$V_{CBO}$		15	volts
$V_{\rm ECO}$		5.5	volts
Collector Current (Continuous)		50	milliamps

\*\*Derate 6.7mW/°C above 25°C. \*\*\*Derate 11.1mW/°C above 25°C.

### TOTAL DEVICE

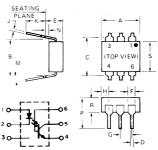
Storage Temperature -55 to 150°C
Operating Temperature 0 to 70°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output)
3535V<sub>(peak)</sub> 2500V<sub>(RMS)</sub>
Steady-State Isolation Voltage (Input to Output)
3180V<sub>(peak)</sub> 2250V<sub>(RMS)</sub>

(peak)

VDE Approved to 0883/6.80 0110b Certificate # 35025

Ru Covered under U.L. component recognition program, reference file E51868





SYMBOL	MILLIM	ETERS	INCHES		NOTES
SAIMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
. С		8.64		.340	2
D .	.406	.508	.016	.020	1
E	_ :	5.08	- '	.200	3
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
н		2.16	817	.085	4
J	.203	.305	.008	.012	
K	2.54		.100		
M	-	15	* *	15	
N	.381		.015	-	
Р		9.53		.375	
R	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	l

#### NOTES

- 1. INSTALLED POSITION LEAD CENTERS
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE
- 4 FOUR PLACES

### Electrical Characteristics of H74A1\*

\*All specifications refer to the following bias configuration (Figure 1) over the full operating temperature (0°C to  $70^{\circ}$ C) and logic supply voltage range (4.5 to  $5.5V_{\rm DC}$ ) unless otherwise noted.

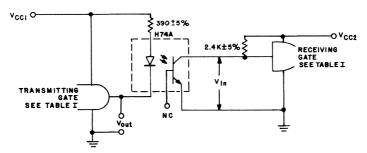


Figure 1. H74A1 BIAS CIRCUIT

V <sub>in</sub> (0), Receiving Gate For V <sub>OUT(0)</sub> from Transmitting Gate –	0.8	V Max.
V <sub>in</sub> (1), Receiving Gate for V <sub>OUT(1)</sub> from Transmitting Gate	2.4	V Min.
t <sub>p</sub> (0), Transmitting Gate to Receiving Gate Propagation Time –	20	usec. Tvp.
t <sub>p</sub> (1), Transmitting Gate to Receiving Gate Propagation Time –	4	usec. Tvp.
Isolation Resistance (Input to Output = $500V_{DC}$ )	00	gigaohms Min.
Input to Output Capacitance (Input to Output Voltage = O, f = 1 MHz)	2.5	pF Max.

TABLE I.

CHARACTERISTICS REQUIRED OF TTL GATES WHICH ARE
TO BE INTERFACED BY H74A1

		TEST CONDITIONS, FIGURE 2						LIMITS	;
PARAMETER	Min.	V <sub>cc</sub> Max.	Min.	Max.	I <sub>S</sub> Min.	INK Max.	Min.	Max.	Units
V <sub>OUT</sub> (1)	4.5V					-0.4mA	2.4		Volts
V <sub>OUT</sub> (0)	4.5V	1			12.0mA			0.4	Volts
V <sub>IN</sub> (1)		5.5V		1.0mA			2.0		Volts
V <sub>IN</sub> (0)		5.5V	-1.6mA					0.8	Volts

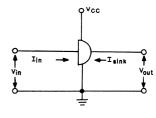


Figure 2.

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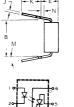
### H74C1, H74C2

## **Optoisolator**

# GaAs Infrared Emitting Diode and Light Activated SCR TTL Interface



The H74Cl and H74C2 are gallium arsenide infrared emitting diodes coupled with light activated silicon controlled rectifiers. They are specifically designed to operate from TTL logic inputs and allow control of 120 or 240V AC power with 7400, 74H00 and 74S00 series logic gates. It can also control up to 400V DC power circuits. They are guaranteed and specified to operate over TTL voltage and temperature ranges using standard tolerance components. The H74Cl and H74C2 are mounted in dual inline packages. These devices are also available in surfacemount packaging.



	SYMBOL	MILLIM	ETERS	INC	HES	NOTES
- A	SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
ппп	А	8.38	8.89	.330	.350	
+	В	7.62	REF.	.300	REF.	1
3 1	c	-	8.64	-	.340	2
C (TOP VIEW) S	D	.406	.508	.016	.020	
	E		5.08	-	.200	3
4 6	F	1.01	1.78	.040	.070	
<del>'</del> \\\\	G	2.28	2.80	.090	.110	
	н		2.16		.085	4
]   H     F	J	.203	.305	300.	.012	
	К	2.54	_	.100	-	
	M	-	15		15	
-5000	N	.381	-	.015	-	
1 11 11 11	P	-	9.53		.375	
	R	2.92	3.43	.115	.135	
G-+ - D	s	6.10	6.86	.240	.270	

NOTES

- 1. INSTALLED POSITION LEAD CENTERS
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE. 4. FOUR PLACES.

## absolute maximum ratings: (25°C) (unless otherwise specified)

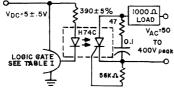
INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current	1	ampere
(Peak 100µsec 1% duty cycle)		
Reverse Voltage	6	volts
*Derate 1.33 mW/°C above 25°C ambient		

PHOTO - SCR		
Peak Forward Voltage		
H74C1	200	volts
H74C2	400	volts
RMS Forward Current	300	milliamps
Forward Current	10	amperes
(Peak, 100µsec 1% duty cycle)		
Surge Current (10 msec)	5	amperes
Reverse Gate Voltage	6	volts
Power Dissipation (25°C Ambient)	** 400	milliwatts
Power Dissipation (25°C Case)	***1000	milliwatts
**Derate 5.3 mW/°C above 25°C ambi ***Derate 13.3 mW/°C above 25°C case.	ient.	

### electrical characteristics of H74C

\*All specifications refer to the following bias configuration (Figure 1) over the full operating temperature (0°C to 70°C) and logic supply voltage range (4.5 to 5.5 V<sub>DC</sub>) unless otherwise noted.

SCR Leakage, Logic Gate V <sub>OUT(1)</sub> , Both Directions	$\mu$ A Max.
SCR Drop, Anode Positive, Logic Gate V <sub>OUT(0)</sub> , I <sub>TM</sub> = 250mA	V Max.
Coupled dv/dt to Trigger, V <sub>DC</sub> to V <sub>AC</sub> (25°)	$V/\mu$ sec. Min.
Capacitance (Input to Output Voltage = O, f = 1 MHz)	pF Max.
Isolation Resistance (Input to Output Voltage = 500 V <sub>DC</sub> )	Gigaohms Min.
Turn-On Time of SCR; $V_{OUT(0)}$ , Input to Output (25°C)	μsec. Max.



+ Vin Vout

Figure 1. H74C BIAS CIRCUIT

Figure 2

Ru Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate # 35025, except type H74C2.

### absolute maximum ratings - total device

SCR Current	See Figure 5
Operating Temperature Range	0°C to 70°C
Operating Voltage Range, VDC	4.5 to 5.5V <sub>DC</sub>
Operating Voltage Range, H74C1	50 to 200 Vpk
H74C2	50 to 400 Vpk
Storage Temperature Range	-55°C to 150°C
Lead Soldering Time (at 260°C)	10 sec. Max.
Surge Isolation Voltage	
(Input to Output)	
3535V <sub>(peak)</sub> 2500	$V_{(RMS)}$
Steady-State Isolation Voltage	

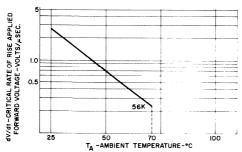
(Input to Output) 3180V<sub>(peak)</sub>

TABLE 1. Ch	naracteristics re	quired of TTL	gate which is to	be int	erfaced	with H	74C.
	TEST CONDITIONS, FIGURE 2			LIMITS			
PARAMETER	V <sub>CC</sub>	I <sub>IN</sub>	I <sub>SINK</sub>	MIN.	MAX.	UNITS	

	TEST CONDITIONS, FIGURE 2				LIMITS				
PARAMETER	V MIN.	CC MAX.	MIN.	MAX.	I <sub>SI</sub> MIN.	NK <b>MAX</b> .	MIN.	MAX.	UNITS
V <sub>OUT</sub> (1)	4.5V					-0.4mA	2.4		Volts
V <sub>OUT</sub> (0)	4.5V				12.0mA			0.4	Volts

### TYPICAL CHARACTERISTICS OF OUTPUT (SCR)

2250V<sub>(RMS)</sub>



### FIGURE 2. dv/dt VS. TEMPERATURE

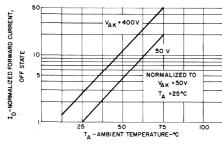


FIGURE 4. OFF-STATE FORWARD CURRENT VS. TEMPERATURE

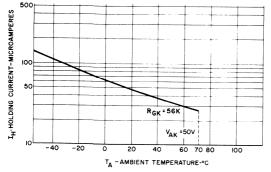


FIGURE 6. HOLDING CURRENT VS. TEMPERATURE

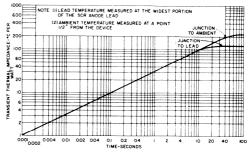


FIGURE 3. MAXIMUM TRANSIENT THERMAL IMPEDANCE

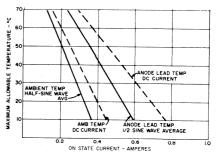


FIGURE 5. ON-STATE CURRENT VS. **MAXIMUM ALLOWABLE TEMPERATURE** 

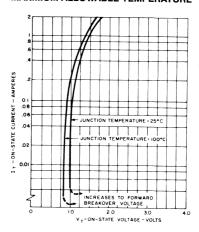


FIGURE 7. ON-STATE CHARACTERISTICS

## H11D1-H11D4

## **Optoisolator**

# GaAs Infrared Emitting Diode and NPN Silicon High Voltage Phototransistor

The H11D1-H11D4 are gallium arsenide, infrared emitting diodes coupled with silicon high voltage phototransistors in a dual in-line package. These devices are also available in surface-mount packaging.

## absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1µsec 300 P Ps)		
Reverse Voltage	6	volts
*Derate 1.33mW/°C above 25	o°C ambient.	

SEATING PLANE B M C (TOP VIEW) 4 6	\$ \$
20 G G G G G G G G G G G G G G G G G G G	

014001	WILLIMETER	EIEN	HVC	INCITES	
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
A	8.38	8.89	.330	.350	
8	7.62	REF.	.300	REF.	1 1
C		8.64		.340	2
D	.406	.508	016	.020	1 1 1
Ε		5.08		.200	3
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
н		2.16		.085	, 4
J	.203	.305	.008	.012	
К	2.54		.100		
M	-	15		15	
N	.381		.015		
Р	-	9.53		.375	
R	2.92	3.43	.115	.135	
s	6.10	6.86	.240	.270	-

NOTES:

- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.

MILLIMETER

3. THESE MEASUREMENTS ARE MADE FROM THE

4000V<sub>(RMS)</sub>

2500V(RMS)

SEATING PLANE. 4. FOUR PLACES.

PHOTO-TRANSISTOR			
	H11D1-D2	H11D3-D4	
Power Dissipation	**300	**300	milliwatts
$V_{CER}$	300	200	volts
$V_{CBO}$	300	200	volts
$V_{\rm ECO}$	7	7	volts
Collector Current	100	100	milliamps
(Continuous)		1	
**Derate 4.0	mW/°C above	25°C ambient.	

### TOTAL DEVICE

Storage Temperature -55 to 150°C Operating Temperature -55 to 100°C

Lead Soldering Time (at 260°C) 10 seconds. Surge Isolation Voltage (Input to Output).

H11D1 5656V<sub>(peak)</sub> H11D2, D3, D4 3535V<sub>(peak)</sub>

Steady-State Isolation Voltage (Input to Output).

H11D1 5300V<sub>(peak)</sub> 3750V<sub>(RMS)</sub> H11D2, D3, D4 3180V<sub>(peak)</sub> 2250V<sub>(RMS)</sub>

## individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> = 10mA)	1.1	1.5	volts
Reverse Current (V <sub>R</sub> = 6V)		10	microamps
Capacitance (V = O,f = 1MHz)	50		picofarads

PHOTO-TRANSISTOR	MIN.	MAX.	UNITS
Breakdown Voltage - V <sub>(BR)CER</sub> D1,2	300	-	volts
$(I_C = 1 \text{ mA}; I_F = 0, R_{BE} = 1 \text{ meg}) D3,4$	200	_	volts
Breakdown Voltage – V <sub>(BR)CBO</sub> D1,2	300		volts
$(I_C = 100\mu A; I_F = 0)$ D3,4	200	- 1	volts
Breakdown Voltage – V <sub>(BR)EBO</sub>	7	-	volts
$(I_E = 100\mu A; I_F = 0)$			
Collector Dark Current - I <sub>CER</sub> ,			
$R_{BE} = 1 \text{ meg.}$			
$(V_{CE}=200V; I_F=0; T_A=25^{\circ}C)$ D1,2	-	100	nanoamps
$(V_{CE}=200V; I_F=0; T_A=100^{\circ}C)$ D1,2		250	microamps
$(V_{CE}=100V; I_F=0; T_A=25^{\circ}C)$ D3,4	_	100	nanoamps
$(V_{CE}=100V; I_F=0; T_A=100^{\circ}C)$ D3,4		250	microamps

## coupled electrical characteristics (25°C)

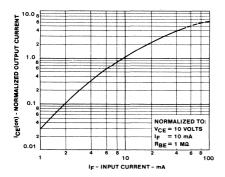
	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_E = 10$ mA, $V_{CE} = 10$ V, $R_{BE} = 1$ meg) H11D1, D2, D3	20		_	%
H11D4	10		-	%
Saturation Voltage – Collector to Emitter ( $I_F = 10\text{mA}$ , $I_C = 0.5\text{mA}$ , $R_{BE} = 1\text{ meg}$ )	-	0.1	0.4	volts
Isolation Resistance (Input to Output Voltage = 500V <sub>DC</sub> )	100	-		gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1 MHz)	_	-	2	picofarads
Switching Speeds: Turn-On Time $-(V_{CE} = 10V, I_{CE} = 2mA, R_L = 100\Omega)$	_	5	_	microseconds
Turn-Off Time $- (V_{CB} = 10V, I_{CE} = 2mA, R_L = 100\Omega)$	-	5		microseconds

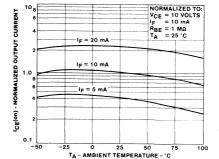
Na Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate # 35025

#### H11D1-H11D4

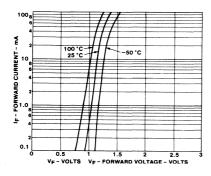
#### TYPICAL CHARACTERISTICS

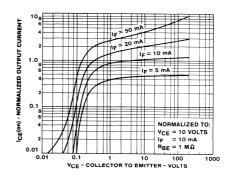




#### 1. OUTPUT CURRENT VS INPUT CURRENT

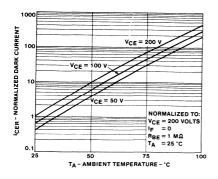
#### 2. OUTPUT CURRENT VS. TEMPERATURE

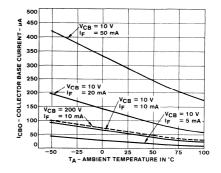




#### 3. INPUT CHARACTERISTICS

4. OUTPUT CHARACTERISTICS





5. NORMALIZED DARK CURRENT VS. TEMPERATURE

6. COLLECTOR BASE CURRENT VS. TEMPERATURE

12

#### H11F1, H11F2, H11F3

# **Optoisolator GaAlAs Infrared Emitting Diode and Bilateral Analog FET**

The H11F family consists of a gallium-aluminum-arsenide infrared emitting diode coupled to a symmetrical bilateral silicon photodetector. The detector is electrically isolated from the input and performs like an ideal isolated FET designed for distortion-free control of low level ac and dc analog signals. The H11F series devices are mounted in dual in-line packages. These devices are also available in surface-mount packaging.

As a Remote Variable Resistor -

- $\leq 100\Omega$  to  $\geq 300M \Omega$
- ≥ 99.9% Linearity
- ≤ 15 pF Shunt Capacitance
- $\geq 100$ G  $\Omega$  I/O Isolation Resistance

As An Analog Signal Switch -

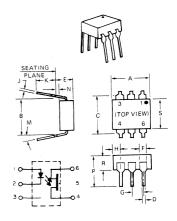
- · Extremely Low Offset Voltage
- 60V pk-pk Signal Capability
- No Charge Injection or Latchup
- $t_{on}$ ,  $t_{off} \le 15 \mu sec$ .

# Absolute Maximum Ratings: (25°C Unless Otherwise Specified)

INFRARED EMITTING DIODE	
Power Dissipation Forward Current (Continuous) Forward Current (Peak)	*100 milliwatts 60 milliamps
(Pulse Width 10 µsec Duty Cycle 1%)	l amp
Reverse Voltage	6 volts
* Derate 1.33 mW/° C above 25° C.	

PHOTO DETECTOR	
Power Dissipation Breakdown Voltage	$T_A = 25^{\circ}C$ **300 milliwatts
H11F1 – H11F2	± 30 volts
H11F3	± 15 volts
Detector Current (Continuous)	±100 milliamps
**Derate 4.0 mW/°C above 25°C.	

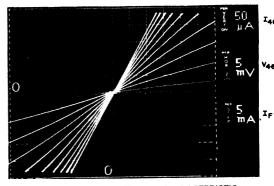
TOTAL DEVICE	
Storage Temperature	-55 to +150°C
Operating Temperature	-55 to +100°C
Lead Soldering Time (at 260°C),	10 Seconds
Surge Isolation Voltage (Input to Output)	
H11F1—H11F3 3535V <sub>(PEAK)</sub>	$2500V_{(RMS)}$
Steady-State Isolation Voltage (Input to Output	)
H11F1—H11F3 3180V <sub>(PEAK)</sub>	$2250V_{(RMS)}$



a) a mou	MILLIMETERS		INC	HES	NOTES
SYMBOL	MIN.	MAX.	MIN.	MAX.	140120
Α	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
C	_	8.64		.340	2
D	.406	.508	.016	.020	
E	-	5.08		.200	3
F	1.01	1.78	.040	.0.70	
G	2.28	2.80	.090	.110	
н		2.16		.085	4
1 1	.203	.305	.008	.012	
К	2.54		.100		
M	-	15		15	
N	.381		.015	-	
P		9.53	-	.375	
R	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	

#### NOTES:

- INSTALLED POSITION LEAD CENTERS
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES



1. TYPICAL LOW LEVEL OUTPUT CHARACTERISTIC

NaCovered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate # 35025

Individual Electrical Characteristics: (25°C Unless Otherwise Specified)

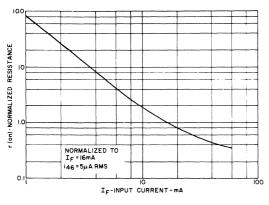
INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage V <sub>F</sub> (I <sub>F</sub> = 16 mA)	1.1	1.75	volts
Reverse Current I <sub>R</sub> (V <sub>R</sub> = 5V)	_	10	microamps
Capacitance C <sub>J</sub> (V = 0, f = 1 MHz)	50	-	picofarads

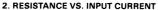
PHOTO-DETECTOR (Either Polarity)	MIN.	MAX.	UNITS
Breakdown Voltage-V(BR) 46			
$(I_{46} = 10\mu A; I_F = 0) - F1.2$	30	-	volts
- F3	15		volts
Off-State Dark Current - I46			
$(V_{46}=15V; I_F=0; T_A=25^{\circ}C)$		50	nanoamps
$(V_{46}=15V;I_F=0;T_A=100^{\circ}C)$		50	microamps
Off-State Resistance - r46			
$(V_{46} = 15V; I_F = 0)$	300	-	megohms
Capacitance – C <sub>46</sub>			
$(V_{46} = 0, I_F = 0, f = 1 \text{ MHz})$	_	15	picofarads

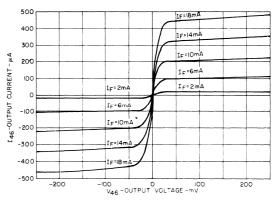
Coupled Electrical Characteristics: (25°C)

		MIN.	TYP.	MAX.	UNITS
On-State Resistance - r <sub>46</sub>					
$(I_F = 16 \text{ mA}, I_{46} = 100 \mu\text{A})$	H11F1	-		200	ohms
	H11F2	-	_	330	ohms
	H11F3	-	_	470	ohms
On-State Resistance - r <sub>64</sub>				İ	
$(I_F = 16 \text{ mA}, I_{64} = 100 \mu\text{A})$	H11F1	l -	-	200	ohms
	H11F2	-	_	330	ohms
	H11F3	_		470	ohms
Isolation Resistance (Input to Output)		l			
$(V_{:IO} = 500V)$		100	-	-	gigohms
Input to Output Capacitance		1	l	l	
$(V_{1O} = 0, f = 1 \text{ MHz})$		_	_	2	picofarads
Turn-On Time - ton				Ì	·
$(I_F = 16 \text{ mA}, R_L = 50 \Omega, V_{46} = 5 V)$		_	_	15	microseconds
Turn-Off Time - toff					
$(I_F = 16 \text{ mA}, R_L = 50 \Omega, V_{46} = 5 V)$		l _		15	microseconds
Resistance, Non-Linearity and Asymmetry					
$(I_F = 16 \text{ mA}, i_{46} = 25 \mu \text{A RMS}, f = 1 \text{ KHz})$		_	_	0.1	percent
					P

#### TYPICAL CHARACTERISTICS (25°C) - EITHER POLARITY

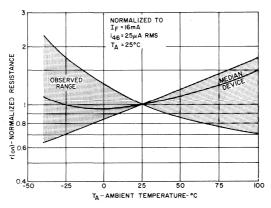




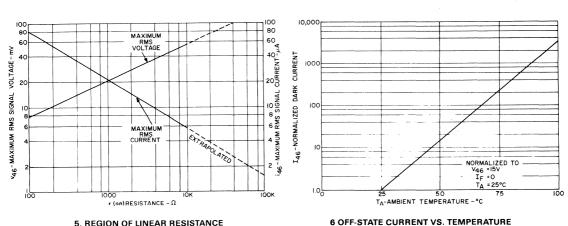


3. OUTPUT CHARACTERISTICS

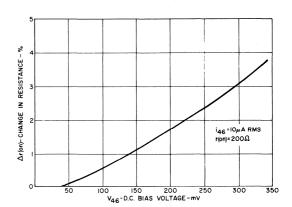
# H11F1, H11F2, H11F3



4. RESISTANCE VS. TEMPERATURE



5. REGION OF LINEAR RESISTANCE



IF - FORWARD CURRENT - MA 0.4

7. INPUT VOLTAGE VS. INPUT CURRENT

VF -- FORWARD VOLTAGE -- VOLTS

8. RESISTIVE NON-LINEARITY VS. D.C. BIAS

# 12

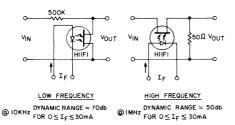
#### H11F1, H11F2, H11F3

#### TYPICAL APPLICATIONS

#### AS A VARIABLE RESISTOR

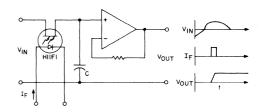
#### AS AN ANALOG SIGNAL SWITCH

#### ISOLATED VARIABLE ATTENUATORS



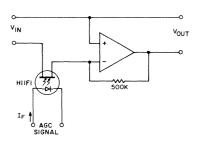
Distortion free attenuation of low level A.C. signals is accomplished by varying the IRED current,  $I_{\rm F}.$  Note the wide dynamic range and absence of coupling capacitors; D.C. level shifting or parasitic feedback to the controlling function.

#### ISOLATED SAMPLE AND HOLD CIRCUIT



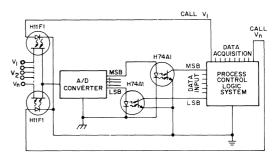
Accuracy and range are improved over conventional FET switches because the H11F has no charge injection from the control signal. The H11F also provides switching of either polarity input signal up to 30V magnitude.

#### **AUTOMATIC GAIN CONTROL**



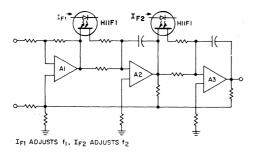
This simple circuit provides over 70db of stable gain control for an AGC signal range of from 0 to 30mA. This basic circuit can be used to provide programmable fade and attack for electronic music and can be modified with six components to a high performance compression amplifier.

#### MULTIPLEXED, OPTICALLY-ISOLATED A/D CONVERSION



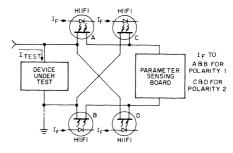
The optical isolation, linearity and low offset voltage of the H11F allows the remote multiplexing of low level analog signals from such transducers as thermocouplers, Hall effect devices, strain gauges, etc. to a single A/D converter.

#### **ACTIVE FILTER FINE TUNING/BAND SWITCHING**



The linearity of resistance and the low offset voltage of the H11F allows the remote tuning or band-switching of active filters without switching glitches or distortion. This schematic illustrates the concept, with current to the H11F1 IRED's controlling the filter's transfer characteristic.

#### TEST EQUIPMENT - KELVIN CONTACT POLARITY



In many test equipment designs the auto polarity function uses reed relay contacts to switch the Kelvin Contact polarity. These reeds are normally one of the highest maintenance cost items due to sticking contacts and mechanical problems. The totally solid-state H11F eliminates these troubles while providing faster switching.

### H11G1, H11G2

# **Optoisolator**

GaAs Infrared Emitting Diode and NPN Silicon Darlington

**Connected Phototransistor** 

The H11G series consists of a gallium arsenide, infrared emitting diode coupled with a silicon Darlington-connected phototransistor which has an integral base-emitter resistor to optimize switching speeds and elevated temperature characteristics. These devices are mounted in dual in-line packages. These devices are also available in surface-mount packaging.

# absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)		
(Pulse width 300 μsec,		
2% Duty Cycle)	0.5	amperes
(Pulse width 1 µsec, 300 Hz)	3	amperes
Reverse Voltage	6	volts
*Derate 1.33 mW/°C above 2	5°C ambient	

*Derate 1.33 mW/°C above	25°C ambien	t.			
DARLINGTON CONNECTED PHOTO-TRANSISTOR					
Power Dissipation	**150	milliwatts			
V <sub>CEO</sub> - H11G1	100	volts			
- H11G2	80	volts			
$V_{CBO}$ – H11G1	100	volts			
– H11G2	80	volts			
$V_{ m EBO}$	7	volts			
Collector Current (Continuous)					
<ul><li>Forward</li></ul>	150	milliamps			
Collector Current (Continuous)					
- Reverse	10	milliamps			

\*\*Derate 2.0 mW/°C above 25°C ambient.

#### MILLIMETERS INCHES NOTES MIN. MAX. MAX MIN. 8.89 330 .350 7.62 REF .300 REF 8.64 .406 .016 .020 3 5.08 200 1.01 .070 2.28 .110 2.80 .090 2.16 203 กกล 012 100 15 .381 .015 9.53 .375 292 3 43 115 .135 6.86 1. INSTALLED POSITION LEAD CENTERS. 2. OVERALL INSTALLED DIMENSION. 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE

# TOTAL DEVICE Storage Temperature -55°C to +150°C Operating Temperature -55°C to +100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output) 5656V<sub>(peak)</sub> 4000V<sub>(RMS)</sub> Steady-State Isolation Voltage (Input to Output) 5300V<sub>(peak)</sub> 3750V<sub>(RMS)</sub>

4. FOUR PLACES.

# individual electrical characteristics:(25°C)

EMITTER	TYP.	MAX.	UNITS
Forward Voltage V <sub>I</sub> (I <sub>F</sub> = 10 mA)	1.1	1.5	volts
Reverse Current I <sub>R</sub> (V <sub>R</sub> = 3 V)	,	10	microamps
Capacitance C <sub>J</sub> (V = O,f = 1 MHz)	50	_	picofarads

DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - V <sub>(BR)CEO</sub>				
$(I_C = 1.0 \text{ mA}, I_F = 0) - H11G1$	100	_	-	volts
- H11G2	80		-	volts
Breakdown Voltage - V(BR)CBO				
$(I_C = 100 \mu A, I_F = O) - H11G1$	100	_		volts
- H11G2	80	_	-	volts
Breakdown Voltage — V <sub>(BR)EBO</sub>	7	-		volts
$(I_E = 100 \mu A, I_F = 0)$				
Collector Dark Current - I <sub>CEO</sub>				
$(V_{CE} = 80 \text{ V}, I_F = 0) - \text{H}11\text{G}1$			100	nanoamps
$(V_{CE} = 60 \text{ V}, I_F = 0) - \text{H11G2}$		ı— "	100	nanoamps
$(V_{CE} = 80 \text{ V}, I_F = 0, T_A = 80^{\circ}\text{C})$				
- H11G1	-	_	100	microamps
$(V_{CE} = 60 \text{ V}, I_F = 0, T_A = 80^{\circ}\text{C})$				
- H11G2	-	_	100	microamps
Capacitance	-	6	-	picofarads
$(V_{CE} = 10V, f = 1 MHz)$				

NA Covered under U.L. component recognition program, reference file E51868

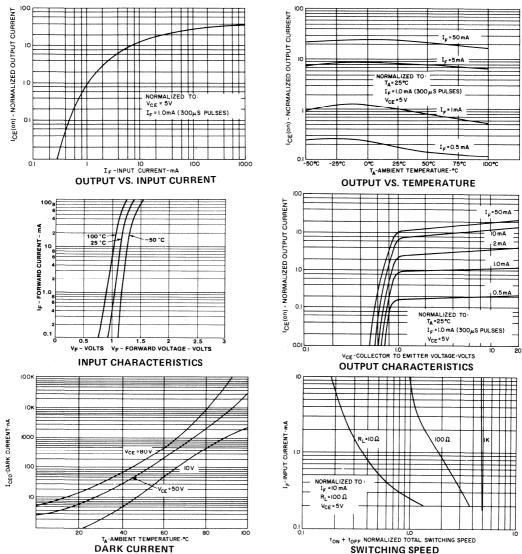
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# H11G1, H11G2

# coupled electrical characteristics:(25°C)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio $- (I_F = 10 \text{ mA}, V_{CE} = 1 \text{ V})$	1000	_		%
$- (I_F = 1 \text{ mA}, V_{CE} = 5 \text{ V})$	500	-		%
Saturation Voltage – Collector to Emitter – $(I_F = 1 \text{ mA}, I_C = 1 \text{ mA})$		0.75	1.0	volts
$- (I_F = 16 \mathrm{mA}, I_C = 50 \mathrm{mA})$	-	0.85	1.0	volts
Isolation Resistance (Input to Output Voltage = $500  V_{DC}$ )	100	-		gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1 MHz)	_		2	picofarads
Switching Speeds:				
On-Time – $(V_{CE} = 5 \text{ V}, R_L = 100 \Omega, I_F = 10 \text{ mA})$		5	-	microseconds
Off-Time – (Pulse width $\leq 300 \mu\text{sec}$ , $f \leq 30 \text{Hz}$ )	_	100	-	microseconds

#### TYPICAL CHARACTERISTICS

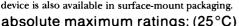


#### H11G3

# **Optoisolator**

# **GaAs Infrared Emitting Diode and NPN Silicon Darlington Connected Phototransistor**

The H11G series consists of a gallium arsenide, infrared emitting diode coupled with a silicon Darlington-connected phototransistor which has an integral base-emitter resistor to optimize switching speeds and elevated temperature characteristics. The H11G3 is mounted in a dual in-line package. This device is also available in surface-mount packaging.



INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)		
(Pulse width 300 µsec,		
2% Duty Cycle)	0.5	amperes
(Pulse width 1 µsec, 300 Hz)	3	amperes
Reverse Voltage	6	volts
*Derate 1.33 mW/°C above 2	5°C ambient	:

PLANE
177 H-K-175 - 1- A
3 10 1
B C (TOP VIEW) S
M 4 6
1-777
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G

	SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
	Α	8.38	8.89	.330	.350	
	В	7.62	REF.	.300	REF.	1
	С	-	8.64	-	.340	2
	D	.406	.508	.016	.020	
	E	-	5.08	-	.200	3
	F	1.01	1.78	.040	.070	
	G	2.28	2.80	.090	.110	
	н	-	2.16		.085	4
-	J	.203	.305	.008	.012	
1	К	2.54	- '	.100	-	
5	M	-	15		15	
	N	.381		.015	-	
Ŀ	Р	-	9.53		.375	
	. R	2.92	3.43	.115	.135	
	S	6.10	6.86	.240	.270	

NOTES:

1. INSTALLED POSITION LEAD CENTERS.

2. OVERALL INSTALLED DIMENSION.

MILLIMETERS

- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES.

DARLINGTON CONNECTED PHOTO-TRANSISTOR				
Power Dissipation	**150	milliwatts		
$V_{CEO}$	55	volts		
$V_{CBO}$	55	volts		
$V_{EBO}$	7	volts		
Collector Current (Continuous)				
<ul><li>Forward</li></ul>	100	milliamps		
Collector Current (Continuous)				
- Reverse	10	milliamps		
**Derate 2.0 mW/°C above 2	25°C ambien	ıt.		

#### TOTAL DEVICE

Storage Temperature -55°C to +150°C Operating Temperature -55°C to +100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output)

> 2500V(RMS)  $3535V_{(peak)}$

Steady-State Isolation Voltage (Input to Output) 3180V<sub>(peak)</sub> 2280V(RMS)

# individual electrical characteristics:(25°C)

EMITTER	TYP.	MAX.	UNITS
Forward Voltage V <sub>F</sub> (I <sub>F</sub> = 10 mA)	1.1	1.5	volts
Reverse Current $I_R$ $(V_R = 3 V)$	<u>-</u>	10	microamps
Capacitance C <sub>J</sub> (V = O,f = 1 MHz)	50	_	picofarads

DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage $-V_{(BR)CEO}$ ( $I_C = 1.0 \text{ mA}, I_F = O$ )	55	-	- ,	volts
Breakdown Voltage $-V_{(BR)CBO}$ ( $I_C = 100 \mu A, I_F = O$ )	55		-	volts
Breakdown Voltage $-V_{(BR)EBO}$ $(I_E = 100 \mu A, I_F = O)$	7	-	-	volts
Collector Dark Current $-I_{CEO}$ ( $V_{CE} = 30 \text{ V}, I_{F} = 0$ )	-	5	100	nanoamps
Capacitance $(V_{CE} = 10 \text{ V}, f = 1 \text{ MHz})$	-	6	-	picofarads

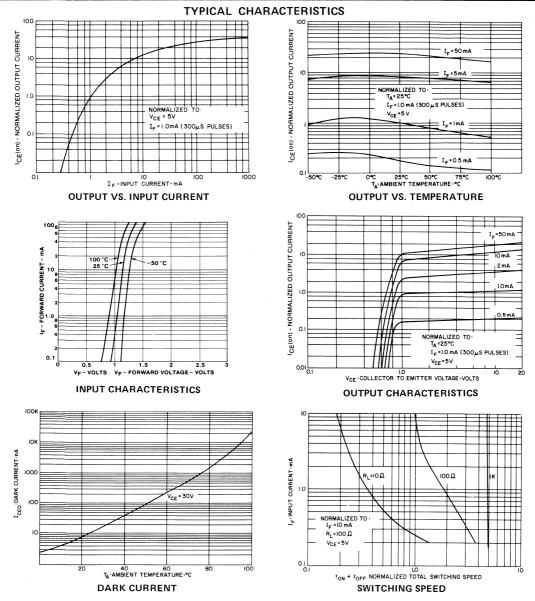
Nu Covered under U.L. component recognition program, reference file E51868

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#### H11G3

# coupled electrical characteristics:(25°C)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio $(I_F = 1 \text{ mA}, V_{CE} = 5 \text{ V})$	200			%
Saturation Voltage – Collector to Emitter $(I_F = 20 \text{ mA}, I_C = 50 \text{ mA})$	-	0.85	1.2	volts
Isolation Resistance (Input to Output Voltage = 500 V <sub>DC</sub> )	100		~	gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1 MHz)	-		2	picofarads
Switching Speeds:				
On-Time $- (V_{CE} = 5 V, R_L = 100 \Omega, I_F = 10 mA)$	-	5		microseconds
Off-Time – (Pulse width $\leq 300 \mu\text{sec}$ , $f \leq 30 \text{Hz}$ )	-	100	~	microseconds



# H11G45, H11G46

# **Optoisolator**

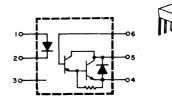
# **GaAs Infrared Emitting Diode and NPN Silicon Darlington Connected Phototransistor**

The H11G series consists of a gallium arsenide, infrared emitting diode coupled with a silicon Darlington-connected phototransistor which has an integral base-emitter resistor to optimize switching speeds and elevated temperature characteristics. These devices are designed to equal the 4N45 and 4N46 characteristics while providing greater voltage and current capability. These devices are mounted in a dual in-line package. These devices are also available in surface-mount packaging.

absolute maximum ratings: (25°C)

Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)		· <del>-</del>
(Pulse width 300 μsec,		
2% Duty Cycle)	0.5	amperes
(Pulse width 1 µsec, 300 Hz)	3	amperes
Reverse Voltage	6	volts

\*Derate 1.33 mW/°C above 25°C ambient.





	SYMBOL	MILLIMETERS		INC	HES	NOTES
A	STIMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
ллл	Α	8.38	8.89	.330	.350	
المنات ال	В	7.62	REF.	.300	REF.	1 1 1
3 1•	С		8.64	_	.340	2
C (TOP VIEW) S	D	406	.508	.016	.020	1
4 6	E	_	5.08		.200	3
	F	1.01	1.78	.040	.070	
	G	2.28	2.80	.090	.110	
	н		2.16	-	.085	4
]  H   F	J	.203	.305	.008	.012	1
+	к	2.54	-	.100	-	
	M	-	15		15	
	N	.381	-	.015	-	
1 11 11 11 11	Р	-	9.53		.375	
u w w	R	2.92	3.43	.115	.135	
G   D	S	6.10	6.86	.240	.270	

- NOTES:

  1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES

DARLINGTON CONNECTED PHOTO-TRANSISTOR				
Power Dissipation	**150	milliwatts		
Output Voltage VO (Pin 5-4)	55	volts		
Reverse Voltage V <sub>B</sub> (Pin 4-6)	7	volts		
Output Current (Continuous)				
- Forward	100	milliamps		
Output Current (Continuous)				
- Reverse	10	milliamps		
**Derate 2.0 mW/°C abov	ve 25°C ambier	it.		

#### TOTAL DEVICE

Storage Temperature -55°C to +150°C Operating Temperature -55°C to +100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output) 5656V<sub>(peak)</sub> 4000V(RMS) Steady-State Isolation Voltage (Input to Output)

5300V<sub>(peak)</sub> 3750V<sub>(RMS)</sub>

# individual electric characteristics: (0-70°C)

EMITTER	TYP.	MAX.	UNITS
Forward Voltage V <sub>F</sub> (I <sub>F</sub> = 10 mA)	1.1	1.7	volts
Reverse Current I <sub>R</sub> (V <sub>R</sub> = 3V)		100	microamps
Capacitance C <sub>J</sub> (V = 0, f = 1 MHz)	50	<del></del>	picofarads

DETECTOR	MIN.	TYP.	MAX.	UNITS
Output Breakdown Voltage (Pin 5-4)	55	_	_	volts
$I_{54} = 1.0 \text{mA}, I_F = 0$	1			
Base Breakdown Voltage	7			volts
(Pin 4-6)				
$I_{46} = 100 \mu A, I_F = 0$				
Logic High Output			100	microamps
$(V_{54} = 18V, I_F = 0)$				
Capacitance		6		picofarads
$(V_{54} = 10V, f = 1MHz)$	- 9			

No Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate # 35025

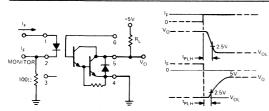
# H11G45, H11G46

# coupled electrical characteristics (0-70°C)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio — I <sub>F</sub> = 0.5mA, V <sub>O</sub> = 1.0V H11G46	350	A,		%
$I_F = 1.0 \text{mA}, V_O = 1.0 \text{V}$ H11G46	500			%
$I_F = 1.0 \text{mA}, V_O = 1.0 \text{V}$ H11G45	250			%
$I_F = 10 \text{mA}, V_O = 1.2 \text{V}$ H11G45, H11G46	200	10 T		%
Logic Low Output Voltage — I <sub>F</sub> = 0.5mA, I <sub>OL</sub> = 1.75mA H11G46			1.0	volts
$I_F = 1.0 \text{mA}, I_{OL} = 5.0 \text{mA}$ H11G46			1.0	volts
$I_F = 1.0 \text{mA}, I_{OL} = 2.5 \text{mA}$ H11G45	_		1.0	volts
I <sub>F</sub> = 10mA, I <sub>OL</sub> = 20mA H11G45, H11G46	<u> </u>		1.2	volts
Isolation Resistance (Input to Output Voltage = 500VDC)				gigaohms
Input to Output Capacitance (Input to Output Voltage = 0, f = 1MHz)			2	picofarads

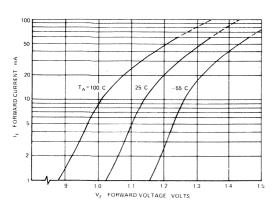
# switching characteristics (25°C)

		MIN.	TYP.	MAX.	UNITS
Propagation Delay Time to $I_F$ = 1.0mA, $R_L$ = 10K $\Omega$ Logic Low at Output $I_F$ = 10mA, $R_L$ = 220 $\Omega$	t PHL	-	80 5	— 50	microseconds microseconds
Propagation Delay Time to $I_F$ = 1.0mA, $R_L$ = 10K $\Omega$ Logic High at Output $I_F$ = 10mA, $R_L$ = 220 $\Omega$	t PLH t PLH		1500 150	<u> </u>	microseconds microseconds
Common Mode Transient $I_F$ = 0mA, $R_L$ = 10K $\Omega$ Immunity at Logic High $(V_{CM})$ = 10Vp-p Level Output	CM <sub>H</sub>		500		volts microsecond
Common Mode Transient $I_F$ = 1.0mA, $R_L$ = 10K $\Omega$ Immunity at Logic Low $(V_{CM})$ = 10Vp-p Level Output	CM <sub>L</sub>		500	<del></del> '.	volts microsecond



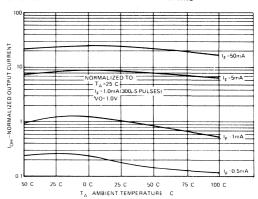
# 

#### SWITCHING TEST CIRCUIT



FORWARD VOLTAGE VS. FORWARD CURRENT

# TEST CIRCUIT FOR TRANSIENT IMMUNITY AND TYPICAL WAVEFORMS



**OUTPUT VS. TEMPERATURE** 

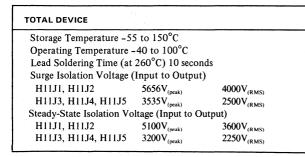
# Optoisolator GaAs Infrared Emitting Diode and Light Activated Triac Driver

The H1 IJ series consists of a gallium arsenide infrared emitting diode coupled with a light activated silicon bilateral switch, which functions like a triac, in a dual in-line package. These devices are also available in surface-mount packaging.

# absolute maximum ratings: (25°C)

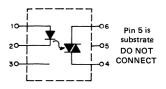
INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	amperes
(Pulse width 1 $\mu$ sec. 300 pps)		
Reverse Voltage	3	volts
*Derate 1.33 mW/°C abo	ve 25°C ambier	nt.

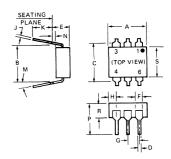
OUTPUT DRIVER		
Off-State Output Terminal Voltage	250	volts
On-State RMS Current	100	milliamps
(Full Cycle Sine Wave, 50 to 60 Hz)		
Peak Nonrepetitive Surge Current	1.2	amperes
(PW = 10  ms, DC = 10%)		
Total Power Dissipation @ $T_A = 25^{\circ}C$	**300	milliwatts
**Derate 4.0 mW/°C above	25°C.	



Covered under U.L. component recognition program, reference file E51868







SYMBOL	MILLIN	ETERS	INC	HES	NOTES
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
С	_	8.64	-	.340	2
D	.406	.508	.016	.020	
E	-	5.08	- 1	.200	3
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
н		2.16	-	.085	4
J	.203	.305	.008	.012	
к	2.54		.100	-	
M	***	15°	-	15	
N	.381	-	.015	-	
Р	-	9.53	-	.375	
R	2.92	3.43	.115	.135	
s	6.10	6.86	.240	.270	

#### NOTES

- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES.

# individual electrical characteristics (25°C)

EMITTER	SYMBOL	TYP.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> = 10 mA)	V <sub>F</sub>	1.2	1.5	volts
Reverse Current (V <sub>R</sub> = 3V)	I <sub>R</sub>	_	100	microamps
Capacitance (V = O, f = 1 MHz)	$\mathrm{C}_{\mathrm{J}}$	50	-	picofarads

DETECTOR	See Note 1		SYMBOL	TYP.	MAX.	UNITS
Peak Off-State Current		$V_{DRM} = 250V$	I <sub>DRM</sub>	_	100	nanoamps
Peak On-State Voltage		$I_{TM} = 100 \text{ mA}$	V <sub>TM</sub>	2.5	3.0	volts
Critical Rate-of-Rise of	Off-State Voltage	$Vin = 30V_{(RMS)}$ (See Figure 6)	dv/dt	4.0	_	volts/μsec.
Critical Rate-of-Rise of Off-State Voltage	Commutating	$I_{load}$ = 15 mA Vin = 30V <sub>(RMS)</sub> (See Figure 6)	dv/dt <sub>(C)</sub>	0.15	-	volts/μsec.
Critical Rate-of-Rise of	Off-State Voltage	$V_{in} = 120V_{(RMS)}$ JEDEC conditions	dv/dt	2.0	_	volts/μsec.

# coupled electrical characteristics (25°C)

		SYMBOL	TYP.	MAX.	UNITS	
IRED Trigger Current, Current Required to Latch Output	H11J1, H11J3	$I_{FT}$	_	10	milliamps	
(Main Terminal Voltage = 3.0V, $R_L = 150 \Omega$ )	H11J2, H11J4	$I_{\mathrm{FT}}$	_	15	milliamps	
	H11J5	$I_{FT}$	_	25	milliamps	
					milliamps	
Holding Current, Either Direction		I <sub>H</sub>	250		microamps	
(Main Terminal Voltage 3.0V, Initiating Current – 10 m	<b>A</b> )					

NOTE 1: Ratings apply for either polarity of Pin 6 - referenced to Pin 4.

#### TYPICAL CHARACTERISTICS

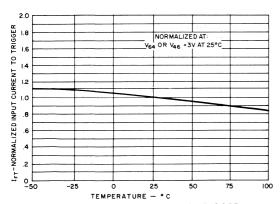


FIGURE 1. INPUT CURRENT TO TRIGGER VS. TEMPERATURE

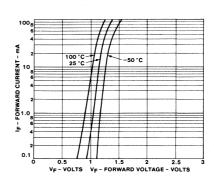


FIGURE 2. FORWARD VOLTAGE VS. FORWARD CURRENT

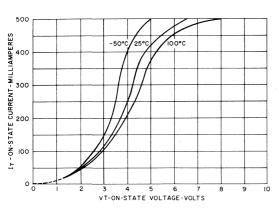


FIGURE 3. ON-STATE VOLTAGE VS.
OUTPUT CURRENT

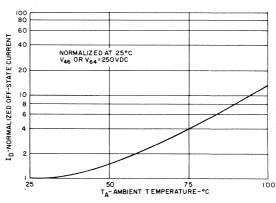


FIGURE 4. OFF-STATE CURRENT VS. TEMPERATURE

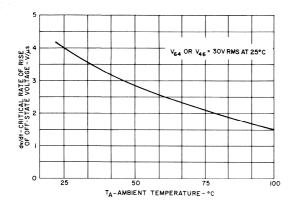


FIGURE 5. dv/dt VS. TEMPERATURE

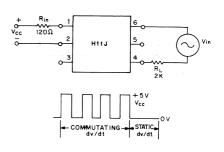
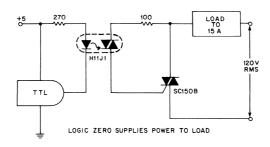
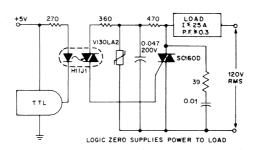


FIGURE 6. dv/dt - TEST CIRCUIT

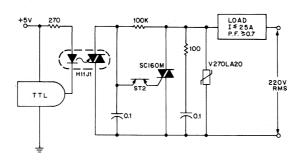
# TYPICAL APPLICATION CIRCUITS TTL COMPATIBLE LOGIC CONTROL OF POWER LINE



RESISTIVE LOAD AND NON-CRITICAL APPLICATIONS
LOW COST, LIMITED NOISE AND dv/dt IMMUNITY



INDUCTIVE LOADS AND CRITICAL APPLICATIONS
GOOD dv/dt AND NOISE IMMUNITY



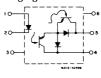
INDUSTRIAL VOLTAGES AND CRITICAL APPLICATIONS EXCELLENT dv/dt, NOISE AND OVERVOLTAGE CAPABILITY

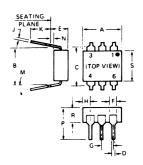
# **Optoisolator**

# **GaAlAs Infrared Emitting Diode and** Two NPN Silicon Photo-Darlington Amplifiers



The H11K series consists of a gallium-aluminum-arsenide, infrared emitting diode coupled with two high voltage silicon Darlingtonconnected phototransistors which have integral base-emitter resistors to optimize switching speeds and elevated temperature characteristics. The two photo-Darlingtons are inverse-series-connected and have steering diodes to provide ac and bidirectional dc current switching controlled by the IRED. These devices are mounted in dual in-line packages. These devices are also available in surface-mount packaging.





#### absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE					
Power Dissipation	*100	milliWatts			
Forward Current (Continuous)	60	milliamps			
Forward Current (Peak) (Pulse Width 10 µsec Duty Cycle	3 e 1%) 1	ampere ampere			
Reverse Voltage	6	volts			
*Derate 1.33mW/°C above 25°C ambient.					

	MILLIMETERS				
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	8.38	8.89	.330	.350	
В	7.62 REF.		.300	REF.	1
С		8.64	1	.340	2
D	.406	.508	0.16	.020	1
E		5.08		.200	3
F	1.01	1.78	.040	.070	1
G	2.28	2.80	.090	.110	i
н (		2.16	[ ]	.085	4
J	.203	.305	.008	.012	
K	2.54		.100		1
M	-	15*	1	15*	1
N	.381		.015		ł
Р		9.53	1	.375	1
R '	2.92	3.43	.115	.135	1
s	6.10	6.86	.240	.270	1

- NOTES

  1. INSTALLED POSITION LEAD CENTERS.
  2. OVERALL INSTALLED DIMENSION.
  3. THESE MEASUREMENTS ARE MADE FROM THE SEATING
- PLANE. 4. FOUR PLACES.

PHOTO DETECTOR	H11K1	H11K2	
Power Dissipation**	400	400	milliwatts
Detector Current			
(dc)	150	120	milliamps
(RMS ac)	200	150	milliamps
V <sub>45, 54</sub>	250	200	volts
**Derate 5.3 mW/°C above 2	5°C ambien	it.	

Nu Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80

#### **TOTAL DEVICE**

Storage Temperature -55°C to +150°C

Operating Temperature -55 to 100°C

Lead Soldering Time (at 260°C) 10 seconds

Surge Isolation Voltage (Input to Output)

3535 V<sub>(peak)</sub> 2500 V<sub>(RMS)</sub>

Steady-State Isolation Voltage (Input to Output). 3180 V<sub>(neak)</sub> 2250  $V_{(RMS)}$ 

# Individual electrical characteristics (25°C)

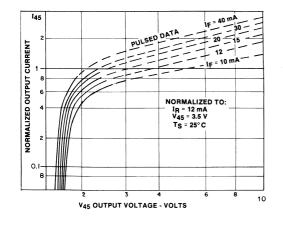
INFRARED EMITTING DIODE	MAX.	UNITS
Forward Voltage $V_F$ ( $I_F = 16 \text{ mA}$ )	1.75	volts
Reverse Current $I_R$ $(V_R = 5 V)$	10	μΑ
Capacitance C <sub>J</sub> V <sub>R</sub> = 0 V, f = 1 MHz	100	pF

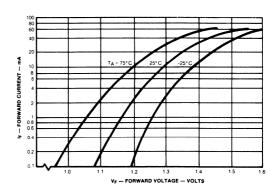
PHOTO-DETECTOR (Either Polarity)	MAX.	UNITS
Leakage Current (dc) V <sub>45</sub> = 200 V, H11K1	200	nA
V <sub>45</sub> = 165 V, H11K2 Leakage Current (RMS ac)	200	nA
$T_j$ = 65° C, H11K1 $V_{as}$ = 100 V RMS ac @ 160 Hz	10	μΑ
Capacitance $V_{45} = 50 \text{ V}, f = 1 \text{ MHz}$	20	pF

# coupled electrical characteristics: (25°C)

(Either Polarity)		MIN.	TYP.	MAX.	UNITS
D.C. Current Transfer Ratio - $(I_F = 12 \text{ mA}, V_{45} = 3.5 \text{ V})$ $(I_F = 20 \text{ mA}, V_{45} = 4.0 \text{ V})$	H11K1 H11K2	1000 500	×1		% %
On State Voltage - $(I_F = 12 \text{ mA}, I_{45} = 100 \text{ mA})$ $(I_F = 16 \text{ mA}, I_{45} = 75 \text{ mA})$	H11K1 H11K2			2.5 2.5	volts volts
Isolation Resistance (Input to Output Voltage = $500 V_{DC}$ )		100			GΩ
Input to Output Capacitance ( $V_{10} = 0$ , $f = 1$ MHz)				2	pF
Switching Speeds: $(V_{CC} = 48V, R_1 = 500\Omega, I_F = 16 \text{ mA})$ Pulse width = 300 $\mu$ sec, f = 30 Hz)					
On Time Off Time			20 40		μs μs

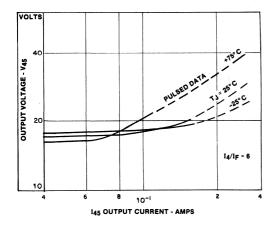
#### TYPICAL CHARACTERISTICS (25°C) — EITHER POLARITY

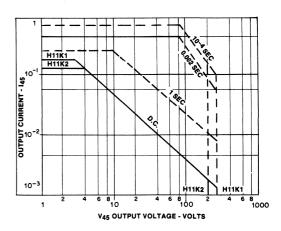




1. OUTPUT CHARACTERISTICS

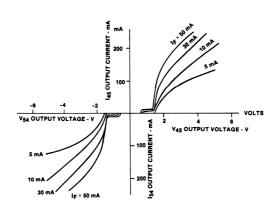
2. INPUT VOLTAGE VS. INPUT CURRENT



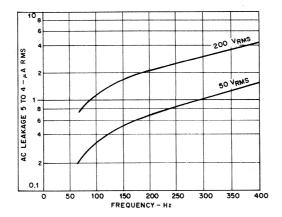


3. SATURATION REGION

4. FORWARD BIAS SAFE OPERATING AREA



5. TYPICAL CHARACTERISTICS (25°C)



6. AC DARK CURRENT VS. FREQUENCY

# **Optoisolator**

# GaAs Infrared Emitting Diode and Microprocessor Compatible Schmitt Trigger

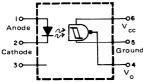
The H11L series has a gallium arsenide, infrared emitting diode optically coupled across an isolating medium-to-high speed integrated circuit detector. The output incorporates a Schmitt trigger which provides hysteresis for noise immunity and pulse shaping. The detector circuit is optimized for simplicity of operation and utilizes an open collector output for maximum application flexibility. These devices are mounted in dual in-line packages. These devices are also available in surface-mount packaging.

#### **FEATURES**

- Free from latch up and oscillation throughout voltage and temperature ranges
- High data rate, 1 MHz typical (NRZ)
- Microprocessor compatible drive
- Logic compatible output sinks 16 milliamperes at 0.4 volts maximum
- High isolation between input and output
- Guaranteed On/Off threshold hysteresis
- High common mode rejection ratio
- Fast switching: t rise, t fall = 100 nanoseconds typical
- Wide supply voltage capability, compatible with all popular logic systems

#### MECHANICAL SPECIFICATIONS

- Plastic 6 PIN dual in line package, tin plated leads
- Lead orientation as shown:





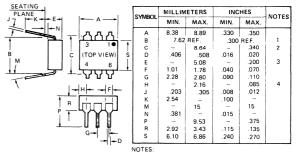
# absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliampere
Forward Current (Peak)	3	amperes
(Pulse Width 1 µsec 300pps)		•
Reverse Voltage	6	volts
*Derate 1.33 mW°C abov	ve 25°C ai	mbient.

PHOTO DETECTOR						
Power Dissipation	**150	milliwatts				
V <sub>45</sub> Allowed Range	0 to 16	volts				
V <sub>65</sub> Allowed Range	0 to 16	volts				
I <sub>4</sub> Output Current	50	milliampere				
**Derate 2.0 mW/°C above 25°C ambient.						

#### **APPLICATIONS**

- Logic to logic isolator
- Programmable current level sensor
- Line receiver eliminates noise and transient problems
- Logic level shifter couples TTL to CMOS
- A.C. to TTL conversion square wave shaping
- Digital programming of power supplies
- Interfaces computers with peripherals



- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION
- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE. 4. FOUR PLACES.

#### TOTAL DEVICE

Storage Temperature -55°C to +150°C
Operating Temperature -55°C to +100°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output)
3535 V<sub>(peak)</sub> 2500 V<sub>(RMS)</sub>
Steady-State Isolation Voltage (Input to Output)
3180V<sub>(peak)</sub> 2250V<sub>(RMS)</sub>

VDE Approved to 0883/6.80 0110b Certificate #35025

Covered under U.L. component recognition program, reference file E51868

# electrical characteristics: (TA = 0-70°C)

INFRARED EMITTING DIODE		MIN.	TYP.	MAX.	UNITS	PHOTO DETECTOR		MIN.	TYP.	MAX.	UNITS
Forward Voltage  I <sub>I</sub> : = 10 mA  I <sub>F</sub> = 0.3 mA  Reverse Current  (V <sub>R</sub> = 3V)  Capacitance  (V = 0, f = 1 MHz)	V <sub>F</sub>	0.75 - -	1.10 0.95 - -	1.50 - 10 100	volts volts micro- ampere picofarads	Operating Voltage Range Supply Current (IF = 0, V <sub>CC</sub> = 5V) Output Current, High (IF = 0, V <sub>cc</sub> =V <sub>o</sub> =15V)	V <sub>CC</sub> I <sub>6(off)</sub> I <sub>OH</sub>	3 - -	1.0	15 5.0 100	volts milli- ampere micro- ampere

# coupled electrical characteristics (TA = 0-70°C)

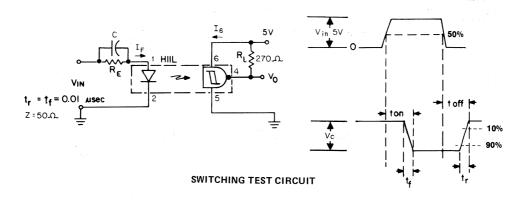
		MIN.	TYP.	MAX.	UNITS
Supply Current $(I_F = 10 \text{ mA}, V_{CC} = 5 \text{ V})$	I <sub>6(on)</sub>	-	1.6	5.0	milliampere
Output Voltage, Low $(R_{64} = 270 \Omega, V_{CC} = 5V, I_F = I_{F(on)} Max)$	$V_{OL}$	-	0.2	0.4	volts
Turn-On Threshold Current $(R_{64}=270 \Omega, V_{CC}=5V)$	I <sub>F(on)</sub> H11L1 H11L2 H11L3	_ _ _	1.0 6.0 3.0	1.6 10.0 5.0	milliampere milliampere milliampere
Turn-Off Threshold Current $(R_{64} = 270\Omega, V_{CC} = 5V)$	$I_{F(off)}$	0.3	1.0	-	milliampere
Hysteresis Ratio $(R_{64}^{=} 270 \Omega, V_{CC} = 5V)$	$I_{F(off)}/I_{F(on)}$	0.50	0.75	0.90	-

# switching characteristics (25°C) H11L1

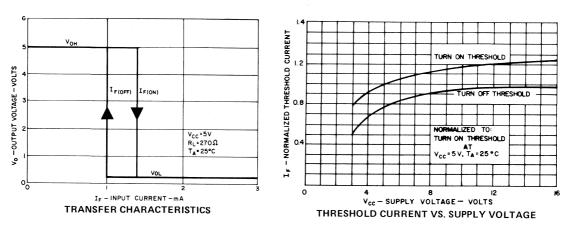
SWITCHING SPEED		MIN.	TYP.	MAX.	UNITS
$R_E = 1200\Omega$ , C=0			,		
Turn- On Time	ton		1.0		μsec.
Fall Time Turn-Off Time	t <sub>f</sub> t <sub>off</sub>	-	0.1 2.0	_	μsec. μsec.
Rise Time	t <sub>r</sub>		0.1	-	μsec.
$R_E$ =1200Ω, C=270ρF, f≤100KHz, tp≥1 $\mu$ sec Turn-On Time	ton		0.65		μsec.
Fall Time Turn-Off Time	t <sub>f</sub>	_	0.05 1.20	_	μsec. μsec.
Rise Time	off t <sub>r</sub>	_	0.07	_	μsec.
Data Rate (NRZ)  Overdrive Switching (IF (Max. ) = 33mA)		-	1.0*	_	MHz
$V_{\rm IN}$ = 5V DC, $R_{\rm E}$ = 120 $\Omega$ , C = 0, $V_{\rm CC}$ = 5V, $R_{\rm L}$ = 270 $\Omega$ Turn-Off Time	t <sub>off</sub>	_	-	.10	μsec.

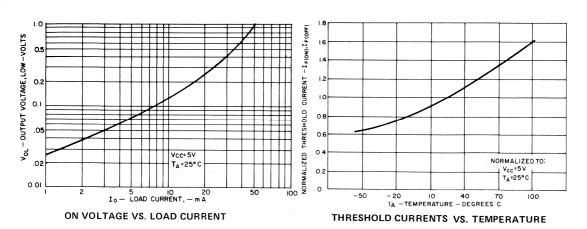
<sup>\*</sup>Maximum data rate will vary depending on the bias conditions and is usually highest when  $R_E$  and C are matched to  $I_{F(o\,n)}$  and  $V_{CC}$  is between 3 and 5V, with this optimized bias, most units will operate at over 1.5 MHz, NRZ.

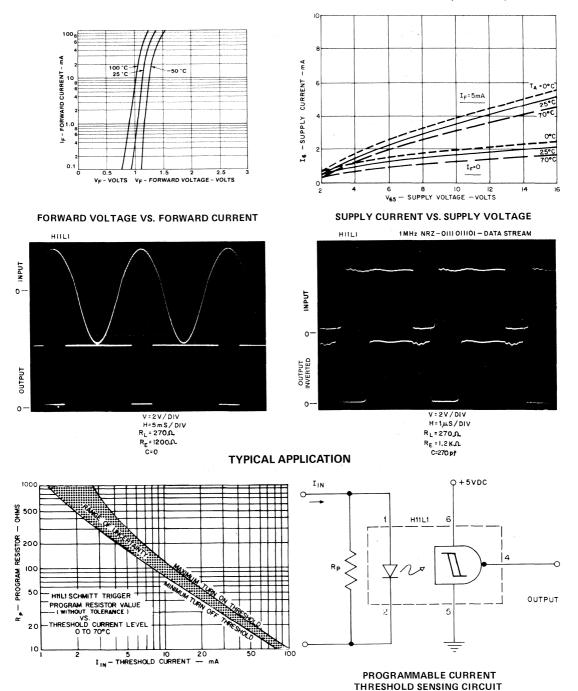
# switching characteristics (25°C) H11L1



#### TYPICAL CHARACTERISTICS







PLEASE NOTE: THE INFORMATION INCLUDED IN THIS SPECIFICATION HAS BEEN CAREFULLY CHECKED AND IS BELIEVED TO BE RELIABLE, HOWEVER, NO RESPONSIBILITY IS ASSUMED FOR INACCURACIES.

#### H11M1, H11M2

# **Optoisolator GaAlAs Infrared Emitting Diode and Light Activated SCR**

The H11M1 and H11M2 contain a gallium-aluminum-arsenide, infrared emitting diode coupled to a unique high voltage silicon controlled rectifier within a dual in-line package. These devices are optimized for high performance and long life. They are especially suited for the control of industrial AC power lines from low voltage logic integrated circuitry. These devices are also available in surface-mount packaging.

#### **FEATURES**

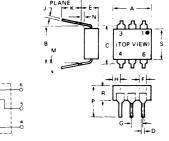
- High blocking voltage, 800 V minimum
- High isolation voltage, 3750 Vrms minimum (steady state)
- High efficiency, low degradation, liquid epitaxial IRED
- Logic compatible drive current, 7 mA at 1.5 V maximum
- Unique, high performance glass dielectric construction

# absolute maximum ratings: (25°C)

Power Dissipation	*100	milliWatts
Forward Current (Continuous)	60	milliAmpere
Forward Current (Peak) (Pulse width 10 µsec		
Duty Cycle 1%)	1	Ampere
Reverse Voltage	6	volts

PHOTO-SCR					
Peak Forward Voltage	800	Volts			
RMS Forward Current	300	milliAmperes			
Peak On-State Current (1 cycle surge, 10 msec)	3	Amperes			
Peak Reverse Gate Voltage	5	Volts			
Power Dissipation (25°C Ambient)  **Derate 5.3 mW/°C above 25°C ambient.	**400	milliWatts			





- 1	MILLIM	MILLIMETERS INCHES		MILLIMETERS		
SYMBOL MIN.	MAX.	MIN.	MAX.	NOTES		
A	8.38	8.89	.330	.350		
В	7.62	REF.	.300	REF.		
C		8.64		.340	2	
D I	.406	.508	0.16	.020		
F		5.08		.200	3	
E F	1.01	1.78	.040	.070		
G	2.28	2.80	.090	110		
н		2.16	11.2	.085	4	
1.01	.203	.305	.008	.012		
ĸ	2.54		.100	400	4.1	
М		15°		15°		
N	.381		.015	120 700		
P.		9.53		.375	96.	
R	2.92	3.43	.115	.135	100	

- IOTES
  INSTALLED POSITION LEAD CENTERS.
  OVERALL INSTALLED DIMENSION.
  THESE MEASUREMENTS ARE MADE FROM THE SEATING
- 4 FOUR PLACES

#### **TOTAL DEVICE**

Storage Temperature -55°C to +150°C

Operating Temperature -55 to +100°C

Lead Soldering Time (at 260°C) 10 seconds

Surge Isolation Voltage (Input to Output)

4000 V<sub>(RMS)</sub> 5656 V<sub>(peak)</sub>

Steady-State Isolation Voltage (Input to Output).

3750 V<sub>(RMS)</sub> 5300 V<sub>(neak)</sub>

Na Covered under U.L. component recognition program, reference file E51868

# H11M1, H11M2

# individual electrical characteristics (25°C) (unless otherwise indicated)

EMITTER	SYMBOL	TYP.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> = 10 mA)	V <sub>F</sub>	1.3	1.65	V
Reverse Current (V <sub>R</sub> = 5V)	I <sub>R</sub>		10	μA
Capacitance $(V_{AK} = 0V, F = 1 \text{ MHz})$	C <sub>j</sub>	50		pF

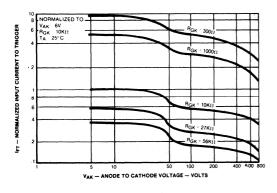
DETECTOR	SYMBOL	MIN.	TYP.	MAX.	UNITS
Off-State Voltage $(R_{GK} = 10K\Omega, I_D = 100\mu A, T_A = 100^{\circ}C)$	V <sub>DM</sub>	800			V
Reverse Voltage $(R_{GK} = 10K\Omega, I_R = 100\mu A, T_A = 100^{\circ}C)$	V <sub>RM</sub>	800		4	V
On-State Voltage (I <sub>1M</sub> = 300mA)	V <sub>TM</sub>			1.5	V
Off-State Current $(R_{GK} = 10K\Omega, V_{DM} = 800V, T_A = 100^{\circ}C)$ $(T_A = 25^{\circ}C)$	I <sub>DM</sub>	_		100 400	μA nA
Reverse Current $(R_{GK} = 10K\Omega, V_{RM} = 800V, T_A = 100^{\circ}C)$ $(T_A = 25^{\circ}C)$	I <sub>RM</sub>	- -		100 400	μA nA
Critical Rate-of-Rise of Off-State Voltage $(V_{AK} = 800V, R_{GK} = 10K\Omega)$	dv/dt		25		V/µsec
Holding Current $(R_{GK} = 10K\Omega)$	I <sub>H</sub>			2	mA

# coupled electrical characteristics (25°C)

COUPLED		SYMBOL	MIN.	TYP.	MAX.	UNITS
Input Current to Trigger $(V_{AK} = 6V, R_{GK} = 10K\Omega)$	HIIMI HIIM2	I <sub>FT</sub>			10 20	mA mA
Input Current to Trigger $(V_{AK} = 6V, R_{GK} = 27K\Omega)$	H11M1 H11M2	I <sub>FT</sub>			7 15	mA mA
Isolation Resistance (Input to Output) $(V_{IO} = 500V)$		r <sub>io</sub>	100			GΩ
Isolation Capacitance (Input to Output) (V <sub>10</sub> = 0V, F = 1 MHz)		c <sub>io</sub>			2	pF
Isolation dv/dt Immunity (Input to Output) See Figure 10			500			V/µsec

Tests of input to output isolation voltage, isolation resistance, and isolation capacitance are performed with the input terminals (pins 1, 2 & 3) shorted together and the output terminals (pins 4, 5 & 6) shorted together.

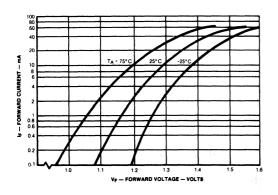
# H11M1, H11M2

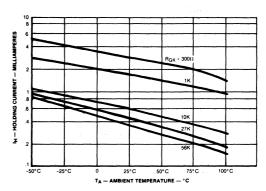


| NORMALIZED TO | NORMALIZED TO | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 67 | YAK 6

1. INPUT CURRENT TO TRIGGER VS. ANODE TO CATHODE VOLTAGE

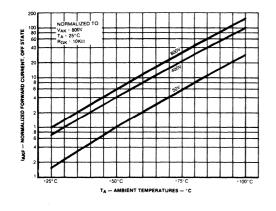
2. INPUT CURRENT TO TRIGGER VS. TEMPERATURE

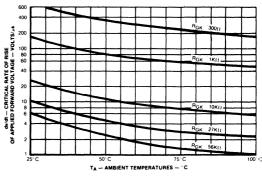




3. INPUT VOLTAGE VS. INPUT CURRENT

4. HOLDING CURRENT VS. TEMPERATURE

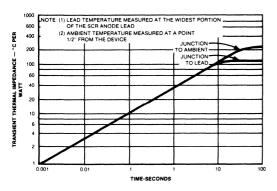


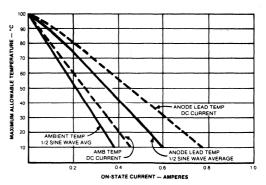


5. OFF-STATE LEAKAGE VS. TEMPERATURE

6. dv/dt VS. TEMPERATURE

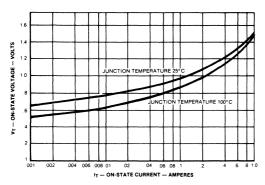
276 \_

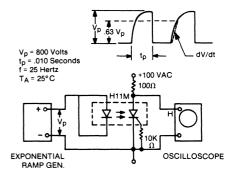




#### 7. MAXIMUM TRANSIENT THERMAL IMPEDANCE

8. ON-STATE CURRENT VS. MAXIMUM ALLOWABLE TEMPERATURE





9. ON-STATE CHARACTERISTICS

10. ISOLATION dv/dt IMMUNITY TEST CIRCUIT

12

# H11M3, H11M4

# **Optoisolator**

# **GaAlAs Infrared Emitting Diode and Light Activated SCR**

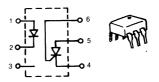
The H11M3 and H11M4 contain a gallium-aluminum-arsenide, infrared emitting diode coupled to a unique high voltage silicon controlled rectifier within a dual in-line package. These devices are optimized for high performance and long life. They are especially suited for the control of industrial AC power lines from low voltage logic integrated circuitry. These devices are also avaiable in surface-mount packaging.

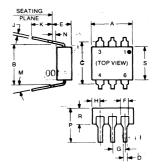
#### **FEATURES**

- High blocking voltage, 600 V minimum
- High isolation voltage, 3750 Vrms minimum (steady state)
- High efficiency, low degradation, liquid epitaxial IRED
- Logic compatible drive current, 7 mA at 1.5 V maximum
- Unique, high performance glass dielectric construction

# absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE								
Power Dissipation	*100	milliWatts						
Forward Current (Continuous)	60	milliAmpere						
Forward Current (Peak) (Pulse width 10 µsec								
Duty Cycle 1%)	1	Ampere						
Reverse Voltage	6	volts						
*Derate 1.33mW/°C above 25°C ambient.								





	MILLIN	IETERS	INC	HES	1		
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES		
Α.	8.38	8.89	.330	.350			
В	7.62	REF.	.300	REF.	1		
C		8.64		.340	2		
- D	.406	.508	0.16	.020	1		
E.		5.08	f .	.200	3		
F	1.01	1.78	.040	.070	1		
G ]	2.28	2.80	.090	.110	1		
н		2.16		.085	- 4		
3 1	.203	.305	.008	.012	1		
K I	2.54		.100		1		
м		15°		15°	1		
N	.381		.015	-	1		
P		9.53		.375	i		
R	2.92	3.43	.115	.135			
s l	6.10	6.86	.240	.270	1		

**TOTAL DEVICE** 

- IOLES
  INSTALLED POSITION LEAD CENTERS.
  OVERALL INSTALLED DIMENSION.
  THESE MEASUREMENTS ARE MADE FROM THE SEATING

PHOTO-SC	R	
Peak Forward Voltage	600	Volts
RMS Forward Current	300	milliAmperes
Peak On-State Current (1 cycle surge, 10 msec)	3	Amperes
Peak Reverse Gate Voltage	5	Volts
Power Dissipation (25° C Ambient) **Derate 5.3 mW/° C above 25° C ambient	**400	milliWatts

Storage Temperature -55°C to +150°C
Operating Temperature –55 to +100° C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output)
$5656 V_{(peak)}$ 4000 $V_{(RMS)}$

Steady-State Isolation Voltage (Input to Output). 5300 V<sub>(peak)</sub> 3750 V(PMS)

A Covered under U.L. component recognition program, reference file E51868

# H11M3, H11M4

# individual electrical characteristics (25°C) (unless otherwise indicated)

EMITTER	SYMBOL	TYP.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> = 10 mA)	$V_{\rm F}$	1.3	1.65	V
Reverse Current (V <sub>R</sub> = 5V)	I <sub>R</sub>	_	10	μΑ
Capacitance $(V_{AK} = 0V, F = 1 MHz)$	C <sub>J</sub>	50		pF

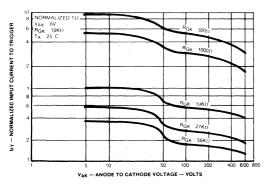
DETECTOR	SYMBOL	MIN.	TYP.	MAX.	UNITS
Off-State Voltage $(R_{GK} = 10K\Omega, I_D = 100\mu A, T_A = 100^{\circ}C)$	V <sub>DM</sub>	600			V
Reverse Voltage $(R_{GK} = 10K\Omega, I_R = 100\mu A, T_A = 100^{\circ}C)$	V <sub>RM</sub>	600		-	V
On-State Voltage $(I_{TM} = 300 \text{mA})$	V <sub>TM</sub>	_		1.6	V
Off-State Current $(R_{GK} = 10K\Omega, V_{DM} = 600V, T_A = 100^{\circ}C)$ $(T_A = 25^{\circ}C)$	$I_{DM}$			100 400	μA nA
Reverse Current $(R_{GK} = 10K\Omega, V_{RM} = 600V, T_A = 100^{\circ}C)$ $(T_A = 25^{\circ}C)$	I <sub>RM</sub>			100 400	μA nA
Critical Rate-of-Rise of Off-State Voltage $(V_{AK} = 600V, R_{GK} = 10K\Omega)$	dv/dt		25		V/µsec
Holding Current $(R_{GK} = 10K\Omega)$	I <sub>H</sub>			2	mA

# coupled electrical characteristics (25°C)

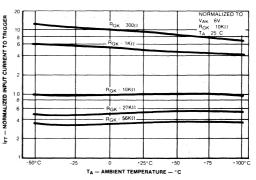
COUPLED		SYMBOL	MIN.	TYP.	MAX.	UNITS
Input Current to Trigger $(V_{AK} = 6V, R_{GK} = 10K\Omega)$	H11M3 H11M4	I <sub>FT</sub>			10 20	mA mA
Input Current to Trigger $(V_{AK} = 6V, R_{GK} = 27K\Omega)$	H11M3 H11M4	I <sub>FT</sub>			7 15	mA mA
Isolation Resistance (Input to Output) (V <sub>10</sub> = 500V)		r <sub>io</sub>	100			GΩ
Isolation Capacitance (Input to Output) (V <sub>IO</sub> = 0V, F = 1 MHz)		C <sub>io</sub>			2	pF
Isolation dv/dt Immunity (Input to Output) See Figure 10			500			V/µsec

Tests of input to output isolation voltage, isolation resistance, and isolation capacitance are performed with the input terminals (pins 1, 2 & 3) shorted together and the output terminals (pins 4, 5 & 6) shorted together.

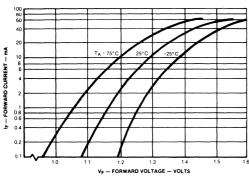
# H11M3, H11M4



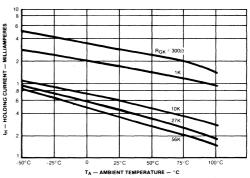
1. INPUT CURRENT TO TRIGGER VS. ANODE TO CATHODE VOLTAGE



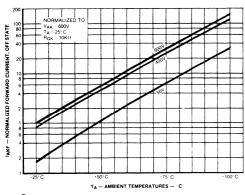
2. INPUT CURRENT TO TRIGGER VS. TEMPERATURE



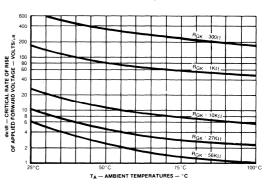
3. INPUT VOLTAGE VS. INPUT CURRENT



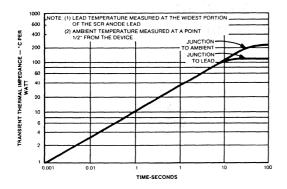
4. HOLDING CURRENT VS. TEMPERATURE

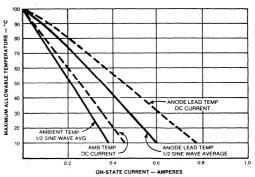


5. OFF-STATE LEAKAGE VS. TEMPERATURE

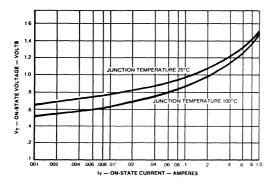


6. dv/dt VS. TEMPERATURE



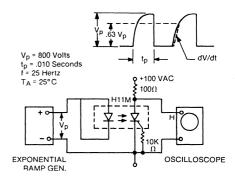


#### 7. MAXIMUM TRANSIENT THERMAL IMPEDANCE



9. ON-STATE CHARACTERISTICS

# 8. ON-STATE CURRENT VS. MAXIMUM ALLOWABLE TEMPERATURE



10. ISOLATION dv/dt IMMUNITY TEST CIRCUIT

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#### H11N1, H11N2, H11N3

# **Optoisolator**

# GaAlAs Infrared Emitting Diode and Microprocessor-Compatible High-Speed Schmitt Trigger

The H11N series has a gallium-aluminum-arsenide, infrared emitting diode optically coupled across a glass isolating medium-to-high speed integrated circuit detector. The output incorporates a Schmitt trigger, which provides hysteresis for noise immunity and pulse shaping. The detector circuit is optimized for simplicity of operation and utilizes an open collector output for maximum application flexibility. These deivces are mounted in dual in-line packages. These devices are also available in surface-mount packaging.

#### Features:

- High data rate, 5 MHz typical (NRZ)
- Free from latch up and oscillation throughout voltage and temperature ranges
- Microprocessor compatible drive
- Logic compatible output sinks 16 mA at 0.5 V maximum
- High isolation between input and output
- Guaranteed on/off threshold hysteresis
- High common mode transient immunity 2000V/µs minimum
- Fast switching: t<sub>r</sub>,t<sub>t</sub> = 10 ns typical
- Wide supply voltage capability, compatible with all popular logic systems





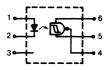
Surface Mount Version

#### **MECHANICAL SPECIFICATIONS**

- Plastic 6 PIN dual-in-line package
- · Lead orientation as shown:

#### **APPLICATIONS**

- Logic to logic isolator
- · Programmable current level sensor
- Line receiver eliminates noise and transient problems
- Logic level shifter couples TTL to CMOS
- A.C. to TTL conversion square wave shaping
- Isolated power MOS driver for power supplies
- · Interfaces computers with peripherals



Schematic diagram for H11N1, H11N2, and H11N3.

#### MAXIMUM RATINGS, Absolute-Maximum Values (TA=25°C):

INFRARED EMITTING DIODE							
Power Dissipation	*50	milliwatts					
Forward Current (Continuous)	30	milliampere					
Forward Current (Peak) (Pulse width 300 µsec							
2% Duty Cycle)	50	milliampere					
Reverse Voltage	6	volts					
*Derate 1.67 mW°C above 70°C ambient.							

PHOTO DETECTOR							
Power Dissipation	**150	milliwatts					
V <sub>45</sub> Allowed Range	0 to 16	volts					
V <sub>65</sub> Allowed Range	0 to 16	volts					
I4 Output Current	50	milliampere					
**Derate 5.0 mW/°C above 25°C ambient.							

тот	AL DEVICE	
Storage Temperature -	55°C to +125°C	
Operating Temperature	-25 to +85°C	
Lead Soldering Time (a	t 260°C) 10 seco	onds
Surge Isolation Voltage	(Input to Outp	ut)
H11N1, H11N2	5656 V <sub>(peak)</sub>	4000 V <sub>(RMS)</sub>
H11N3	3535 V <sub>(peak)</sub>	2500 V <sub>(RMS)</sub>
Steady-State Isolation V	Voltage (Input to	Output).
HIINI, HIIN2	5300 V <sub>(peak)</sub>	3750 V <sub>(RMS)</sub>
H11N3	3180 V <sub>(peak)</sub>	2250 V <sub>(RMS)</sub>

(ove) VDE approved to 0883/6.80 0110b

Covered under U.L. component recognition program, reference file E51868

# H11N1, H11N2, H11N3

#### ELECTRICAL CHARACTERISTICS: (TA = 0-70°C) See Note 1

INFRARED EMITTING DIODE	MIN.	TYP.	MAX.	UNITS	PHOTO DETECTOR	MIN.	TYP.	MAX.	UNITS
Forward Voltage VF				1	Operating Voltage Range V <sub>CC</sub>	4		15	volts
$I_F = 10 \text{ mA}$ $I_F = 0.3 \text{ mA}$	0.75	1.6 1.45	2.0	volts volts	Supply Current $I_{6(off)}$ ( $I_F = 0, V_{CC} = 5V$ )		5.5	10	milli- ampere
Reverse Current $T_A=25^{\circ}C$ $I_R$ ( $V_R = 5V$ ) $T_A=100^{\circ}C$	_	-	10 100	micro- ampere	Output Current, High $I_{OH}$ ( $I_E = 0.3 \text{ mA}, V_{CC} = V_O = 15V$ )	_	_	100	micro- ampere
Capacitance $C_J$ (V = 0, f = 1 MHz)			100	picofarads					

#### COUPLED ELECTRICAL CHARACTERISTICS (TA = 0-70°C) See Note 1

		MIN.	TYP.	MAX.	UNITS
Supply Current $(I_F = 10 \text{ mA}, V_{CC} = 5\text{V})$	I <sub>6(on)</sub>		5	10	milliampere
Output Voltage, Low $(R_L = 270 \Omega, V_{CC} = 5V, I_F = I_{F(on)} max.$	V <sub>oi</sub>	_	0.3	0.5	volts
Turn-On Threshold Current $(R_L = 270 \Omega, V_{CC} = 5V)$	I <sub>F(on)</sub> H11N1 H11N2 H11N3	0.8 2.3 4.1	_	3.2 5.0 10.0	milliampere milliampere milliampere
Turn-Off Threshold Current $(R_L = 270 \Omega, V_{CC} = 5V)$	$I_{Ftoff)}$	0.3	1.5		milliampere
Hysteresis Ratio $R_L = 270 \Omega$ , $V_{CC} = 5V$ )	$I_{ m F(off)}/I_{ m F(on)}$	0.65	0.8	0.95	-

#### DYNAMIC CHARACTERISTICS: (0-70°C) See Note 1

SWITCHING SPEED (See Figures 7 & 8)		MIN.	TYP.	MAX.	UNITS
$C = 120 \text{pF}$ , tp = $1\mu \text{sec}$ , $R_{\text{E}}$ : See Note 4					
Propagation delay, high to low	t <sub>PHI</sub> .		150	330	nsec.
Rise Time	t <sub>r</sub>		10		nsec.
Propagation delay, low to high	tel H	-	150	330	nsec.
Fall Time	tr	'	15		nsec.
Date Rate (NRZ) See Note 3	_		5	_	MHz
OVERDRIVE SWITCHING (See Figures 7 & 8) See	e Note 2				
$C = 0, R_1 = 270 \Omega$					
I <sub>F</sub> (Max.) H11N1: 5mA H11N2: 10mA H11N3: 20mA					11 (1) (1) (1) (1) (1) (1) (1) (1) (1) (
Turn-Off Time	t <sub>oti</sub>	-	0.2	0.5	μsec.
TRANSIENT IMMUNITY (See Figure 9)					
Common Mode Transient Immunity (TA = 25°C)					
$V_{\rm pk} = 50 \text{V}, V_{\rm CC} = 5 \text{V}, R_{\rm L} = 270 \Omega$			1		
$I_{\rm F} = 0$	$CM_u$	±2000	±10000		V/μsec
$I_F = I_F = I_{F(on)} \text{ max. x } 2.35$	$Cm_1$	±2000	±10000		V/μsec

#### NOTES:

- 1. All measurements are with 100nF bypass capacitor from pin 6 to pin 5.
- Steady overdrive increases t<sub>off</sub>. Use of a large RE and a small C as in Figure 7 is preferred over overdrive current.
- 3. Maximum data rate will vary depending on the bias conditions and is usually highest when RE and C are matched to IF(ON) and VCC is between 5 and 15V. With this optimized bias, most units will operate at over 10MHz, NRZ.
- 4. H11N1:  $R_E = 910\Omega$ ; H11N2:  $R_E = 560\Omega$ ; H11N3:  $R_E = 240\Omega$

# H11N1, H11N2, H11N3

#### TYPICAL CHARACTERISTICS

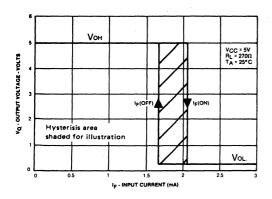


Fig. 1 - Transfer characteristics.

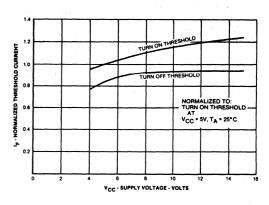


Fig. 2 - Threshold current vs. supply voltage.

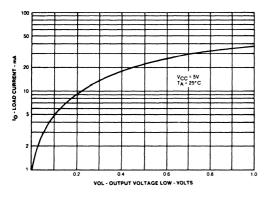


Fig. 3 - ON voltage vs. current.

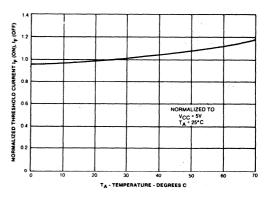


Fig. 4 - Threshold current vs. temperature.

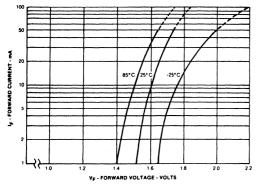


Fig. 5 - Forward voltage vs. forward current.

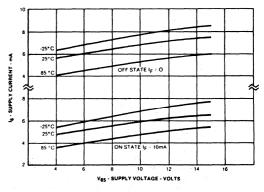
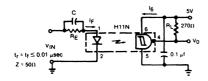


Fig. 6 - Supply current vs. supply voltage.

# 12

# H11N1, H11N2, H11N3



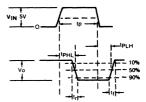
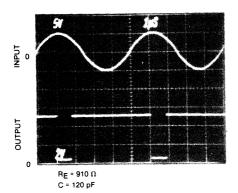


Fig. 7 - Switching test circuit.



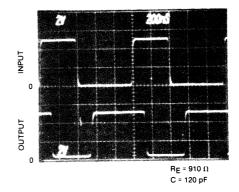
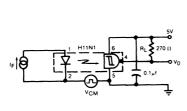


Fig. 8 - Switching test waveforms.



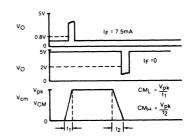
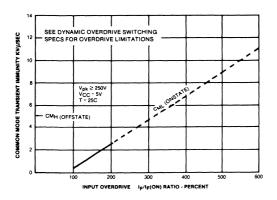
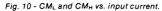


Fig. 9 - Common-mode transient immunity, test circuit and voltage waveforms.





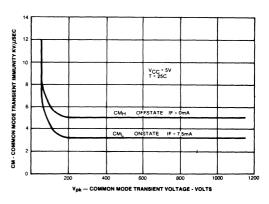


Fig. 11 -  $CM_L$  and  $CM_H$  vs. common-mode transient voltage.

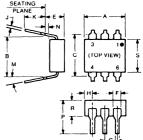
# H11V1, H11V2, H11V3

# **Optoisolator**

# **GaAlAs Infrared Emitting Diode and** Silicon Integrated Circuit Video Signal Amplifier

The H11V series consists of a high-speed gallium-aluminumarsenide, infrared emitting diode coupled across a glass isolating medium to a photosensitive high-frequency linear integrated circuit amplifier. The input and output are matched to optimize video linearity at minimum quiescent power. These devices are mounted in dual in-line packages. These devices are also available in surface-mount packaging.





#### **FEATURES**

- High gain, typical transimpedence, 1000Ω
- Low input current requirement, typical 3.5mA at 1.6V
- 0 to 10MHz operating bandwidth
- 100mA peak output drive capability

#### ABSOLUTE MAXIMUM RATINGS (25°C)

Infrared Emitting Diode	
Power Dissipation	50mW*
Forward Current	30mA
Reverse Voltage	6V
*Derate 1.67mW/°C above 70	0°C ambient

Integrated Circuit Dete	ector
Power Dissipation	150mW**
V <sub>65</sub> allowed range	0 to 16V
V <sub>45</sub> allowed range	0 to 16V
Output Current	50mA
**Derate 5.0mW per °C	above 70°C

Storage remperature.
-40°C to +100°C
Operating Temperature:
−25°C to +80°C
Lead Solder Temperature:
(≤10sec) 260°C
Surge Isolation Voltage:
4000 VRMS
Steady State Isolation Voltage:

3750 VRMS

**Total Device** Storage Temperature:

MILLIN	MILLIMETERS INCHES		INCHES	
MIN.	MAX.	MIN.	MAX.	NOTES
8.38	8.89	.330	.350	
7.62	REF.	.300	REF.	1 1
	8.64	1	.340	2
.406	.508	0.16	.020	1
	5.08		.200	. 3
1.01	1.78	.040	.070	1
2.28	2.80	.090	.110	1
	2.16	1	.085	4
.203	.305	.008	.012	1
2.54		.100		
	15°	1	15°	
381		.015		1
	9.53		375	1
2.92	3.43	.115	.135	1
6.10	6.86	.240	.270	1
	MIN.  8.38 7.62 .406 1.01 2.28 .203 2.54 .381	MIN. MAX.  8.38 8.89 7.62 REF. 8.64 .406 5.08 1.01 1.78 2.28 2.80 2.03 .305 2.54 15 .381 15 2.92 3.43	MIN. MAX. MIN.  8.38 8.89 .330 7.62 REF. 3.00  4.06 5.08 0.16 1.01 1.03 0.40 2.28 2.80 0.90 2.16 0.90 2.54 15° .000 2.54 15° .015 3.81 9.53 2.92 9.53 3.43 1.115	MIN.   MAX.   MIN.   MAX.   8.38   8.89   .330   .350   .350   .360   REF.   .300   REF.   .300   REF.   .300   REF.   .300

- IOTES
  INSTALLED POSITION LEAD CENTERS.
  OVERALL INSTALLED DIMENSION.
  THESE MEASUREMENTS ARE MADE FROM THE SEATING
- PLANE. 4. FOUR PLACES.

#### INDIVIDUAL ELECTRICAL CHARACTERISTICS (25°C)

Infrared Emitting Di	ode	Min.	Тур.	Max.	Units
Forward voltage	$(I_F = 5mA)$	1.2	1.5	2.0	V
Dynamic Resistance	$(I_F = 5mA)$		10		Ω
Reverse Current	$(V_R = 5V)$			10	μΑ
Capacitance	$(V_R = 0V, 1MHz)$		60	******	pF

Infrared Circuit Detector	Min.	Тур.	Max.	Units
Operating Voltage Range	5	10	15	V
Supply Current ( $V_{CC} = 10V$ , $R_L = \infty$ , $I_F = 0$ )	-	6.0		mA
Output Voltage ( $V_{CC} = 10V$ , $R_L = 390\Omega$ , $I_F = 0$ )	0.25	0.75	1.50	V

BIAS CIRCUIT
SUPPLY VCC
1 6 01 =
V <sub>out</sub>
H11V 3 RL
-

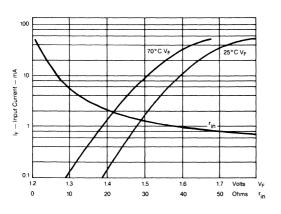
COUPLED ELECTRICAL CHARACTERISTICS (25°C) (V <sub>CC</sub> = 10V, R <sub>L</sub> = 3900	), Bias Ckt.)	Min.	Тур.	Max.	Units
D.C. Output Voltage (I <sub>F</sub> = 3.5 mA)		2.0	4.0	7.0	V
A.C. Output Voltage ( $I_F = 3.5 \text{ mA}$ , $I_F = 1 \text{ mA pk-pk}$ , 1KHz)	HIIVI	0.50	0.90	1.25	Vpk-pk
	H11V2	0.75	1.00		Vpk-pk
	H11V3	0.33	0.80	********	Vpk-pk
Dynamic Output Impedence (I <sub>F</sub> = 3.5 mA, i <sub>F</sub> = 1mA pk-pk, 1KHz)			15	_	Ω
Supply Current (I <sub>F</sub> = 10 mA)			30	*****	mA
6db Down High Frequency (I <sub>F</sub> = 3.5 mA, i <sub>F</sub> = 1mA pk-pk)			10		MHz
Short Circuit Output Current (I <sub>F</sub> = 10 mA)			100		mA
Isolation Capacitance (V <sub>IO</sub> = 0, f = 1MHz)		_	0.8	2.0	pF
Isolation Resistance (V <sub>IO</sub> = 500V)		100	_		GΩ

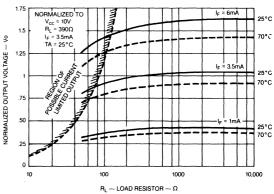
Na Covered under U.L. Component Recognition Program File E51868

⟨o<sup>V</sup>E⟩ VDE approved to 0883/6.80 0110b

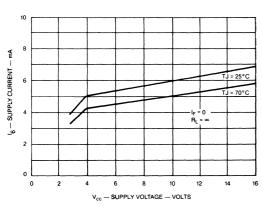
# 12

#### TYPICAL CHARACTERISTICS

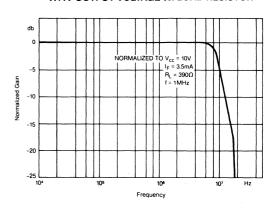




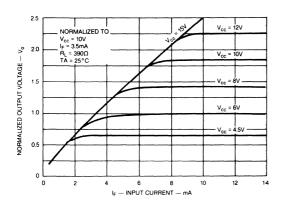
#### **H11V INPUT CHARACTERISTICS**



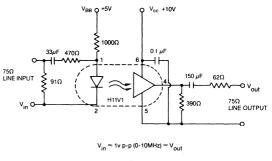
H11V OUTPUT VOLTAGE vs. LOAD RESISTOR



#### H11V SUPPLY CURRENT vs. SUPPLY VOLTAGE



H11V GAIN ROLLOFF



**H11V TRANSFER CHARACTERISTICS** 

#### TYPICAL VIDEO COMPOSITE COUPLING CIRCUIT

#### MOC3009-MOC3012

### **Optoisolator GaAs Infrared Emitting Diode and Light Activated Triac Driver**

The MOC3009-MOC3012 series consists of a gallium arsenide, infrared emitting diode coupled with a light activated silicon bilateral switch, which functions like a triac, in a dual in-line package.

These devices are especially designed for triggering power triacs while maintaining dielectric isolation from the trigger control circuit. They are mounted in dual in-line packages. These devices are also available in surface-mount packaging.

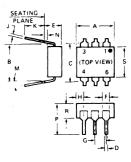
### absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE				
Power Dissipation	*100	milliwatts		
Forward Current (Continuous)	50	milliamps		
Forward Current (Peak) (Pulse width 1 µsec. 300 pps)	3	amperes		
Reverse Voltage	3	volts		
*Derate 1.33mW/°C above 25°C ambient.				

OUTPUT DRIVER					
Off-State Output Terminal Voltage	250	Volts			
On-State RMS Current (Full Cycle Sine Wave, 50 to 60 Hz)	100	milliamps			
Peak Nonrepetitive Surge Current (PW = 10 ms, DC = 10%)	1.2	amperes			
Total Power Dissipation @ T <sub>A</sub> = 25°C	**300	milliwatts			
**Derate 4.0 mW/°C above 25°C ambient.					

#### **TOTAL DEVICE** Storage Temperature -55°C to +150°C Operating Temperature -40°C to +100°C Lead Soldering Time (at 260°C) 10 seconds Isolation Surge Voltage: (Input to Output) 7500VAC (Peak AC Voltage, 60 Hz, 5 second duration)

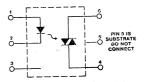




	MILLIN	ETERS	INC	HES	1
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α .	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
C	1	8.64		.340	2
D I	.406	.508	0.16	.020	1
E		5.08		.200	3
E F	1.01	1.78	.040	.070	1
G	2.28	2.80	.090	.110	1
Ĥ		2.16		.085	4
j	.203	.305	.008	.012	1
ĸ l	2.54		.100	Į.	1
м		15°	1.	15°	1
N	.381		.015	1	1
Р		9.53	1	.375	1
R	2.92	3.43	.115	.135	1
s	6.10	6.86	.240	.270	

- NOTES

  1. INSTALLED POSITION LEAD CENTERS.
  2. OVERALL INSTALLED DIMENSION.
  3. THESE MEASUREMENTS ARE MADE FROM THE SEATING
- 4. FOUR PLACES.



Na Covered under U.L. component recognition program, reference file E51868

### individual electrical characteristics (25°C)

EMITTER	SYMBOL	TYP.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> = 10 mA)	$V_{\rm F}$	1.2	1.5	volts
Reverse Current (V <sub>R</sub> = 3V)	I <sub>R</sub>		100	microamps
Capacitance (V = O, f = 1 MHz)	C <sub>J</sub>	50	_	picofarads

DETECTOR See Note 1		SYMBOL	TYP.	MAX.	UNITS
Peak Off-State Current	V <sub>DRM</sub> 250 V	I <sub>DRM</sub>		100	nanoamps
Peak On-State Voltage	$I_{TM} = 100 \text{ mA}$	V <sub>TM</sub>	2.5	3.0	volts
Critical Rate-of-Rise of Off-State Voltage	$T_A = 85^{\circ}C$	dv/dt	12.0		volts/µsec.

### coupled electrical characteristics (25°C)

		SYMBOL	TYP.	MAX.	UNITS
IRED Trigger Current, Current Required to Latch Output	MOC3009	I <sub>FT</sub>		30	milliamps
(Main Terminal Voltage = 3.0 V, $R_L = 150 \Omega$	MOC3010	I <sub>FT</sub>		15	milliamps
	MOC3011	$I_{FT}$		10	milliamps
	MOC3012	I <sub>FT</sub>		5	milliamps
Holding Current, Either Direction		I <sub>H</sub>	100	- Anna Marie	microamps

NOTE 1: Ratings apply to either polarity of Pin 6 — referenced to Pin 4. Voltages must be applied within dv/dt rating.

#### MOC3020-MOC3023

## **Optoisolator GaAs Infrared Emitting Diode and Light Activated Triac Driver**

The MOC3020-MOC3023 series consists of a gallium arsenide, infrared emitting diode coupled with a light activated silicon bilateral switch, which functions like a triac, in a dual in-line package.

These devices are especially designed for triggering power triacs while maintaining dielectric isolation from the trigger control circuit. They are mounted in dual in-line packages. These devices are also available in surface-mount packaging.

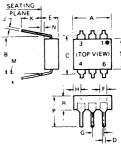
### absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE						
Power Dissipation	*100	milliwatts				
Forward Current (Continuous)	50	milliamps				
Forward Current (Peak) (Pulse width 1 µsec. 300 pps)	3	amperes				
Reverse Voltage	3	volts				
*Derate 1.33mW/°C above 25°C ambient.						

OUTPUT DRIVER				
Off-State Output Terminal Voltage	400	Volts		
On-State RMS Current (Full Cycle Sine Wave, 50 to 60 Hz)	100	milliamps		
Peak Nonrepetitive Surge Current (PW = 10 ms, DC = 10%)	1.2	amperes		
Total Power Dissipation @ $T_A = 25^{\circ}C$	**300	milliwatts		
**Derate 4.0 mW/°C above 25°C ambient.				

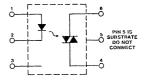
TOTAL DEVICE
Storage Temperature -55°C to +150°C
Operating Temperature –40°C to +100°C
Lead Soldering Time (at 260°C) 10 seconds
Isolation Surge Voltage: (Input to Output) 7500VAC (Peak AC Voltage, 60 Hz, 5 second duration)





- 1	MILLIMETERS		INCHES		]
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Λ .	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1 1
C	1	8,64		.340	2
D	.406	.508	0.16	.020	1
E		5.08		.200	3
F	1.01	1.78	.040	.070	Į.
G	2.28	2.80	.090	.110	1
н		2.16	1	.085	4
J I	.203	.305	008	.012	1
к	2.54		.100		ŀ
M	1	15°		150	1
N I	.381		.015		I
P	- 1	9.53		.375	1
R	2.92	3.43	.115	.135	i
s	6.10	6,86	.240	.270	1

- IOTES
  INSTALLED POSITION LEAD CENTERS.
  OVERALL INSTALLED DIMENSION.
  THESE MEASUREMENTS ARE MADE FROM THE SEATING
- PLANE. 4. FOUR PLACES.



Na Covered under U.L. component recognition program, reference file E51868

### individual electrical characteristics (25°C)

EMITTER	SYMBOL	TYP.	MAX.	UNITS
Forward Voltage (I <sub>+</sub> = 10 mA)	V <sub>F</sub>	1.2	1.5	volts
Reverse Current (V <sub>R</sub> = 3V)	I <sub>R</sub>	sh.*********	100	microamps
Capacitance (V = O, f = 1 MHz)	C,	50	contractors.	picofarads

DETECTOR See Note 1		SYMBOL	TYP.	MAX.	UNITS
Peak Off-State Current	V <sub>DRM</sub> 400 V	I <sub>DRM</sub>		100	nanoamps
Peak On-State Voltage	$I_{TM} = 100 \text{ mA}$	$\mathbf{V}_{TM}$	2.5	3.0	volts
Critical Rate-of-Rise of Off-State Voltage	$T_{\Lambda} = 85^{\circ}C$	dv/dt	12.0		volts/µsec.

### coupled electrical characteristics (25°C)

		SYMBOL	TYP.	MAX.	UNITS
IRED Trigger Current, Current Required to Latch Output	MOC3020	$I_{FT}$		30	milliamps
(Main Terminal Voltage = 3.0 V, $R_L = 150 \Omega$	MOC3021	$I_{FT}$	_	15	milliamps
	MOC3022	$I_{FT}$		10	milliamps
· ·	MOC3023	I <sub>FT</sub>		5	milliamps
Holding Current, Either Direction		I <sub>H</sub>	100		microamps

NOTE 1: Ratings apply to either polarity of Pin 6 — referenced to Pin 4. Voltages must be applied within dv/dt rating.

### SL5500, SL5501

### **Optoisolator**

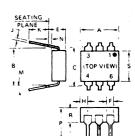
### **GaAs Infrared Emitting Diode and NPN Silicon Phototransistor**

The SL5500-SL5501 consists of a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. They comply with UTE requirements as per UTE C96-551 ADD2. These devices are also available in surface-mount packaging.

#### **FEATURES**

- Included in the CNET LNZ approval list
- Unique patented glass isolation construction
- High efficiency liquid epitaxial IRED
- High humidity resistant silicone encapsulation
- · Fast switching speeds





SEATING

### absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE							
Power Dissipation - $T_A = 25^{\circ} C$	*100	milliwatts					
Forward Current (Continuous)	60	milliamps					
Forward Current (Peak) (Pulse width 1 µsec, 300 pps)	3	amperes					
Reverse Voltage	6	volts					
*Derate 1.33 mW/°C above 25°C ambient.							

PHOTO-TRANSISTOR							
Power Dissipation - $T_A = 25^{\circ}C$	**300	milliwatts					
V <sub>CEO</sub>	30	volts					
V <sub>CBO</sub>	70	volts					
V <sub>EBO</sub>	7	volts					
Collector Current (Continuous)	100	millamps					
**Derate 4.0 mW/°C above 25°C							

**300	milliwatts
30	volts
70	volts
7	volts
100	millamps
	30 70 7

l G	2.28	2.80	.090	.110
н		2.16	ı	.085
J	.203	.305	.008	.012
l ĸ	2.54		.100	
М		15°		15°
N	.381		.015	
P		9.53		.375
R	2.92	3.43	.115	.135
S	6.10	6.86	.240	.270
NOTES				
INSTALL	ED POSITI	ON LEAD C	ENTERS.	
OVERAL	INSTALL	ED DIMENS	ION.	
		ENTS ARE		M THE
PLANE				
FOUR PL	ACES.			

MILLIMETERS

8.38 7.62 REI

#### **TOTAL DEVICE**

Storage Temperature -55°C to +150°C

Operating Temperature -55 to 100°C

Lead Soldering Time (at 260°C) 10 seconds

Nominal Voltage 500 V (DC)

Steady-State Isolation Voltage (Input to Output). 3500 V<sub>(DC)</sub> 2500 V<sub>(RMS)</sub>

Covered under U.L. component recognition program, reference file E51868

### SL5500, SL5501

### individual electrical characteristics (25°C) (unless otherwise indicated)

INFRARED EMITTER DIODE	MIN.	MAX.	UNITS
Forward Voltage - $V_F$ ( $I_F = 20 \text{ mA}$ )	_	1.3	volts
Forward Voltage - $V_F$ ( $I_F = 2 \text{ mA}$ )		1.2	volts
Reverse Current - $I_R$ ( $V_R = 3V$ )	_	10	microamps
Capacitance - C <sub>J</sub> (V = O, f = 1 MHz)	_	100	picofarads

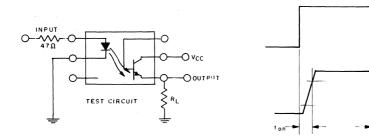
PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - V <sub>(BR)CEO</sub> (I <sub>C</sub> = 10 mA, I <sub>F</sub> = O)	30		ARRESTS.	volts
Breakdown Voltage - $V_{(BR)CBO}$ ( $I_C = 10 \mu A, I_F = O$ )	70		_	volts
Breakdown Voltage - $V_{(BR)EBO}$ ( $I_F = 10 \mu A, I_F = O$ )	7		_	volts
Collector Dark Current - $I_{CEO}$ ( $V_{CE} = 10 \text{ V}, I_F = O$ )		5	50	nano- amps
Collector Dark Current - $I_{CEO}$ ( $V_{CE} = 10 \text{ V}, I_{F} = O$ ) $T_{A} = 70^{\circ}\text{C}$	_		500	micro- amps
$h_{FE}$ ( $I_C = 4 \text{ mA}, V_{CE} = 0.4, I_F = O$ )	200		1200	

### coupled electrical characteristics (25°C) (unless otherwise specified)

		MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_F = 10 \text{ mA}$ , $V_{CE} = 0.4 \text{ V}$ )	SL5500 SL5501	40 25	-	300 400	%
DC Current Transfer Ratio ( $I_F = 2mA$ , $V_{CF} = 5 \text{ V}$	SL5500	30			%
Saturation Voltage - Collector to Emitter ( $I_F = 50 \text{ mA}$ , $I_C = 10 \text{ mA}$ )	SL5501 SL5500	25		0.4	% volts
Saturation Voltage - Collector to Emitter ( $I_F = 20 \text{ mA}$ , $I_C = 2 \text{ mA}$	SL5501 SL5500	_		0.4	volts volts
Isolation Resistance (Input to Output Voltage = (1 K V <sub>DC</sub> See Note 1)	SL5501	10		0.4	volts gigaohms
Input to Output Capacitance (Input to Output Voltage = (1 K V <sub>DC</sub> Sec Note 1)		_		1.3	picofarads
Turn-On Time — $t_{on}$ ( $V_{CC}$ = 5 V, $I_F$ = 16 mA, $R_L$ = 1 K $\Omega$ ). (See Figure 1)			5	20	microseconds
Turn-Off Time — $t_{off}$ ( $V_{CC}$ = 5 V, $I_F$ = 16 mA, $R_L$ = 1 K $\Omega$ ). (See Figure 1)			5	50	microseconds

NOTE 1:

Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together.



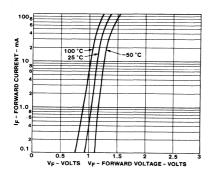
#### **TEST CIRCUIT AND VOLTAGE WAVEFORMS**

INPUT PULSE

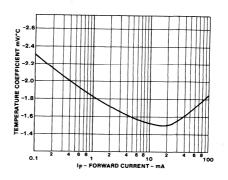
> 90 % OUTPUT

### SL5500-SL5501

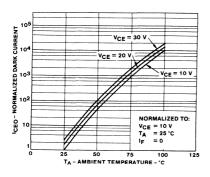
#### TYPICAL CHARACTERISTICS



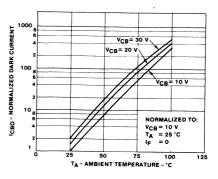
1. INPUT CHARACTERISTICS



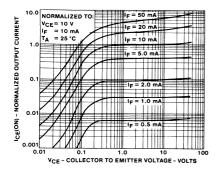
2. FORWARD VOLTAGE TEMPERATURE COEFFICIENT



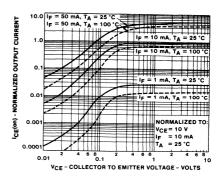
3. DARK I<sub>CEO</sub> CURRENT VS TEMPERATURE



4. I<sub>CBO</sub> VS. TEMPERATURE



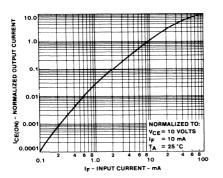
5. OUTPUT CHARACTERISTICS



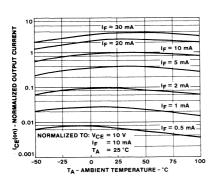
6. OUTPUT CHARACTERISTICS

# 12

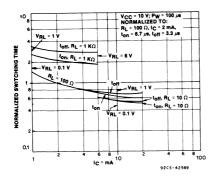
#### TYPICAL CHARACTERISTICS



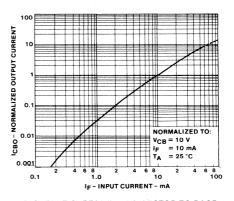
7. OUTPUT CURRENT VS. INPUT CURRENT



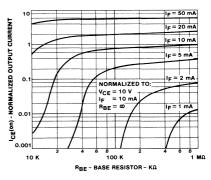
9. OUTPUT CURRENT VS TEMPERATURE



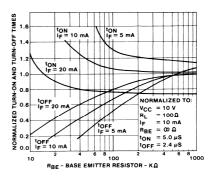
11. SWITCHING SPEED VS. COLLECTOR CURRENT (NOT SATURATED)



8. OUTPUT CURRENT — COLLECTOR TO BASE VS. INPUT CURRENT



10. OUTPUT CURRENT VS. BASE EMITTER RESISTANCE



12. SWITCHING TIME VS RBE

#### **SL5504**

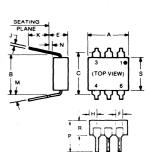
### **Optoisolator GaAs Infrared Emitting Diode and NPN Silicon Phototransistor**

The SL5504 consists of a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. The SL5504 complies with UTE requirements as per UTE C96-551 ADD2. This device is also available in surface-mount packaging.

#### **FEATURES**

- Included in the CNET LNZ approval list
- · Unique patented glass isolation construction
- High efficiency liquid epitaxial IRED
- High humidity resistant silicone encapsulation
- Fast switching speeds





### absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE						
Power Dissipation - $T_A = 25^{\circ}C$	*100	milliwatts				
Forward Current (Continuous)	60	milliamps				
Forward Current (Peak) (Pulse width 1 µsec, 300 pps)	3	amperes				
Reverse Voltage	6	volts				
*Derate 1.33 mW/°C above 25°C ambient.						

PHOTO-TRANSISTOR							
Power Dissipation - $T_A = 25^{\circ}C$	**300	milliwatts					
V <sub>CFO</sub>	80	volts					
V <sub>CBO</sub>	120	volts					
V <sub>EBO</sub>	7	volts					
Collector Current (Continuous)	100	milliamps					
**Derate 4.0 mW/°C above 25°C							

1 1	MILLIMETERS		INCHES		j
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Λ	8.38	8.89	.330	.350	
В	7.62	REF.		REF.	1 1
C		8.64	l	.340	2
D	.406	.508	0.16	.020	1
E F		5.08	ı	.200	3
	1.01	1.78	.040	.070	1
G	2.28	2.80	.090	.110	l
H		2.16		.085	4
1 1	.203	.305	.008	.012 -	l
K	2.54		.100		l
- M		15°	1	15°	1
l N	.381		.015	l	I
P 1		9.53	1	.375	ì
R	2.92	3.43	.115	.135	j
S	6.10	6.86	.240	.270	l .
NOTES					

#### **TOTAL DEVICE**

Storage Temperature -55°C to 150°C

Operating Temperature -55 to 100°C

Lead Soldering Time (at 260°C) 10 seconds

Nominal Voltage 500 V (DC)

Steady-State Isolation Voltage (Input to Output).

3500 V<sub>(DC)</sub>

2500 V(RMS)

NOTES

1. INSTALLED POSITION LEAD CENTERS.
2. OVERALL INSTALLED DIMENSION.
3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
4. FOUR PLACES.

Na Covered under U.L. component recognition program, reference file E51868

### individual electrical characteristics (25°C) (unless otherwise indicated)

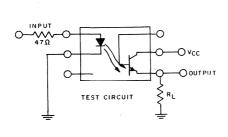
INFRARED EMITTER DIODE	MIN.	MAX.	UNITS
Forward Voltage - V <sub>F</sub> (I <sub>F</sub> = 20 mA)		1.3	volts
Forward Voltage - V <sub>F</sub> (I <sub>F</sub> = 2 mA)	and the second	1.2	volts
Reverse Current - I <sub>R</sub> (V <sub>R</sub> = 3V)		10	microamp
Capacitance - $C_1$ (V = O, f = 1 MHz)		100	picofarads

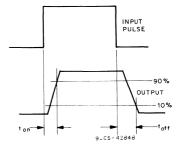
PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - $V_{(BR)CEO}$ ( $I_C = 10 \text{ mA}, I_E = O$ )	80			volts
Breakdown Voltage - $V_{(BR)CBO}$ ( $I_C = 10 \mu A, I_F = O$ )	120			volts
Breakdown Voltage - $V_{(BR)EBO}$ ( $I_F = 10 \mu A, I_F = O$ )	7	-		volts
Collector Dark Current - $I_{CFO}$ ( $V_{CE} = 50 \text{ V}, I_{F} = O$ )		5	50	nano- amps
Collector Dark Current - $I_{CEO}$ ( $V_{CE} = 50 \text{ V}, I_F = O$ )			500	nano- amps
$T_A = 70^{\circ} \text{C}$ $h_{\text{HF}}$ $(I_C = 4 \text{ mA}, V_{\text{CF}} = 0.4, I_F = 0)$	200		1200	

### coupled electrical characteristics (25°C) (unless otherwise specified)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_F = 10 \text{ mA}, V_{CE} = 0.4 \text{ V}$ )	25		400	%
DC Current Transfer Ratio ( $I_F = 2mA$ , $V_{CF} = 5 \text{ V}$	25			%
Saturation Voltage - Collector to Emitter ( $I_F = 20 \text{ mA}$ , $I_C = 2 \text{ mA}$ )			0.4	volts
Isolation Resistance (Input to Output Voltage = 1 K V <sub>DC</sub> See Note 1)	10			gigaohms
Input to Output Capacitance (Input to Output Voltage = O, f = 1 MHz, See Note 1)			1.3	picofarads
Turn-On Time — $t_{on}$ ( $V_{CC}$ = 5 V, $I_F$ = 16 mA, $R_L$ = 1 K $\Omega$ ). (See Figure 1)		5	50	microseconds
Turn-Off Time — $t_{off}$ ( $V_{CC}$ = 5 V, $I_F$ = 16 mA, $R_L$ = 1 K $\Omega$ ). (See Figure 1)		5	150	microseconds

Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together.

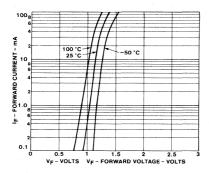




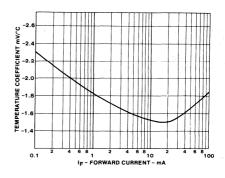
#### **TEST CIRCUIT AND VOLTAGE WAVEFORMS**

#### **SL5504**

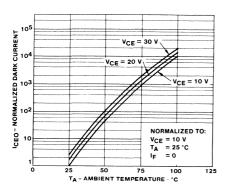
#### **TYPICAL CHARACTERISTICS**



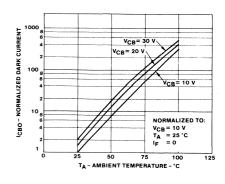
1. INPUT CHARACTERISTICS



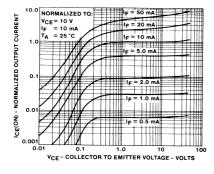
2. FORWARD VOLTAGE TEMPERATURE COEFFICIENT



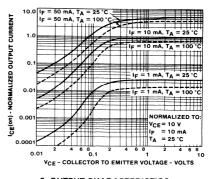
3. DARK ICEO CURRENT VS. TEMPERATURE



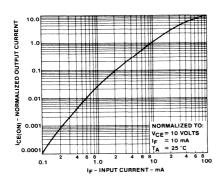
4. I<sub>CBO</sub> VS TEMPERATURE

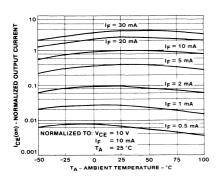


5. OUTPUT CHARACTERISTICS

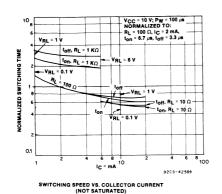


6. OUTPUT CHARACTERISTICS

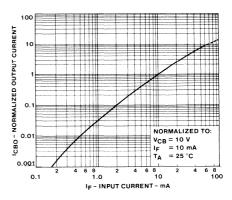




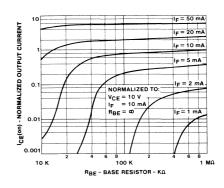
9. OUTPUT CURRENT VS TEMPERATURE



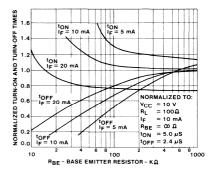
11. SWITCHING SPEED VS. COLLECTOR CURRENT (NOT SATURATED)



8. OUTPUT CURRENT — COLLECTOR TO BASE VS. INPUT CURRENT



10. OUTPUT CURRENT VS. BASE EMITTER RESISTANCE



12. SWITCHING TIME VS RBE

#### **SL5511**

### **Optoisolator**

### GaAs Infrared Emitting Diode and **NPN Silicon Phototransistor**

The SL5511 consists of a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. The SL5511 complies with UTE requirements as per UTE C96-551 ADD2. This device is mounted in a dual in-line package. This device is also available in surface-mount packaging.

#### **FEATURES**

- Included in the CNET LNZ approval list
- Unique patented glass isolation construction
- · High efficiency liquid epitaxial IRED
- High humidity resistant silicone encapsulation
- · Fast switching speeds

absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE								
Power Dissipation - T <sub>A</sub> = 25°C	*100	milliwatts						
Forward Current (Continuous)	60	milliamps						
Forward Current (Peak) (Pulse width 1 µsec, 300 pps)	3	amperes						
Reverse Voltage	6	volts						
*Derate 1.33 mW/°C above 25°C ambient.								

PHOTO-TRANSISTOR							
Power Dissipation - $T_A = 25^{\circ}C$	**300	milliwatts					
V <sub>CEO</sub>	30	volts					
V <sub>CBO</sub>	70	volts					
V <sub>EBO</sub>	7	volts					
Collector Current (Continuous)	100	milliamps					
**Derate 4.0 mW/°C above 25°C							

#### **TOTAL DEVICE**

Storage Temperature -55°C to +150°C

Operating Temperature -55 to 100°C

Lead Soldering Time (at 260°C) 10 seconds

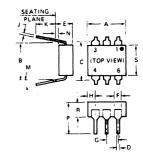
Nominal Voltage 500 V (DC)

Steady-State Isolation Voltage (Input to Output). 3500 V<sub>(DC)</sub> 2500 V<sub>(RMS)</sub>









- 1	MILLIN	ETERS	INC	HES	]
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
A	8.38	8.89	.330	.350	1
в	7.62	7.62 REF.		REF.	1 1
c		8.64		340	2
D	.406	.508	0.16	.020	
E	1	5.08	1	.200	3
F	1.01	1.78	.040	.070	1
G I	2.28	2.80	.090	.110	i
н		2.16		.085	4
Ĵ	.203	.305	.008	.012	1
ĸ.	2.54		.100		1
м		15°		15°	1
N I	.381		.015		1
P		9.53		.375	1
R	2.92	3.43	.115	.135	1
S	6.10	6.86	.240	.270	1

- NOTES

  1. INSTALLED POSITION LEAD CENTERS.

  2. OVERALL INSTALLED DIMENSION.

  3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.

  4. FOUR PLACES.

### individual electrical characteristics (25°C) (unless otherwise indicated)

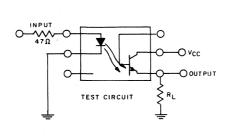
INFRARED EMITTER DIODE	MIN.	MAX.	UNITS
Forward Voltage - V <sub>F</sub> (I <sub>F</sub> = 20 mA)	14 Mariente	1.3	volts
Forward Voltage - $V_F$ ( $I_F = 2 \text{ mA}$ )		1.2	volts
Reverse Current - $I_R$ ( $V_R = 3V$ )		10	microamp
Capacitance - C <sub>1</sub> (V = O, f = 1 MHz)		100	picofarads

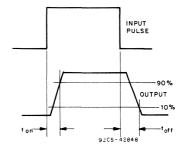
PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - V <sub>(BR)CFO</sub> (I <sub>C</sub> = 10 mA, I <sub>F</sub> = O)	30			volts
Breakdown Voltage - $V_{(BR)CBO}$ ( $I_C = 10 \mu A, I_F = O$ )	70			volts
Breakdown Voltage - $V_{(BR)FBO}$ ( $I_F = 10 \mu A, I_F = O$ )	7		***************************************	volts
Collector Dark Current - $I_{CEO}$ ( $V_{CE} = 10 \text{ V}, I_{E} = O$ )		5	50	nano- amps
Collector Dark Current - $I_{CEO}$ ( $V_{CF} = 10 \text{ V}, I_F = O$ ) $T_A = 70^{\circ}\text{C}$	-		500	micro- amps
$h_{FE}$ ( $I_C = 4 \text{ mA}, V_{CE} = 0.4, I_F = O$ )	200		1200	

### coupled electrical characteristics (25°C) (unless otherwise specified)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio (I <sub>F</sub> = 0.5 mA, V <sub>CE</sub> = 0.4 V)	20	-		%
DC Current Transfer Ratio ( $I_F = 2mA$ , $V_{CF} = 5 \text{ V}$	25			%
Saturation Voltage - Collector to Emitter ( $I_F = 20 \text{ mA}$ , $I_C = 2 \text{ mA}$ )		_	0.4	volts
Isolation Resistance (Input to Output Voltage = 1 K V <sub>DC</sub> See Note 1)	10			gigaohms
Input to Output Capacitance (Input to Output Voltage = O, f = 1 MHz, See Note 1)		_	1.3	picofarads
Turn-On Time — $t_{on}$ ( $V_{CC}$ = 5 V, $I_F$ = 16 mA, $R_L$ = 1 K $\Omega$ ). (See Figure 1)		5	20	microseconds
Turn-Off Time — $t_{off}$ ( $V_{CC}$ = 5 V, $I_F$ = 16 mA, $R_L$ = 1 K $\Omega$ ). (See Figure 1)		5	50	microseconds

NOTE 1: Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together.

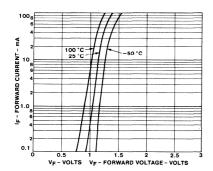




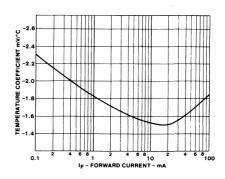
#### TEST CIRCUIT AND VOLTAGE WAVEFORMS

#### SL5511

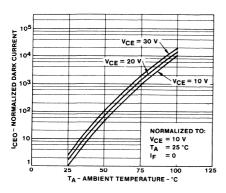
#### TYPICAL CHARACTERISTICS



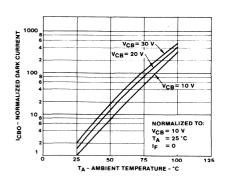
1. INPUT CHARACTERISTICS



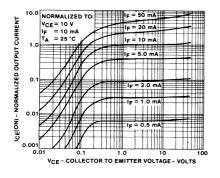
2. FORWARD VOLTAGE TEMPERATURE COEFFICIENT



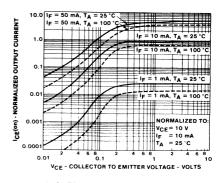
3. DARK I<sub>CEO</sub> CURRENT VS. TEMPERATURE



4. I<sub>CBO</sub> VS TEMPERATURE



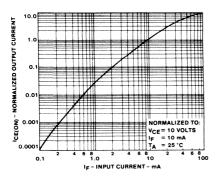
5. OUTPUT CHARACTERISTICS

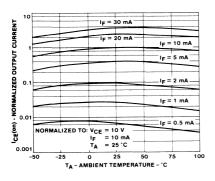


6. OUTPUT CHARACTERISTICS

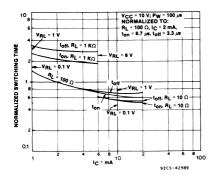
# 12

#### TYPICAL CHARACTERISTICS

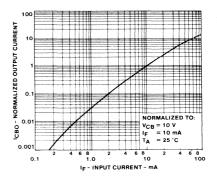




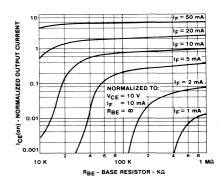
9. OUTPUT CURRENT VS TEMPERATURE



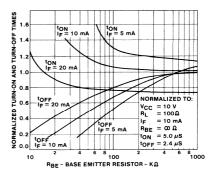
11. SWITCHING SPEED VS COLLECTOR CURRENT (NOT SATURATED)



8. OUTPUT CURRENT — COLLECTOR TO BASE VS INPUT CURRENT



10. OUTPUT CURRENT VS BASE EMITTER RESISTANCE



12. SWITCHING TIME VS RBE

### H21A1, H21A2, H21A3

## **Optointerrupter**

GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

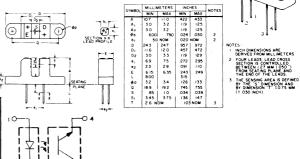
Module with 1mm Aperture

The H21A Interrupter Module is a gallium arsenide infrared emitting diode coupled to a silicon phototransistor in a plastic housing. The packaging system is designed to optimize the mechanical resolution, coupling efficiency, ambient light rejection, cost, and reliability. The gap in the housing provides a means of interrupting the signal with an opaque material, switching the output from an "ON" into an "OFF" state.

### absolute maximum ratings: (25°C)

TOTAL DEVICE		
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	T <sub>STG</sub> T <sub>J</sub> T <sub>L</sub>	-55°C to +100°C -55°C to +100°C 260°C

INFRARED EMITTING DIOD	E		
Power Dissipation	$P_{\rm E}$	*100	mW
Forward Current	$I_{\mathrm{F}}$	60	mA
(Continuous)			
Forward Current (Peak)	$I_{\mathrm{F}}$	3	Α
(Pulse Width $\leq 1 \mu$ s			
$PRR \le 300  pps$ )			
Reverse Voltage	$V_R$	6	V
*Derate 1.33 mW/	°C above 25°	'C ambient.	
L			



PHOTOTRANSISTOR			
Power Dissipation	$P_{\mathrm{D}}$	**150	mW
Collector Current (Continuous)	$I_{\rm C}$	100	m <b>A</b>
Collector-Emitter Voltage	$V_{CEO}$	30	V
Emitter-Collector Voltage	$V_{ECO}$	6	, . <b>V</b>
**Derate 2.0 m	W/°C above 25°C	ambient.	

### individual electrical characteristics:(25°C) (See Note 1)

	EMITTER	MIN.	TYP.	MAX.	UNITS
-	Reverse Breakdown Voltage	6	_	_	V
	$V_{(BR)R}$ $I_R = 10 \mu A$ Forward Voltage			1.7	Ÿ
	$V_F = I_F = 60 \mathrm{mA}$				
	Reverse Current	-	-	1	μΑ
	$I_R$ $V_R = 3V$ Capacitance $C_i$ $V = O, f = 1 MHz$		30	_	pF
	•		1		1

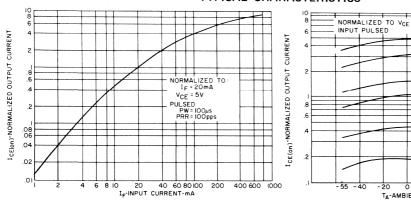
DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage	30	)	_	V
$V_{(BR)CEO}$ $I_C = 1 \text{ mA}$ Breakdown Voltage $V_{(BR)ECO}$ $I_E = 100 \mu A$	6	_	-	v
Collector Dark Current	-	-	100	n <b>A</b>
$I_{CEO} V_{CE} = 25 V$ Capacitance $C_{ce} V_{CE} = 5V, f = 1 MHz$	-	3.3	5	pF

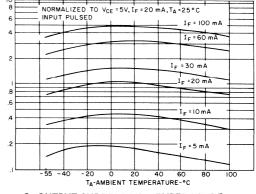
### coupled electrical characteristics:(25°C) (See Note 1)

		H21A1			H21A2	2		H21A3		
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	UNITS
$I_{CE(on)}$ $I_F = 5mA$ , $V_{CE} = 5V$	0.15			0.30	_	_	0.60	_	_	mA
$I_{CE(on)}$ $I_F = 20mA$ , $V_{CE} = 5V$	1.0	_	-	2.0		_	4.0	_		mA
$I_{CE(on)}$ $I_F = 30mA, V_{CE} = 5V$	1.9		_	3.0		_	5.5	-	-	mA
$V_{CE(sat)}$ $I_F = 20mA$ , $I_C = 1.8mA$	-			-		0.40		_ `	0.40	v
$V_{CE(sat)}$ $I_F = 30mA$ , $I_C = 1.8mA$		_	0.40	****		-				V
$t_{on}$ $V_{CC} = 5V, I_F = 30mA, R_L = 2.5K\Omega$	-	8		-	8			8	-	μs
$t_{off}$ $V_{CC} = 5V, I_F = 30mA, R_L = 2.5K\Omega$	-	50		-	50	-		50	- 1	μs

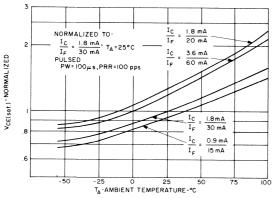
### H21A1, H21A2, H21A3

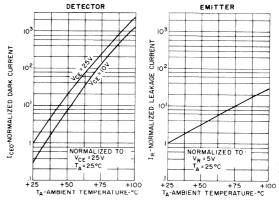
#### TYPICAL CHARACTERISTICS





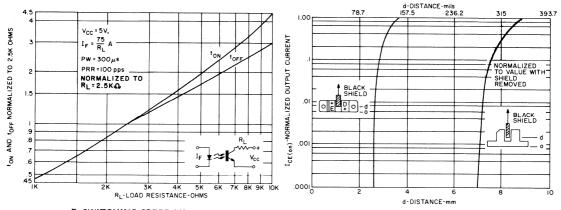
2. OUTPUT CURRENT VS. TEMPERATURE





3. V<sub>CE(sat)</sub> VS. TEMPERATURE

4. LEAKAGE CURRENTS VS. TEMPERATURE



5. SWITCHING SPEED VS.  $R_L$ 

6. OUTPUT CURRENT VS. DISTANCE

### H21A4, H21A5, H21A6

### **Optointerrupter**

GaAs Infrared Emitting Diode and NPN Silicon Phototransistor Module with 1mm Aperture

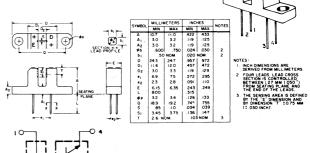
The H21A Interrupter Module is a gallium arsenide infrared emitting diode coupled to a silicon phototransistor in a plastic housing. The packaging system is designed to optimize the mechanical resolution, coupling efficiency, ambient light rejection, cost, and reliability. The gap in the housing provides a means of interrupting the signal with an

opaque material, switching the output from an "ON" into an "OFF" state.

absolute maximum ratings: (25°C)

TOTAL DEVICE		
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	T <sub>STG</sub> T <sub>J</sub> T <sub>L</sub>	-55°C to +100°C -55°C to +100°C 260°C

INFRARED EMITTING DIODE	:		
Power Dissipation	$P_{\rm E}$	*100	mW
Forward Current	$I_{\mathbf{F}}$	60	mA
(Continuous)			
Forward Current (Peak)	$I_F$	3	Α
(Pulse Width $\leq 1 \mu$ s			
PRR ≤ 300 pps)			
Reverse Voltage	$V_R$	6	V
*Derate 1.33 mW/	°C above 25°	°C ambient.	



PHOTOTRANSISTOR			
Power Dissipation Collector Current	$P_D$	**150 100	mW mA
(Continuous) Collector-Emitter Voltage	$V_{CEO}$	55	V
Emitter-Collector Voltage	$V_{ECO}$	6	V

### individual electrical characteristics:(25°C)(See Note 1)

EMITTER	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage	6	-		V
$V_{(BR)R}$ $I_R = 10 \mu A$ Forward Voltage	_		1.7	v
$V_F I_F = 60 \text{ mA}$ Reverse Current	-		1	μА
$I_R V_R = 3V$ Capacitance	-	30	_	pF
$C_i V = O, f = 1 MHz$	1	1		

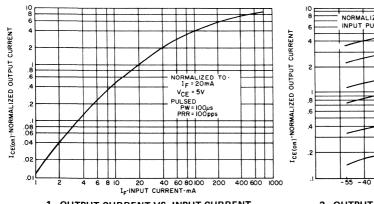
DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage	55	_	_	V
$V_{(BR)CEO}$ $I_C = 1 \text{ mA}$ Breakdown Voltage $V_{(BR)ECO}$ $I_E = 100 \mu \text{A}$	6	_	-	v
Collector Dark Current			100	nA
$ \begin{array}{c c} I_{CEO} & V_{CE} = 45V \\ Capacitance & C_{ce} & V_{CE} = 5V, f = 1 MHz \end{array} $	_	3.3	5	pF

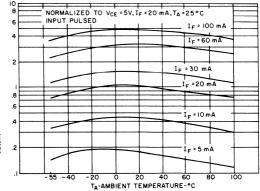
### coupled electrical characteristics:(25°C) (See Note 1)

		H21A4			H21A5			H21A6		
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	UNITS
$I_{CE(on)}$ $I_F = 5mA, V_{CE} = 5V$	0.15		_	0.30	-		0.60	_		mA
$I_{CE(on)}$ $I_F = 20mA$ , $V_{CE} = 5V$	1.0	-	-	2.0	_	_	4.0	_	-	mA
$I_{CE(on)}$ $I_F = 30mA$ , $V_{CE} = 5V$	1.9	-		3.0		_	5.5	-	-	mA
$V_{CE(sat)}$ $I_F = 20mA$ , $I_C = 1.8mA$			_			0.40		-	0.40	V
$V_{CE(sat)}$ $I_F = 30mA$ , $I_C = 1.8mA$	-	-	0.40	-					_	V
$t_{on}$ $V_{CC} = 5V, I_F = 30mA, R_L = 2.5K\Omega$		8	-		8	-		8	-	μs
$t_{off}$ $V_{CC} = 5V, I_F = 30mA, R_L = 2.5K\Omega$	_	50	. —	_	50	-		50	_	μs

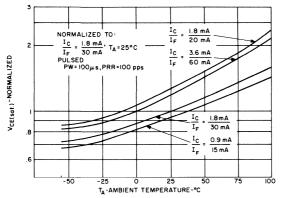
### H21A4, H21A5, H21A6

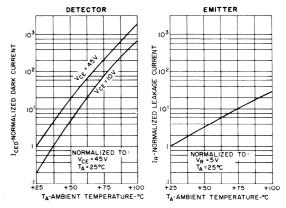
#### TYPICAL CHARACTERISTICS





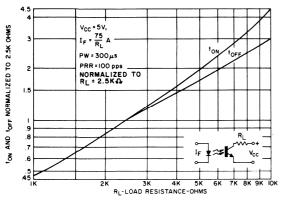


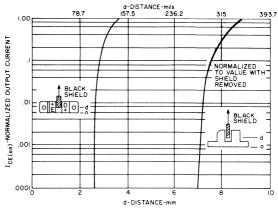




3. V<sub>CE (sat)</sub> VS. TEMPERATURE

4. LEAKAGE CURRENTS VS. TEMPERATURE





5. SWITCHING SPEED VS. R.

6. OUTPUT CURRENT VS. SHIELD DISTANCE

### H21B1, H21B2, H21B3

### **Optointerrupter**

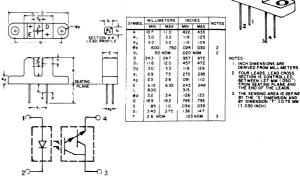
GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier Module with 1mm Aperture

The H21B Interrupter Module is a gallium arsenide infrared emitting diode coupled to a silicon Darlington-connected phototransistor in a plastic housing. The packaging system is designed to optimize the mechanical resolution, coupling efficiency, ambient light rejection, cost, and reliability. The gap in the housing provides a means of interrupting the signal with an opaque material, switching the output from an "ON" into an "OFF" state.

### absolute maximum ratings: (25°C)

TOTAL DEVICE		
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	T <sub>STG</sub> T <sub>J</sub> T <sub>L</sub>	-55°C to +100°C -55°C to +100°C 260°C

INFRARED EMITTING DIOD	E					
Power Dissipation	$P_{\rm E}$	*100	mW			
Forward Current	$I_F$	60	mA			
(Continuous)						
Forward Current (Peak)	$I_{\mathbf{F}}$	3	Α			
(Pulse Width $\leq 1 \mu$ s						
PRR ≤ 300 pps)						
Reverse Voltage	$V_{R}$	6	V			
*Derate 1.33 mW/°C above 25°C ambient.						
L						



DARLINGTON CONNECTED PHOTOTRANSISTOR						
Power Dissipation Collector Current (Continuous)	$P_{D}$ $I_{C}$	**150 100	mW mA			
Collector-Emitter Voltage	$V_{CEO}$	30	V			
Emitter-Collector Voltage	$V_{ECO}$	7	V			
**Derate 2.0 m	ıW/°C above 25°C	ambient.				

### individual electrical characteristics:(25°C) (See Note 1)

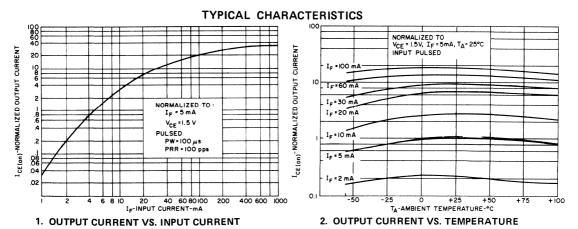
EMITTER	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage	6	_	_	V
$V_{(BR)R}$ $I_R = 10 \mu A$ Forward Voltage	_	_	1.7	V
V <sub>F</sub> I <sub>F</sub> = 60 mA Reverse Current	-	_	1	μA
$ \begin{array}{ll} I_R & V_R = 3V \\ Capacitance \\ C_i & V = O, f = 1 MHz \end{array} $	-	30	-	pF
1 -, -, -, -, -, -, -, -, -, -, -, -, -,	1	1	l	l .

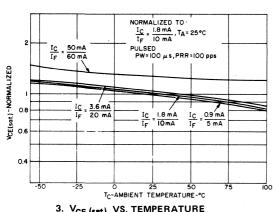
DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage	30	-	-	V
$V_{(BR)CEO}$ $I_C = 1 \text{ mA}$ Breakdown Voltage $V_{(BR)ECO}$ $I_E = 100 \mu A$	7	_	= 1	V
Collector Dark Current $I_{CEO}  V_{CE} = 25 \text{ V}$	-	₹;	100	n <b>A</b>
Capacitance $C_{ce}$ $V_{CE} = 5V, f = 1 MHz$	<del>-</del>	5	8	pF

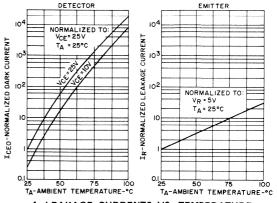
### coupled electrical characteristics: (25 $^{\circ}$ C) (See Note 1)

		H21B1		H21B1 H21B2			H21B1 H21B2 H21B		H21B3			UNITS
- L		MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	UNITS	
I <sub>CE(on)</sub>	$I_{\rm F} = 2mA, V_{\rm CE} = 1.5V$	0.5	_	_	1.0	_	_	2.0	_	-	mA	
I <sub>CE(on)</sub>	$I_{\rm F} = 5 \text{mA}, V_{\rm CE} = 1.5 \text{V}$	2.5		-	5.0		_	10	_	_	mA	
I <sub>CE(on)</sub>	$I_{\rm F} = 10 \text{mA}, V_{\rm CE} = 1.5 \text{V}$	7.5	_		14		_	25	_	_	mA	
V <sub>CE(sat)</sub>		-	_	1.0		-	1.0		_	1.0	V	
V <sub>CE(sat)</sub>	$I_F = 60 \text{mA}, I_C = 50 \text{mA}$	_	-	_	_	_	1.5	-	_	1.5	V	
ton	$V_{CC} = 5V, I_F = 10mA, R_L = 750\Omega$	-	45	-	-	45	_		45		μs	
	$V_{CC} = 5V, I_F = 60mA, R_L = 75\Omega$	-	_	-	_	7			7	_	μs	
toff	$V_{CC} = 5V, I_F = 10mA, R_L = 750\Omega$	-	250	-	_	250		-	250	_	μs	
	$V_{CC} = 5V, I_F = 60mA, R_L = 75\Omega$				_	45	-	-	45	_	μs	

### H21B1, H21B2, H21B3

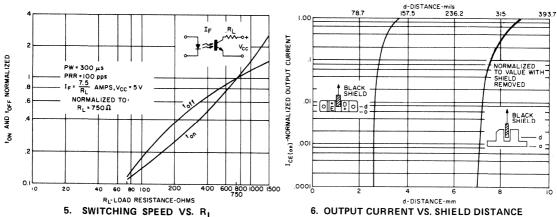












### H21B4, H21B5, H21B6

## **Optointerrupter**

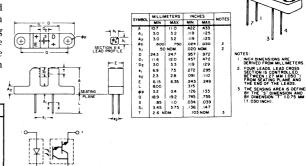
GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier Module with 1mm Aperture

The H21B Interrupter Module is a gallium arsenide infrared emitting diode coupled to a silicon Darlington-connected phototransistor in a plastic housing. The packaging system is designed to optimize the mechanical resolution, coupling efficiency, ambient light rejection, cost, and reliability. The gap in the housing provides a means of interrupting the signal with an opaque material, switching the output from an "ON" into an "OFF" state.

### absolute maximum ratings: (25°C)

TOTAL DEVICE		
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	$T_{\mathrm{STG}}$ $T_{\mathrm{J}}$ $T_{\mathrm{L}}$	-55°C to +100°C -55°C to +100°C 260°C

E		
$P_{E}$	*100	mW
$I_{\mathbf{F}}$	60	mA
$I_{\mathbf{F}}$	3	Α
$V_R$	6	V
°C above 25°	C ambient.	
	$egin{array}{c} P_E \ I_F \ I_F \ \end{array}$	P <sub>E</sub> *100 I <sub>F</sub> 60 I <sub>F</sub> 3



Power Dissipation	$P_{\mathrm{D}}$	**150	mW
Collector Current (Continuous)	$I_C$	100	mA
Collector-Emitter Voltage	$V_{CEO}$	55	V
Emitter-Collector Voltage	$V_{ECO}$	7	V

### individual electrical characteristics:(25°C) (See Note 1)

EMITTER	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage	6	-	ļ	V
$V_{(BR)R}$ $I_R = 10 \mu A$ Forward Voltage		-	1.7	v
V <sub>F</sub> I <sub>F</sub> = 60 mA Reverse Current		-	1	μA
$ \begin{array}{ccc} I_R & V_R = 3V \\ Capacitance \\ C_i & V = O, f = 1 MHz \end{array} $	_	30	-	pF

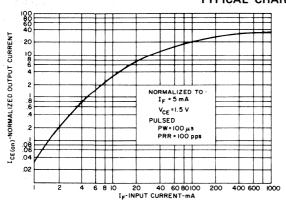
-	_	V V
_	-	V.
_	100	n A
5	8	pF
	5	5 8

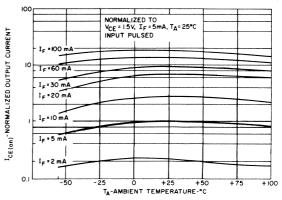
### coupled electrical characteristics:(25°C) (See Note 1)

		H21B4			H21B5			H21B6		
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	UNITS
$I_{CE(on)}$ $I_F = 2mA$ , $V_{CE} = 1.5V$	0.5	_	_	1.0	_		2.0			mA
$I_{CE(on)}$ $I_F = 5mA$ , $V_{CE} = 1.5V$	2.5	-		5.0		-	10	~		mA
$I_{CE(on)}$ $I_{F} = 10mA, V_{CE} = 1.5V$	7.5	_	_	14		_	25	-	_	mA
$V_{CE(sat)}$ $I_F = 10mA, I_C = 1.8mA$		_	1.0	_		1.0	_		1.0	V.
$V_{CE(sat)}$ $I_F = 60mA$ , $I_C = 50mA$		-	_	_	_	1.5	_		1.5	V
$t_{on}$ $V_{CC} = 5V, I_F = 10mA, R_L = 750\Omega$	_	45	_	_	45	-	_	45	-	μs
$V_{CC} = 5V, I_F = 60mA, R_L = 75\Omega$	-	-		-	- 7		-	7		μs
$t_{off}$ $V_{CC} = 5V, I_F = 10mA, R_L = 750\Omega$		250		_	250		-	250		μs
$V_{CC} = 5V, I_F = 60mA, R_L = 75\Omega$	-	_		-	45		·	45	_	μs

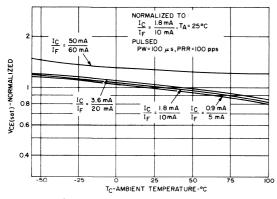
### H21B4, H21B5, H21B6

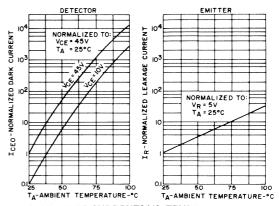
#### TYPICAL CHARACTERISTICS





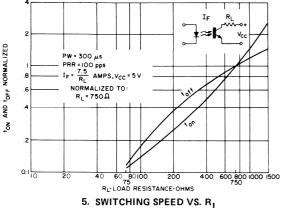
2. OUTPUT CURRENT VS. TEMPERATURE

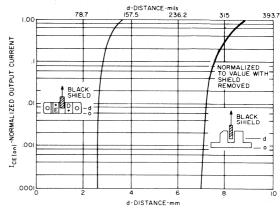




3. V<sub>CE (sat)</sub> VS. TEMPERATURE







6. OUTPUT CURRENT VS. SHIELD DISTANCE

### H21L1, H21L2

## **Optointerrupter**

an "ON" into an "OFF" state.

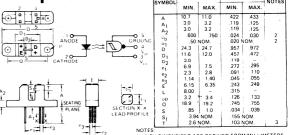
GaAs Infrared Emitting Diode and Microprocessor Compatible Schmitt Trigger Module with 1mm Aperture

The H21L series is a gallium arsenide infrared emitting diode coupled to a high-speed integrated circuit detector. The output incorporates a Schmitt trigger which provides hysteresis for noise immunity and pulse shaping. The gap in the housing provides a means of interrupting the signal with an opaque material, switching the output from

absolute maximum ratings: (25°C)

TOTAL DEVICE		
Storage Temperature	T <sub>STG</sub>	-55°C to +85°C
Operating Temperature	$T_{I}$	-55°C to +85°C
Lead Soldering Temperature (5 seconds maximum)	$T_{L}$	260°C

INFRARED EMITTING DIOD	E		
Power Dissipation	PE	*100	mW
Forward Current (Continuous)	$I_{\mathbf{F}}$	60	mA
Forward Current (Peak) (Pulse width $\leq 1 \mu s$	I <sub>F</sub>	3	Α
$PRR \le 300 \text{ pps}$			
Reverse Voltage	$V_R$	6	V
*Derate 1.33 mW/°	C above 25	C ambient.	



1. INCH DIMENSIONS ARE DERIVED FROM MILLIMETERS.

- 2. FOUR LEADS, LEAD CROSS SECTION IS CONTROLLED BETWEEN 1.27 MM (.050") FROM SEATING PLANE AND THE END OF THE LEADS.
- THE SENSING AREA IS DEFINED BY THE "S" DIMENSION AND BY DIMENSION "T" 0.75 MM (+.030 inch).

$\begin{array}{ccccc} \text{Output Current} & \text{I}_4 & \text{50} & \text{m} \\ \text{Allowed Range} & \text{V}_{35} & \text{0 to 16} & \text{V} \\ \text{Allowed Range} & \text{V}_{45} & \text{0 to 16} & \text{V} \end{array}$	Power Dissipation	$P_{\mathrm{D}}$	**150	mW			
99	Output Current	$I_4$	50	mA			
Allowed Range V <sub>45</sub> 0 to 16 V	Allowed Range	$V_{35}$	0 to 16	- V			
	Allowed Range	$V_{45}$	0 to 16	V			
**Derate 2.0 mW/°C above 25°C ambient.	**Derate 2.0 mW/°C above 25°C ambient.						

### individual electrical characteristics: (0-70°C) (See Note 1)

EMITTER		MIN.	TYP.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> = 20 mA)	$V_{F}$	_	1.10	1.60	volts
Reverse Current (V <sub>R</sub> = 3V)	$I_R$			10	micro- ampere
Capacitance (V = 0, f = 1 MHz)	$C_{J}$	arranger them.		100	pico- farads

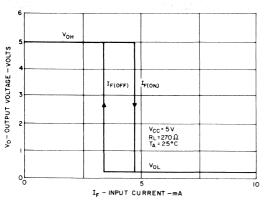
DETECTOR	MIN.	TYP.	MAX.	UNITS
Operating Voltage Range V <sub>C</sub>	4		15	volts
Supply Current $I_{3(off)}$ $(I_F = 0, V_{CC} = 5V)$	_	1.0	5.0	milli- ampere
Output Current, High $I_{OH}$ ( $I_F = 0$ , $V_{CC} = V_O = 15V$ )			100	micro- ampere

### coupled electrical characteristics (0-70°C) (See Note 1)

			MIN.	TYP.	MAX.	UNITS
Supply Current	I <sub>3(on)</sub>			1.6	5.0	milliampere
$(I_F = 20 \text{mA}, V_{CC} = 5 \text{V})$						i i
Output Voltage, Low	$V_{OL}$			0.2	0.4	volts
$(R_L = 270\Omega \ V_{CC} = 5V, I_F = 30 \ mA)$					4. 4.	
Turn-On Threshold Current	$I_{F(on)}$	H21L1, H22L1			30	milliampere
$(R_L = 270\Omega, V_{CC} = 5V)$		H21L2, H22L2			15.0	milliampere
Turn-Off Threshold Current	$I_{F(off)}$	H21L1, H22L2	0.5	15		milliampere
$(R_L = 270\Omega, V_{CC} = 5V)$	$I_{F(off)}$	H21L1, H22L2	0.5	8	_	milliampere
Hysteresis Ratio	$I_{F(off)}/I_{F(on)}$		0.50	0.75	0.90	
$(R_L = 270\Omega, V_{CC} = 5V)$						
Switching Speeds: ( $R_L = 270\Omega$ , $V_{CC} = 5V$ ,	$T_A = 25^{\circ} C$ , $I_F = 20$	mA)				
Rise Time	t <sub>r</sub>		_	0.1		μsec.
Fall Time	t <sub>f</sub>			0.1		μsec.

### H21L1, H21L2

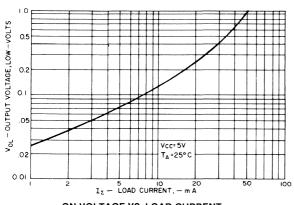
#### TYPICAL CHARACTERISTICS

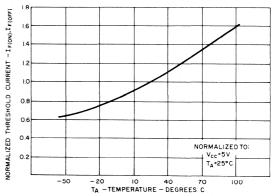


- NORMALIZED THRESHOLD CURRENT
O O O
P TURN ON THRESHOLD TURN OFF THRESHOLD NORMALIZED TO TURN ON THRESHOLD AT V<sub>CC</sub>=5V, T<sub>A</sub>=25°C 0 Vcc - SUPPLY VOLTAGE , VOLTS

TRANSFER CHARACTERISTICS

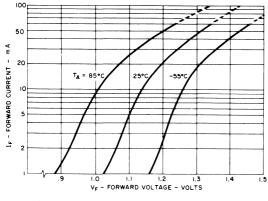
THRESHOLD CURRENT VS. SUPPLY VOLTAGE

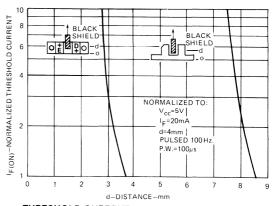




ON VOLTAGE VS. LOAD CURRENT

THRESHOLD CURRENTS VS. TEMPERATURE





FORWARD VOLTAGE VS. FORWARD CURRENT

THRESHOLD CURRENT VS. SHIELD DISTANCE

### H22A1, H22A2, H22A3

### **Optointerrupter**

GaAs Infrared Emitting Diode and NPN Silicon Photo-Transistor

**Amplifier Module with 1mm Aperture** 

The H22A Interrupter Module is a gallium arsenide infrared emitting diode coupled to a silicon phototransistor in a plastic housing. The packaging system is designed to optimize the mechanical resolution, coupling efficiency, ambient light rejection, cost, and reliability. The gap in the housing provides a means of interrupting the signal with an opaque material, switching the output from an "ON" into an "OFF" state.

#### absolute maximum ratings: (25°C)

TOTAL DEVICE		
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	$T_{\mathrm{STG}}$ $T_{\mathrm{J}}$ $T_{\mathrm{L}}$	-55°C to +100°C -55°C to +100°C 260°C

INFRARED EMITTING DIOD	E		
Power Dissipation	$P_{\rm E}$	*100	mW
Forward Current	$\widetilde{\mathrm{I_F}}$	60	mA
(Continuous)			
Forward Current (Peak)	$I_{\mathbf{F}}$	3	Α
(Pulse Width $\leq 1 \mu$ s			
$PRR \leq 300  pps$ )			
Reverse Voltage	$V_R$	6	V
*Derate 1.33 mW/	°C above 25°	C ambient.	

PHOTOTRANSISTOR			
Power Dissipation Collector Current (Continuous)	$P_{D}$ $I_{C}$	**150 100	mW mA
Collector-Emitter Voltage	$V_{CEO}$	30	V
Emitter-Collector Voltage	$V_{ECO}$	6	V
· ·	nW/°C above 25°C	ambient.	

### individual electrical characteristics:(25°C) (See Note 1)

EMITTER	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage	6	_	_	V
$V_{(BR)R}$ $I_R = 10 \mu A$				
Forward Voltage	-	-	1.7	V
$V_F I_F = 60 \mathrm{mA}$		l		
Reverse Current	-	_	1	μA
$I_R V_R = 3V$				
Capacitance	-	30		pF
$C_i$ $V = O, f = 1 MHz$	1			

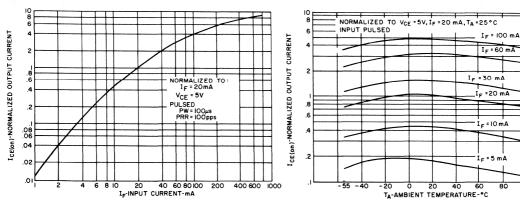
DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage	30		_	V
$V_{(BR)CEO}$ $I_C = 1 \text{ mA}$				
Breakdown Voltage	6	_		V
$V_{(BR)ECO}$ $I_E = 100 \mu A$	·	l		ł
Collector Dark Current	-	-	100	n <b>A</b>
$I_{CEO}$ $V_{CE} = 25 V$		l	_	_
Capacitance	-	3.3	5	pF
$C_{ce}$ $V_{CE} = 5V, f = 1 MHz$				

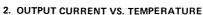
### coupled electrical characteristics:(25°C) (See Note 1)

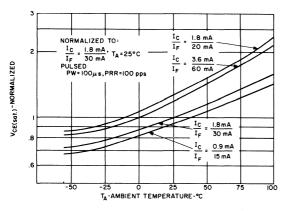
		H22A1		H22A2		2	H22A3			UNITS
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	UNITS
$I_{CE(on)}$ $I_F = 5mA, V_{CE} = 5V$	0.15	_	ı	0.30	_	_	0.60	_	_	mA
$I_{CE(on)}$ $I_F = 20mA$ , $V_{CE} = 5V$	1.0		-	2.0	_		4.0		_	mA
$I_{CE(on)}$ $I_F = 30mA$ , $V_{CE} = 5V$	1.9		_	3.0		-	5.5		_	mA
$V_{CE(sat)}$ $I_{F} = 20mA, I_{C} = 1.8mA$		-	_	-		0.40	_	_	0.40	v
$V_{CE(sat)}$ $I_F = 30mA$ , $I_C = 1.8mA$	,		0.40		_				-	V
$t_{on}$ $V_{CC} = 5V, I_F = 30mA, R_L = 2.5K\Omega$	-	8		_	8	_		8		μs
$t_{off}$ $V_{CC} = 5V, I_F = 30mA, R_L = 2.5K\Omega$	_	50	_	_	50	7	_	50		μs

### H22A1, H22A2, H22A3

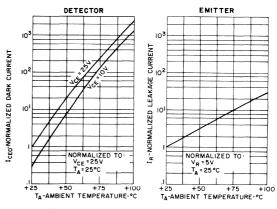
#### TYPICAL CHARACTERISTICS



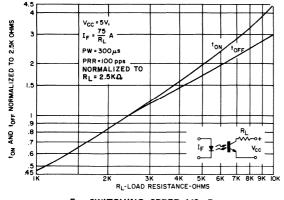




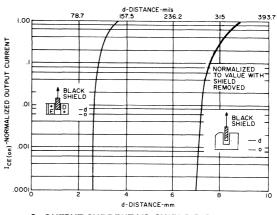
3. V<sub>CE (sat)</sub> VS. TEMPERATURE



4. LEAKAGE CURRENTS VS. TEMPERATURE



5. SWITCHING SPEED VS. R.



6. OUTPUT CURRENT VS. SHIELD DISTANCE

### H22A4, H22A5, H22A6 Optointerrupter

## GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

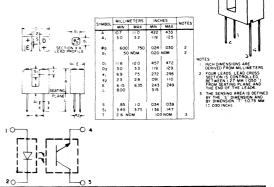
Module with 1mm Aperture

The H22A Interrupter Module is a gallium arsenide infrared emitting diode coupled to a silicon phototransistor in a plastic housing. The packaging system is designed to optimize the mechanical resolution, coupling efficiency, ambient light rejection, cost, and reliability. The gap in the housing provides a means of interrupting the signal with an opaque material, switching the output from an "ON" into an "OFF" state.

### absolute maximum ratings: (25°C)

TOTAL DEVICE		
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	$T_{STG}$ $T_J$ $T_L$	-55°C to +100°C -55°C to +100°C 260°C

INFRARED EMITTING DIOD	E		
Power Dissipation	$P_{\rm E}$	*100	mW
Forward Current	$I_{\mathbf{F}}$	60	mA
(Continuous)			
Forward Current (Peak)	$I_{\mathbf{F}}$	3	Α
(Pulse Width $\leq 1 \mu$ s			
$PRR \le 300 \text{ pps}$			
Reverse Voltage	$V_R$	6	V
*Derate 1.33 mW/	'C ambient.		



PHOTOTRANSISTOR			
Power Dissipation	P <sub>D</sub>	**150	mW
Collector Current	$I_{C}$	100	m <b>A</b>
(Continuous)			
Collector-Emitter	$V_{CEO}$	55	V
Voltage			
Emitter-Collector	$V_{ECO}$	6	V
Voltage			
**Derate 2.0 n	nW/°C above 25°C	ambient.	
	•		

### individual electrical characteristics:(25°C) (See Note 1)

EMITTER	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage	6	_	-	V
$V_{(BR)R}$ $I_R = 10 \mu A$				
Forward Voltage	-	-	1.7	V
$V_F I_F = 60 \mathrm{mA}$				
Reverse Current		-	1	μA
$I_R V_R = 3V$			)	
Capacitance	_	30		pF
$C_i$ $V = O, f = 1 MHz$	l			

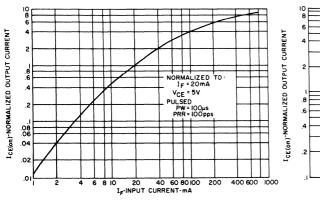
DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage	55	_	_	V
$V_{(BR)CEO}$ $I_C = 1 \text{ mA}$				-
Breakdown Voltage	6	-		V .
$V_{(BR)ECO}$ $I_E = 100 \mu A$				
Collector Dark Current	_	_	100	n <b>A</b>
$I_{CEO}$ $V_{CE} = 45V$			_	_
Capacitance	name.	3.3	5	pF
$C_{ce}$ $V_{CE} = 5V$ , $f = 1 MHz$				

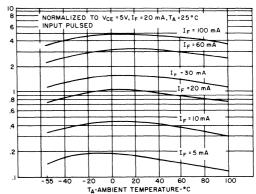
### coupled electrical characteristics:(25°C) (See Note 1)

		H22A4			H22A5			H22A6		UNITS
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	UNITS
$I_{CE(on)}$ $I_F = 5mA$ , $V_{CE} = 5V$	0.15	Phase .	_	0.30	_	_	0.60	_	_	mA
$I_{CE(on)}$ $I_F = 20mA$ , $V_{CE} = 5V$	1.0	-	-	2.0		_	4.0		-	mA
$I_{CE(on)}$ $I_F = 30mA$ , $V_{CE} = 5V$	1.9	~~~		3.0		_	5.5	_	-	mA
$V_{CE(sat)}$ $I_F = 20mA$ , $I_C = 1.8mA$	-	-		-		0.40	-		0.40	v
$V_{CE(sat)}$ $I_F = 30mA, I_C = 1.8mA$			0.40				-	_		V
$t_{on}$ $V_{CC} = 5V, I_F = 30mA, R_L = 2.5K\Omega$	1	8			8	_		8		μs
$t_{off}$ $V_{CC} = 5V, I_F = 30mA, R_L = 2.5K\Omega$	_	50	_	_	50		<u></u>	50	-	μs

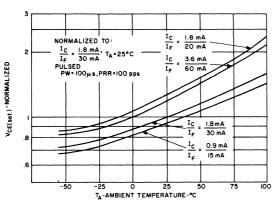
Note 1: Stray irradiation can alter values of characteristics. Adequate shielding should be provided.

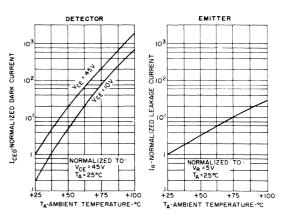
#### TYPICAL CHARACTERISTICS





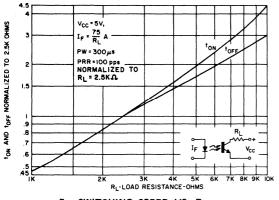
2. OUTPUT CURRENT VS. TEMPERATURE

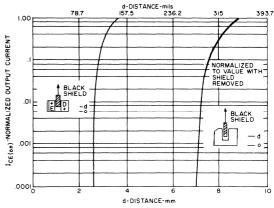




3. V<sub>CE (sat)</sub> VS. TEMPERATURE

4. LEAKAGE CURRENTS VS. TEMPERATURE





5. SWITCHING SPEED VS. RI

6. OUTPUT CURRENT VS. SHIELD DISTANCE

### H22B1, H22B2, H22B3

### **Optointerrupter**

GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington

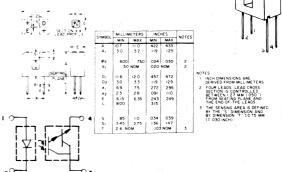
Module with 1mm Aperture

The H22B Interrupter Module is a gallium arsenide infrared emitting diode coupled to a silicon Darlington-connected phototransistor in a plastic housing. The packaging system is designed to optimize the mechanical resolution, coupling efficiency, ambient light rejection, cost, and reliability. The gap in the housing provides a means of interrupting the signal with an opaque material, switching the output from an "ON" into an "OFF" state.

### absolute maximum ratings: (25°C)

TOTAL DEVICE		
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	$T_{\mathrm{STG}}$ $T_{\mathrm{J}}$ $T_{\mathrm{L}}$	-55°C to +100°C -55°C to +100°C 260°C

INFRARED EMITTING DIOD	E		
Power Dissipation	$\overline{P_{\rm E}}$	*100	mW
Forward Current (Continuous)	$I_{\mathrm{F}}$	60	mA
Forward Current (Peak) (Pulse Width ≤ 1 µs	$I_{\mathrm{F}}$	3	A
PRR ≤ 300 pps) Reverse Voltage *Derate 1.33 mW/	V <sub>R</sub> °C above 25°	6 C ambient.	v



DARLINGTON CONNECTED PHOTOTRANSISTOR							
Power Dissipation Collector Current (Continuous)	$rac{ extbf{P}_{ ext{D}}}{ ext{I}_{ ext{C}}}$	**150 100	mW mA				
Collector-Emitter Voltage	$V_{CEO}$	30	V				
Emitter-Collector Voltage	$V_{ECO}$	7	<b>V</b>				
**Derate 2.0 m	W/°C above 25°C	ambient.					

### individual electrical characteristics:(25°C) (See Note 1)

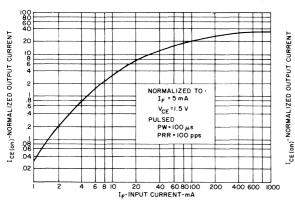
EMITTER	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage	6	_		V
$V_{(BR)R}$ $I_R = 10 \mu A$ Forward Voltage	_		1.7	V
$V_F I_F = 60 \mathrm{mA}$				
Reverse Current		-	1	μΑ
$ \begin{array}{c c} I_R & V_R = 3V \\ Capacitance \\ C_i & V = O, f = 1 MHz \end{array} $	emen	30	_	pF

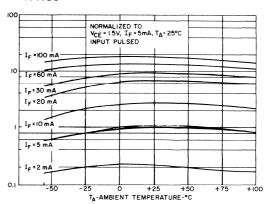
DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage	30	. —		V
$V_{(BR)CEO}$ $I_C = 1 \text{ mA}$ Breakdown Voltage $V_{(BR)ECO}$ $I_E = 100 \mu \text{A}$	7	_	<del></del> }	<b>V</b>
Collector Dark Current	_	-	100	n <b>A</b>
$I_{CEO}$ $V_{CE} = 25 V$ Capacitance $C_{ce}$ $V_{CE} = 5V$ , $f = 1 MHz$	<del></del>	5	8 "	pF

### coupled electrical characteristics:(25°C) (See Note 1)

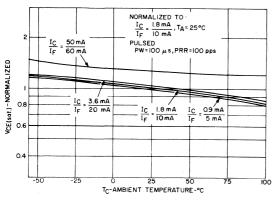
			H22B1			H22B2			H22B3		UNITS
		MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	0.1110
I <sub>CE(on)</sub>	$I_{\rm F} = 2mA, V_{\rm CE} = 1.5V$	0.5	_	<u>-</u>	1.0	_		2.0			m <b>A</b>
I <sub>CE(on)</sub>	$I_{\rm F} = 5 \text{mA}, V_{\rm CE} = 1.5 \text{V}$	2.5	_		5.0		-	10	-	_	m <b>A</b>
I <sub>CE(on)</sub>	$I_{\rm F} = 10 \text{mA}, V_{\rm CE} = 1.5 \text{V}$	7.5	_	_	14		_	25		-	mA
V <sub>CE(sat)</sub>	$I_{\rm F} = 10  \text{mA}, I_{\rm C} = 1.8  \text{mA}$	_		1.0	-		1.0		-	1.0	V
V <sub>CE(sat)</sub>	$I_{\rm F} = 60  \text{mA}, I_{\rm C} = 50  \text{mA}$	_ '	-	l –			1.5	_	-	1.5	V
ton	$V_{CC} = 5V, I_F = 10mA, R_L = 750\Omega$	l –	45	_	-	45	-	-	45	-	μs
	$V_{CC} = 5V, I_F = 60 \text{mA}, R_L = 75 \Omega$	l –	_		-	7	-	_	7		μs
toff	$V_{CC} = 5V, I_F = 10mA, R_L = 750\Omega$		250		-	250		-	250	_	μs
	$V_{CC} = 5V, I_F = 60mA, R_L = 75\Omega$	-	_		_	45	_	_	45	_	μs

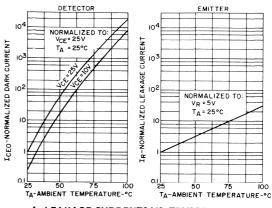
TYPICAL CHARACTERISTICS





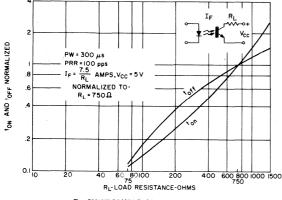
2. OUTPUT CURRENT VS. TEMPERATURE

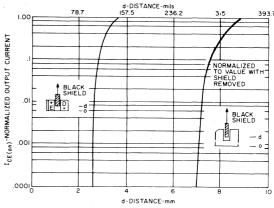




3. V<sub>CE (sat)</sub> VS. TEMPERATURE

4. LEAKAGE CURRENTS VS. TEMPERATURE





5. SWITCHING SPEED VS. R

6. OUTPUT CURRENT VS. SHIELD DISTANCE

### H22B4, H22B5, H22B6

### **Optointerrupter**

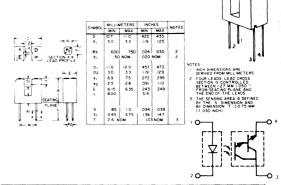
GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier Module with 1mm Aperture

The H22B Interrupter Module is a gallium arsenide infrared emitting diode coupled to a silicon Darlington-connected phototransistor in a plastic housing. The packaging system is designed to optimize the mechanical resolution, coupling efficiency, ambient light rejection, cost, and reliability. The gap in the housing provides a means of interrupting the signal with an opaque material, switching the output from an "ON" into an "OFF" state.

### absolute maximum ratings: (25°C)

TOTAL DEVICE		
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	$egin{array}{l} T_{ m STG} \ T_{ m J} \ T_{ m L} \end{array}$	-55°C to +100°C -55°C to +100°C 260°C

$P_{\rm E}$	*100	mW				
$I_F$	60	m <b>A</b>				
$I_F$	3	A				
$V_R$	6	V				
*Derate 1.33 mW/°C above 25°C ambient.						
	$I_{ m F}$ $I_{ m F}$ $V_{ m R}$	$I_F$ 60 $I_F$ 3 $V_R$ 6				



DARLINGTON CONNECTED PHOTOTRANSISTOR							
Power Dissipation	$P_{D}$	**150	mW				
Collector Current (Continuous)	$I_{\rm C}$	100	mA				
Collector-Emitter Voltage	$V_{CEO}$	55	V				
Emitter-Collector Voltage	$V_{ECO}$	7	V				
**Derate 2.0 mW/°C above 25°C ambient.							

### individual electrical characteristics:(25°C) (See Note 1)

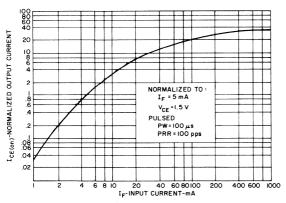
EMITTER	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage	6	_	1	V
$V_{(BR)R}$ $I_R = 10 \mu A$ Forward Voltage $V_F$ $I_F = 60 \text{ mA}$		-	1.7	V
Reverse Current	_		1	μA
$ \begin{array}{c c} I_R & V_R = 3V \\ Capacitance \\ C_i & V = O, f = 1 MHz \end{array} $	_	30	-	pF

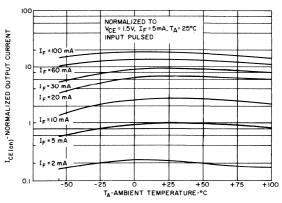
DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage	55	-	_	V
$V_{(BR)CEO}$ $I_C = 1 \text{ mA}$ Breakdown Voltage $V_{(BR)ECO}$ $I_E = 100 \mu A$	7		-	V
Collector Dark Current	-	-	100	n <b>A</b>
$ \begin{vmatrix} I_{CEO} & V_{CE} = 45V \\ Capacitance \\ C_{ce} & V_{CE} = 5V, f = 1 MHz \end{vmatrix} $	_	5	8	pF

### coupled electrical characteristics:(25°C) (See Note 1)

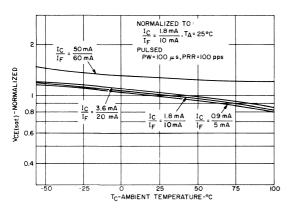
		H22B4			H22B5			H22B6		
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.	UNITS
$I_{CE(on)}$ $I_{F} = 2mA, V_{CE} = 1.5V$	0.5	_	-	1.0	_	_	2.0	_	_	mA
$I_{CE(on)}$ $I_{F} = 5mA, V_{CE} = 1.5V$	2.5		-	5.0	_	-	10			mA
$I_{CE(on)}$ $I_{F} = 10mA, V_{CE} = 1.5V$	7.5	-	-	14	-		25	_		mA
$V_{CE(sat)}$ $I_F = 10mA$ , $I_C = 1.8mA$	_	_	1.0	_		1.0		_	1.0	V
$V_{CE(sat)}$ $I_F = 60 \text{mA}, I_C = 50 \text{mA}$		-			_	1.5	_	_	1.5	V
$t_{on}$ $V_{CC} = 5V, I_F = 10mA, R_L = 750\Omega$	_	45	_		45		_	45		μs
$V_{CC} = 5V, I_F = 60mA, R_L = 75\Omega$	-	-	_		7	-	_	7	-	μs
$t_{off}$ $V_{CC} = 5V, I_F = 10mA, R_L = 750\Omega$	- 1	250	-	-	250	-	_	250	-	μs
$V_{CC} = 5V$ , $I_F = 60mA$ , $R_L = 75\Omega$	-	_	_		45			45		μs

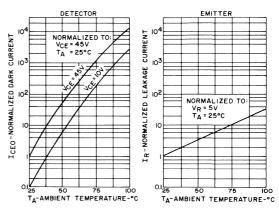
#### TYPICAL CHARACTERISTICS





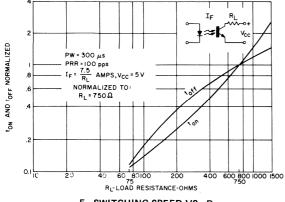
2. OUTPUT CURRENT VS. TEMPERATURE

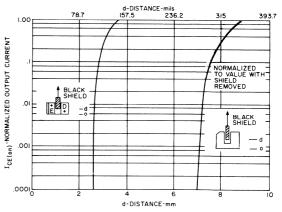




3. V<sub>CE (sat)</sub> VS. TEMPERATURE

4. LEAKAGE CURRENTS VS. TEMPERATURE





5. SWITCHING SPEED VS. R

6. OUTPUT CURRENT VS. SHIELD DISTANCE

### H22L1, H22L2

**Optointerrupter** 

GaAs Infrared Emitting Diode and Microprocessor Compatible Schmitt Trigger Module with 1mm Aperture

The H22L series is a gallium arsenide, infrared emitting diode coupled to a high-speed integrated circuit detector. The output incorporates a Schmitt trigger which provides hysteresis for noise immunity and pulse shaping. The gap in the plastic housing provides a means of interrupting the signal with an opaque material, switching the output from an "ON" into an "OFF" state.

TOTAL DEVICE		
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	T <sub>STG</sub> T <sub>J</sub> T <sub>L</sub>	-55°C to +85°C -55°C to +85°C 260°C

Power Dissipation	$P_{E}$	*100	mW
Forward Current	$I_{\mathbf{F}}$	60	mA
(Continuous)			
Forward Current (Peak)	$I_{\mathbf{F}}$	3	Α
(Pulse width $\leq 1 \mu s$			
$PRR \leq 300 \text{ pps}$			
Reverse Voltage	$V_R$	6	V

			MILLIN	ETERS	IN	СН	
ire		SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
2 3		А	10.7	11.0	.422	.433	
04	- 111	Α-	3.0	3.2	.119	.125	
<u>→</u> •	I P	ob	.600	.750	.024	.030	2
D <sub>1</sub> 5	05	b <sub>1</sub>	.50 1	VOM.	.020	NOM.	2
D2 ANODE	L GROUNE	D <sub>1</sub>	11.6	12.0	.457	.472	
<b>√</b>	17 A	D <sub>2</sub>	3.0	-	.119		
		e <sub>1</sub>	6.9	7.5	.272	.295	
CATHODE	O 3	e <sub>2</sub>	2.3	2.8	.091	.110	1
I CATHOUS E IS	V <sub>cc</sub>		1.14	1.4	.045	.055	
Is <sub>1</sub>	₩ b†	e <sub>3</sub>	6.15	6.35	.243	.249	i .
T 1 A	(-a-1-	L	8.00		.315	-	
SEATING		S	.85	1.0	.034	.039	
AT THE PLANE THE	SECTION X X	S <sub>1</sub>	3.94	NOM.	.155 /	NOM.	
^', T	LEAD PROFILE	Т	2.6 1	NOM.	103 (	NOM.	3
-e1- e3 e3-1-e2	NOTES:	DIMENS	04/6 4 0/	DEDIVI	D EBON	4 AALL 1 IN	ETERS

- I. INCH DIMENSIONS ARE DERIVED FROM MILLIMETER
- 2. FOUR LEADS, LEAD CROSS SECTION IS CONTROLLED BETWEEN 1.27 MM (.050") FROM SEATING PLANE AND THE END OF THE LEADS.
- THE SENSING AREA IS DEFINED BY THE "S" DIMENSION AND BY DIMENSION "T" ±0.75 MM (±.030 INCH).

Power Dissipation	$P_{D}$	**150	mW
Output Current	$I_4$	50	mA
Allowed Range	$V_{35}$	0 to 16	V
Allowed Range	$V_{45}$	0 to 16	V
**Derate 2.0 mV	W/°C above 25°	°C ambient.	

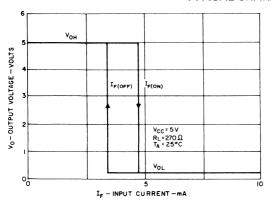
### individual electric characteristics: (0-70°C) (See Note 1)

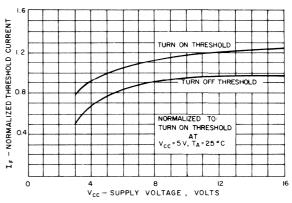
EMITTER		MIN.	TYP.	мах.	UNITS
Forward Voltage (I <sub>F</sub> = 20 mA)	$V_{\rm F}$	_	1.10	1.60	volts
Reverse Current (V <sub>R</sub> = 3V)	$I_R$	_		10	micro- ampere
Capacitance (V = 0, f = 1 MHz)	$C_J$			100	pico- farads

DETECTOR	MIN.	TYP.	MAX.	UNITS
Operating Voltage Range V <sub>C</sub>	4	_	15	volts
Supply Current $I_{3(off)}$ $(I_F = 0, V_{CC} = 5V)$		1.0	5.0	milli- ampere
Output Current, High $I_{OH}$ $(I_F = 0, V_{CC} = V_O = 15V)$			100	micro- ampere

			MIN.	TYP.	MAX.	UNITS
Supply Current	I <sub>3(on)</sub>		_	1.6	5.0	milliampere
$(I_F = 20 \text{mA}, V_{CC} = 5 \text{V})$						
Output Voltage, Low	$V_{OL}$			0.2	0.4	volts
$(R_L = 270\Omega \ V_{CC} = 5V, \ I_F = 30 \ mA)$						
Turn-On Threshold Current	$I_{F(on)}$	H22L1	_	20	30	milliampere
$(R_L = 270\Omega, V_{CC} = 5V)$		H22L2	<del>-</del>	10	15.0	milliampere
Turn-Off Threshold Current	$I_{F(off)}$	H22L1	0.5	15		milliampere
$(R_L = 270\Omega, V_{CC} = 5V)$	$I_{\Gamma(\text{off})}$	H22L2	0.5	8		milliampere
Hysteresis Ratio	$I_{F(off)}/I_{F(on)}$		0.50	0.75	0.90	
$(R_L = 270\Omega, V_{CC} = 5V)$						
Switching Speeds: ( $R_L = 270\Omega$ , $V_{CC} = 5V$ , $T_{CC} = 5V$	$I_A = 25^{\circ} \text{C}, I_F = 20 \text{ mA}$	)				
Rise Time	$t_{r}$		_	0.1	_	μsec.
Fall Time	tf			0.1		μsec.

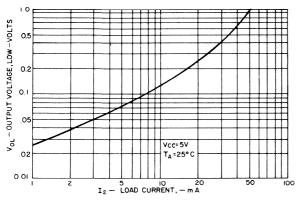
#### TYPICAL CHARACTERISTICS

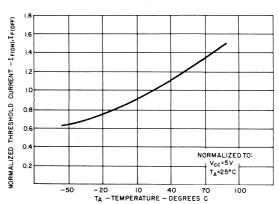




#### TRANSFER CHARACTERISTICS

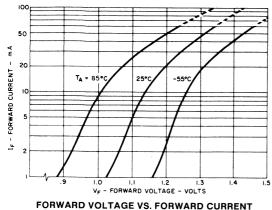
THRESHOLD CURRENT VS. SUPPLY VOLTAGE

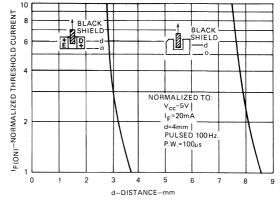




ON VOLTAGE VS. LOAD CURRENT

THRESHOLD CURRENTS VS. TEMPERATURE





THRESHOLD CURRENT VS. SHIELD DISTANCE

#### H23A1, H23A2

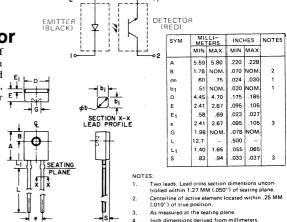
# Matched Emitter-Detector Pair GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The H23A1 is a matched emitter-detector pair which consists of a gallium arsenide infrared emitting diode and a silicon phototransistor. The clear epoxy packaging system is designed to optimize the mechanical resolution, coupling efficiency, cost, and reliability. The devices are marked with a color dot for easy identification of the emitter and detector.

#### absolute maximum ratings: (25°C)

EMITTER-DETECTOR PAIR					
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	$T_{STG}$ $T_{J}$ $T_{L}$	-55°C to +100°C -55°C to +100°C 260°C			

INFRARED EMITTIN	G DIOD	E	
Power Dissipation	$P_{\rm E}$	*100	mW
Forward Current (Continuous)	$I_{\mathrm{F}}$	60	mA
Forward Current (Peak) (Pulse Width ≤ 1µs PRR ≤ 300 pps)	$I_{\mathbf{F}}$	3	Α
Reverse Voltage	$V_R$	6	V
*Derate 1.33 mW/°	C above 25°	'C ambient.	



PHOTOTRANSISTO	OR		
Power Dissipation	$P_{D}$	**150	mW
Collector Current (Continuous)	$I_{C}$	100	mA
Collector-Emitter Voltage	$V_{CEO}$	30	V
Emitter-Collector Voltage	$V_{ECO}$	6	V
**Derate	2.0 mW/°C abov	ve 25°C ambient	i. '

## individual electrical characteristics (25°C) (See Note 1)

EMITTER	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage	6	_	www	V
$V_{(BR)R}$ $I_R = 10\mu A$		-		
Forward Voltage			1.7	V.
$V_F I_F = 60 \text{ mA}$				
Reverse Current	-	-	1	μA
$I_R V_R = 3V$				
Capacitance	-	30	_	pF
$C_i V = O, f = 1 MHz$				

500 11010 1)			,	
DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage	30	_	_	V
V <sub>(BR)CEO</sub> I <sub>C</sub> = 1 mA Breakdown Voltage	6		_	v
$V_{(BR)ECO}$ $I_E = 100\mu A$ Collector Dark Current	_		100	n <b>A</b>
$I_{CEO}$ $V_{CE} = 25V$ Capacitance	-	3.3	5	pF
$C_{ce}$ $V_{CE} = 5V$ , $f = 1$ MHz				

# coupled electrical characteristics (25°C)(See Note 1)

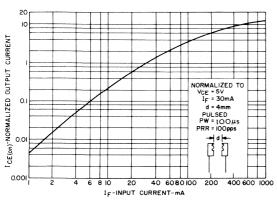
Note: Coupled electrical characteristics are measured at a separation distance of 4mm (.155 inches) with the lenses of the emitter and detector on a common axis within 0.1mm and parallel within 5°.

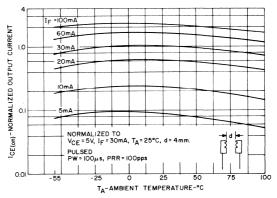
		100	MIN.	TYP.	MAX.	UNITS
I <sub>CE(on)</sub>	$IF = 30 \text{mA}, V_{CE} = 5 V$	H23A1:	1.5	_		mA
		H23A2:	1.0	_	<u> </u>	mA
V <sub>CE(sat)</sub>	$I_F = 30 \text{mA}, I_C = 1.8 \text{mA}$	H23A1:	l ' '		0.40	V
	$I_F = 30 \text{mA}, I_C = .5 \text{mA}$	H23A2:			0.40	V
t <sub>on</sub>	$V_{CC} = 5V, I_F = 30 \text{mA}, R_L = 2.5 \text{K}\Omega$			8	l —	μs
t <sub>off</sub>	$V_{CC} = 5V, I_F = 30mA, R_L = 2.5K\Omega$			50		μs

Note 1: Stray irradiation can alter values of characteristics. Adequate shielding should be provided.

# H23A1, H23A2

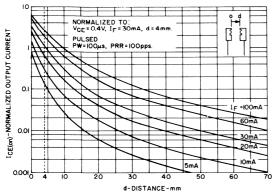
#### TYPICAL CHARACTERISTICS

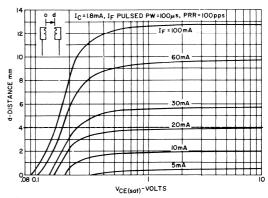




#### 1. OUTPUT CURRENT VS. INPUT CURRENT

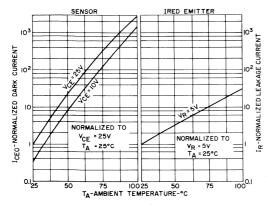
2. OUTPUT CURRENT VS. TEMPERATURE

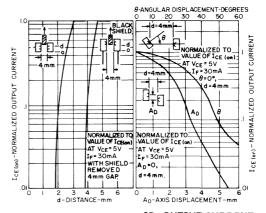




3. OUTPUT CURRENT VS. DISTANCE

4. V<sub>CE(sat)</sub> VS. DISTANCE





5. LEAKAGE CURRENTS VS. TEMPERATURE

6A. OUTPUT CURRENT VS. SHIELD DISTANCE

6B. OUTPUT CURRENT VS. DISPLACEMENT (ANGULAR & AXIS)

#### H23B1

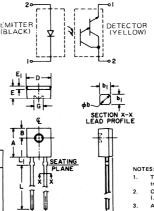
# Matched Emitter-Detector Pair GaAs Infrared Emitting Diode and NPN Photo-Darlington Amplifier

The H23B1 is a matched emitter-detector pair which consists of a gallium arsenide infrared emitting diode and a silicon Darlington-connected phototransistor. The clear epoxy packaging system is designed to optimize the mechanical resolution, coupling efficiency, cost, and reliability. The devices are marked with a color dot for easy identification of the emitter and detector.

### absolute maximum ratings: (25°C)

EMITTER – DETECTOR PAIR					
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum)	T <sub>STG</sub> T <sub>J</sub> T <sub>L</sub>	-55°C to +100°C -55°C to +100°C 260°C			

INFRARED EMITTING DIODE						
Power Dissipation Forward Current (Continuous)	$rac{P_{\mathrm{E}}}{I_{\mathrm{F}}}$	*100 60	mW mA			
Forward Current (Peak) (Pulse Width ≤ 1µs	$I_{\mathbf{F}}$	3	A			
PRR ≤ 300pps) Reverse Voltage	$V_R$	6	v			
*Derate 1.33 mW	*Derate 1.33 mW/°C above 25°C ambient.					



SYM	MET	LI~	INCHES		NOTES
	MIN	MAX	MIN	MAX	
A	5.59	5.80	.220	.228	
В	1.78	NOM.	.070	пом.	2
φb	.60	.75	.024	.030	1
b <sub>1</sub>	.51	NOM.	.020	NOM.	1
D	4.45	4.70	.175	.185	
Ε -	2.41	2.67	.095	.105	
E <sub>1</sub>	.58	.69	.023	.027	
e	2.41	2.67	.095	.105	3
G	1.98	NOM.	.078	NOM.	
L	12.7	-	.500	-	1 1
L <sub>1</sub>	1.40	1.65	.055	.065	
S	.83	.94	.033	.037	3

 Two leads. Lead cross section dimensions uncontrolled within 1.27 MM (.050") of seating plane.
 Centerline of active element located within .25 MM

As measured at the seating plane. Inch dimensions derived from millimeters.

(.010") of true position

1 2						
DARLINGTON CON PHOTOTRANSISTO						
Power Dissipation	$P_{D}$	**150	mW			
Collector Current (Continuous)	$I_{\mathbf{C}}^-$	100	mA			
Collector-Emitter Voltage	$V_{CEO}$	30	, <b>v</b>			
Emitter-Collector Voltage	$V_{ECO}$	7	V			
**Derate 2.0 i	**Derate 2.0 mW/°C above 25°C ambient.					

### individual electrical characteristics (25°C) (See Note 1)

EMITTER	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage $V_{(BR)R}$ $I_R = 10\mu A$	6	-		·V
Forward Voltage $V_{F} I_{F} = 60 \text{ mA}$	-	-	1.7	v
Reverse Current $I_R V_R = 3V$	-		1	μA
Capacitance $C_i V = O, f = 1 MHz$	-	30		pF
	1	1		i

DETECTOR	MIN	TYP.	MAX.	UNITS
Breakdown Voltage	30	_		V
V <sub>(BR) CEO</sub> I <sub>C</sub> = 1 mA Breakdown Voltage	7	_	_	v
$V_{(BR)ECO}$ $I_E = 100 \mu A$ Collector Dark Current	-	_	100	n <b>A</b>
I <sub>CEO</sub> V <sub>CE</sub> = 25 V Capacitance	_	5	8	pF
$C_{ce}$ $V_{CE} = 5V, f = 1 MHz$				

# coupled electrical characteristics (25°C) (See Note 1)

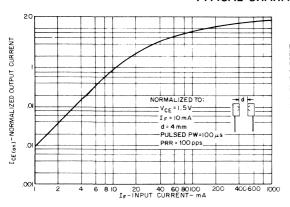
Note: Coupled electrical characteristics are measured at a separation distance of 4mm (.155 inches) with the lenses of the emitter and detector on a common axis within 0.1mm and parallel within 5°.

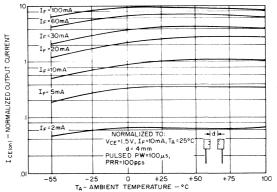
		MIN.	TYP.	MAX.	UNITS
I <sub>CE(on)</sub>	$I_{\rm F} = 10 \text{mA}, V_{\rm CE} = 1.5 \text{V}$	7.5	_	_	mA
V <sub>CE(sat)</sub>	$I_{\rm F} = 10  \text{mA}, I_{\rm C} = 1.8  \text{mA}$			1.0	V
ton	$V_{CC} = 5V$ , $I_F = 10mA$ , $R_L = 750\Omega$	-	45	_	μs
t <sub>off</sub>	$V_{CC} = 5V, I_F = 10mA, R_L = 750\Omega$	-	250	_	μs

Note 1: Stray irradiation can alter values of characteristics. Adequate shielding should be provided.

# 13

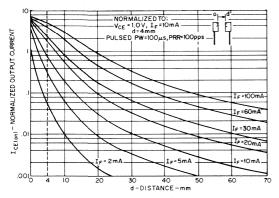
#### TYPICAL CHARACTERISTICS

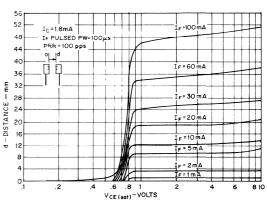




#### 1. OUTPUT CURRENT VS. INPUT CURRENT

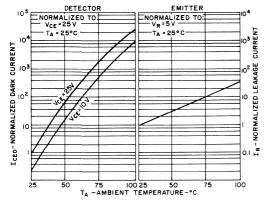
2. OUTPUT CURRENT VS. TEMPERATURE

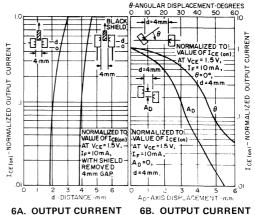




#### 3. OUTPUT CURRENT VS. DISTANCE

4. VCE(sat) VS. DISTANCE





5. LEAKAGE CURRENTS VS. TEMPERATURE

6A. OUTPUT CURRENT VS. SHIELD DISTANCE

6B. OUTPUT CURRENT VS.
DISPLACEMENT (ANGULAR & AXIS)

#### H23L1

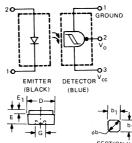
Matched Emitter-Detector Pair GaAs Infrared Emitting Diode and Microprocessor Compatible Schmitt Trigger

The H23L1 is a matched emitter-detector pair which consists of a gallium arsenide, infrared emitting diode and a high-speed integrated circuit detector. The output incorporates a Schmitt trigger which provides hysteresis for noise immunity and pulse shaping. The detector circuit is optimized for simplicity of operation and utilizes an open collector output for maximum application flexibiity. The clear epoxy packaging system is designed to optimize the mechanical resolution, coupling efficiency, cost, and reliability. The devices are marked with a color dot for easy identification of the emitter and detector.

### absolute maximum ratings: (25°C)

EMITTER-DETECTOR PAIR					
Storage Temperature Operating Temperature Lead Soldering Temperature (5 seconds maximum) ≥ 1/16" (1.6 mm) from 0		-55°C to +85°C -55°C to +85°C 260°C			

INFRARED EMITTING DIODE						
Power Dissipation	$P_{\mathbf{E}}$	*100	mW			
Forward Current (Continuous)	$I_{\mathbf{F}}$	60	mA			
Forward Current (Peak) (Pulse Width $\leq 1 \mu s$	$I_{\mathbf{F}}$	3	Α			
PRR ≤ 300 pps) Reverse Voltage	$V_R$	6	v			
*Derate 1.33 mW/	°C above 25°C ambient.					

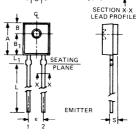


SYM.	MILLIN	ETERS	INC	NOTES	
31M.	MIN.	MAX.	MIN.	MAX.	NUIES
А	5.59	5.80	220	228	
В	1.78	NOM.	.070	NOM.	2
B <sub>1</sub>	3.68	3.94	.145	.155	
φb	.60	.75	024	.030	- 1
b <sub>1</sub>	.51	NOM.	.020	NOM.	1
D	4.45	4.70	.175	.185	
Ε	2.41	2.67	.095	.105	
Εį	.58	69	.023	.027	
e	2.41	2.67	.095	.105	3
e <sub>1</sub>	1.14	1.40	.045	.055	3
G	1.98	NOM.	.078	NOM.	
L	127	-	.500	-	
L1	1.40	1.65	.055	.065	1
R	1.27	NOM.	.050	NOM.	
S	.83	.94	.033	.037	3
т	-	1.65	_	.065	1

#### NOTES:

- Two leads. Lead cross section dimensions uncon trolled within 1.27 MM (.050") of seating plane.
- trolled within 1.27 MM (.050") of seating plane.

  2. Centerline of active element located within .25 MM
- (.010") of true position.
- As measured at the seating plane.
   Inch dimensions derived from millimeters.



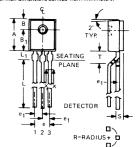


PHOTO DETECTOR			
Power Dissipation	$P_{D}$	**150	mW
Output Current	$I_2$	50	mΑ
Allowed Range	V <sub>cc</sub>	0 to 16	V
Allowed Range	$V_{21}$	0 to 16	V
**Derate 2.0 m	W/°C above 25°C	ambient.	

# individual electrical characteristics (0-70°C)

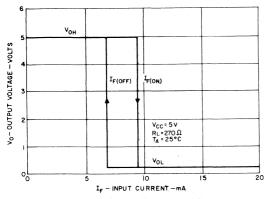
EMITTER		MIN.	TYP.	MAX.	UNITS
Forward Voltage $I_F = 20 \text{ mA}$	$V_{\mathbf{F}}$		1.10	1.50	volts
Reverse Current $(V_R = 3V)$	$I_R$	-		10	micro- ampere
Capacitance $(V = 0, f = 1 \text{ MHz})$	C <sub>J</sub>	-	_	100	pico- farads

$\boxed{ \text{DETECTOR} \left( E_{\text{e}} = 0 \right) }$	MIN.	TYP.	MAX.	UNITS
Operating Voltage Range $V_{CC}$ Supply Current $I_{3(off)}$ $(I_F = 0, V_{CC} = 5V)$ Output Current, High $I_{OH}$	4	1.0	15 5.0 100	volts milli- ampere micro-
$(I_F = 0, V_{cc} = V_o = 15V)$				ampere

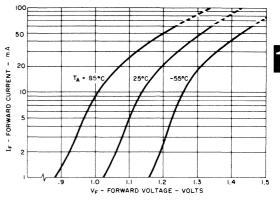
# coupled electrical characteristics (0-70°C)

Note: Coupled electrical characteristics are measured at a separation distance of 4mm (.155 inches) with the lenses of the emitter and detector on a common axis within 0.1mm and parallel within 5°.

	MIN.	TYP.	MAX.	UNITS
Supply Current $I_{3(on)}$ $(I_F = 5 \text{ mA}, V_{CC} = 5V)$	_	1.6	5.0	milliampere
Output Voltage, Low $(R_L = 270\Omega, V_{CC} = 5V)$	-	0.2	0.4	volts
Turn-On Threshold Current $I_{F(on)}$ $(R_L = 270\Omega, V_{CC} = 5V)$		10.0	20.0	milliampere
Turn-Off Threshold Current $I_{F(off)}$ $(R_L = 270\Omega, V_{CC} = 5V)$	1.0	7.5	_	milliampere
Hysteresis Ratio $I_{F(off)}/I_{F(on)}$ $(R_L = 270\Omega, V_{CC} = 5V)$	0.50	0.75	0.90	
Switching Speeds: $(R_L = 270\Omega, V_{CC} = 5V, T_A = 25^{\circ}C$				
Rise Time $t_r$ Fall Time $t_f$	_ _	0.1 0.1	_	μsec. μsec.



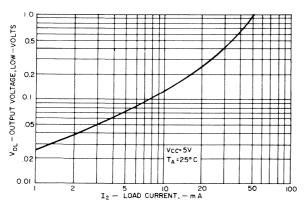
1. TRANSFER CHARACTERISTICS

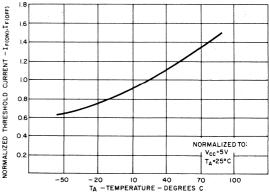


2. FORWARD VOLTAGE VS. FORWARD CURRENT

#### H23L1

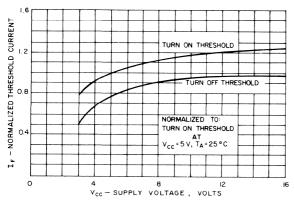
#### TYPICAL CHARACTERISTICS

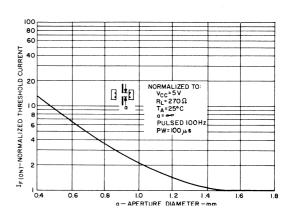




#### 3. ON VOLTAGE VS. LOAD CURRENT

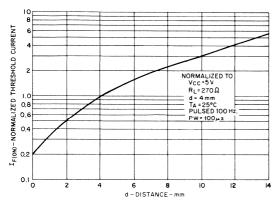
4. THRESHOLD CURRENTS VS. TEMPERATURE

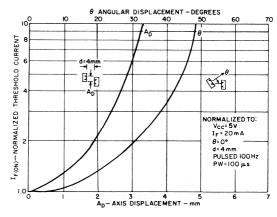




#### 5. THRESHOLD CURRENT VS. SUPPLY VOLTAGE

6. THRESHOLD CURRENT VS. APERTURE DIAMETER

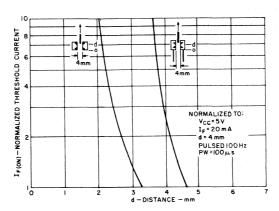




7. THRESHOLD CURRENT VS. DISTANCE

8. THRESHOLD CURRENT VS. DISPLACEMENT (ANGULAR AND AXIS)

#### TYPICAL CHARACTERISTICS



9. THRESHOLD CURRENT VS. SHIELD DISTANCE

# H24A1, H24A2

# **Optoisolator**

# GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The H24A series consists of a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor. The devices are housed in a low-cost plastic package with lead spacing compatible with a dual in-line package.

# absolute maximum ratings: (25°C)

	TOTAL DEVICE		
	Storage Temperature	T <sub>STG</sub>	-55°C to +85°C
	Operating Temperature	$T_{J}$	-55°C to $+85$ °C
i	Lead Soldering Temperature	$T_L$	260°C
į	(5 seconds maximum)		
	Surge Isolation Voltage (Inpu	t to Outp	out).
i	6000V <sub>(peak)</sub>		4242V <sub>(RMS)</sub>
	Steady-State Isolation Voltage	e (Input t	o Output).
	5300V		3750V(DAG)

d			į	φ <sub>b</sub> SECTION X LEAD PRO	b <sub>1</sub>	1 2	° +	D :	D <sup>3</sup>	  4  3	•- E		 +-s1	
SYMBOL	INCI MIN.	HES MAX.	MILL	METERS MAX.	NOTES					Ì		7		Ŧ
A	-	350	_	8.8 9			1			1		1	si	1
Фь	.024	.030	.600	.750	1		1					- 1	31	٨
bı	.020	NOM.	.50	NOM.	1					1		- 1		ī
D	_	375		9.52			l			1				1
e <sub>1</sub>	.285	.315	7.24	8.00			١١١			, ,			SEATING	ŧ
e <sub>2</sub>	.090	.110	2.29	2.79			111		III		1	11	PLANE	F
E	_	.250	_	6.35			17		- 64		Ш	MI.		l
Т	.300	_	7.62		1		lil		III-		1	ii .		Ĺ
R	.050	NOM.	1.27	NOM.			111		1 11	Ť	III	H		1
S	.020	.030	.50	.76			H		x III	x	13	8		l
Sı	.020	.030	.50	.76			۳.		Ψ.		Ψ.	₩		_
				S CONTRO 1E SEATIN			-	e <sub>1</sub>		-	<b>e</b> 2	-		

<sup>1,</sup> FOUR LEADS, LEAD DIMENSIONS CONTROLL BETWEEN .050" (1,27 MM) FROM THE SEATING ... PLANE AND THE END OF THE LEADS.

INFRARED EMITTING DIODE	TER)						
Power Dissipation	PE	*100	mW				
Forward Current	$I_{\mathbf{F}}$	60	mA				
(Continuous)							
Forward Current (Peak)	$I_{\mathbf{F}}$	3	Α				
(Pulse Width $\leq 1 \mu s$							
$PRR \leq 300 \text{ pps}$							
Reverse Voltage	$V_R$	4	V				
*Derate 1.67 mW/°C above 25°C ambient.							

PHOTOTRANSISTOR	(0	(DETECTOR)				
Power Dissipation	$P_{\mathrm{D}}$	**150	mW			
Collector Current (Continuous)	$I_{\mathbb{C}}$	100	mA			
Collector-Emitter Voltage	$V_{\text{CEO}}$	30	V			
Emitter-Collector Voltage	$V_{\text{ECO}}$	6	V			
**Derate 2.5 MW/°C above 25°C ambient.						

# individual electrical characteristics (25°C)

EMITTER	MIN.	TYP.	MAX.	UNITS
Reverse Breakdown Voltage	4	_	_	V
$V_{(BR)R} @ I_R = 10 \mu A$				
Forward Voltage	_	_	1.7	V
$V_F @ I_F = 60 \text{ mA}$				
Reverse Current	_	_	1.0	μΑ
$I_R @ V_R = 3V$				_
Capacitance	-	30	-	pF
$C_i @ V = 0, f = 1 MHz$		l		

-   -	_ V
1	1
-   -	_
5 1	00 nA
3.3	– pF
3	.3

# coupled electrical characteristics (25°C)

	MIN.	TYP.	MAX.	UNITS
CTR – DC Current Transfer Ratio ( $I_F = 10\text{mA}$ , $V_{CE} = 10V$ ) H24A1	100	_		%
H24A2	20	_		%
$V_{CE(sat)}$ - Saturation Voltage - Collector to Emitter ( $I_F = 10mA$ , $I_C = 0.5mA$ )	_	0.1	0.4	V
R <sub>IO</sub> - Isolation Resistance (Input to Output Voltage = 500V <sub>DC</sub> ) †	100	-		$G\Omega$
C <sub>io</sub> - Input to Output Capacitance (Input to Output Voltage = 0,f = 1MHz) †	_	0.5	-	pF
$t_{on}$ - Turn-On Time - ( $V_{CE} = 10V$ , $I_C = 2mA$ , $R_L = 100\Omega$ )	_	9	_	μs
$t_{\text{off}}$ - Turn-Off Time - ( $V_{\text{CE}} = 10V$ , $I_{\text{C}} = 2\text{mA}$ , $R_{\text{L}} = 100\Omega$ )	_	4	_	μs
t <sub>on</sub> - Turn-On Time - $(V_{CC} = 5V, I_F = 10\text{mA}, R_L = 10\text{K}\Omega)$	-	6.5	-	μs
$t_{\text{off}}$ - Turn-Off Time - $(V_{\text{CC}} = 5V, I_{\text{F}} = 10\text{mA}, R_{\text{L}} = 10\text{K}\Omega)$		165		μs

<sup>†</sup> Measured with input diode leads

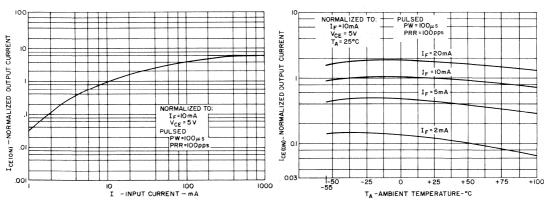
shorted together, and output

detector leads shorted together.

Ru Covered under U.L. component recognition program, reference file E51868

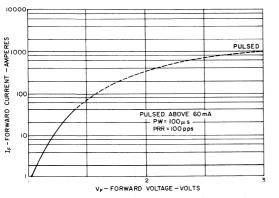
# H24A1, H24A2

#### TYPICAL CHARACTERISTICS

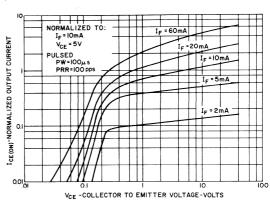


#### 1. OUTPUT CURRENT VS. INPUT CURRENT

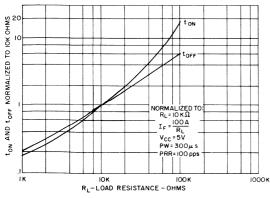
#### 2. OUTPUT CURRENT VS. TEMPERATURE



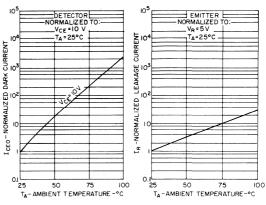




4. OUTPUT CHARACTERISTICS



5. SWITCHING SPEED VS. RL



6. LEAKAGE CURRENTS VS. TEMPERATURE

#### H24B1, H24B2

# **Optoisolator**

# GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier

The H24B series consists of a gallium arsenide, infrared emitting diode coupled with a silicon Darlington-connected phototransistor. The devices are housed in a low-cost plastic package with lead spacing compatible with a dual in-line package.

## absolute maximum ratings: (25°C)

TOTAL DEVICE						
Storage Temperature	T <sub>STG</sub>	-55°C to + 85°C				
Operating Temperature	$T_{J}$	-55°C to + 85°C				
Lead Soldering Temperature	$T_L$	260°C				
(5 seconds maximum)						
Surge Isolation Voltage (Inpu	t to Outp	ut).				
6000V <sub>(peak)</sub>		4242V <sub>(RMS)</sub>				
Steady-State Isolation Voltage	Steady-State Isolation Voltage (Input to Output).					
5300V <sub>(peak)</sub>		$3750V_{(RMS)}$				

INFRARED EMITTING DIODE		(EMIT	TER)
Power Dissipation	PE	*100	mW
Forward Current	$I_{\mathbf{F}}$	60	mA
(Continuous)			
Forward Current (Peak)	$I_{\mathbf{F}}$	3	Α
(Pulse Width $\leq$ 1 $\mu$ s			
PRR ≤ 300 pps)			
Reverse Voltage	$V_R$	4	V
*Derate 1.67 mW/	°C ahove 25°	C ambient.	

NOTE.

1. FOUR LEADS, LEAD DIMENSIONS CONTROLLED
BETWEEN .050" (1.27 MM) FROM THE SEATING
PLANE AND THE END OF THE LEADS.

Power Dissipation	PD	**150	mW
Collector Current (Continuous)	IC	100	mA
Collector-Emitter Voltage	$V_{CEO}$	30	V
Emitter-Collector Voltage	$V_{ECO}$	7	V

#### individual electrical characteristics (25°C)

MIN.	TYP.	MAX.	UNITS
4	_	_	V
-	-	1.7	V
-	-	1.0	μΑ
-	30	-	pF
	V		
			4 1.7 1.0

DETECTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage	30	_	_	V
V <sub>(BR)CEO@</sub> I <sub>C</sub> = 1 mA, I <sub>F</sub> =0 Breakdown Voltage	7		_	v
V <sub>(BR)ECO</sub> @I <sub>E</sub> =100μA, I <sub>F</sub> =0 Collector Dark Current	_	5	100	n <b>A</b>
I <sub>CEO @</sub> V <sub>CE</sub> = 10V, I <sub>F</sub> =0 Capacitance	-	5	-	pF
$C_{ce}@V_{CE}=5V, f=1MHz$				

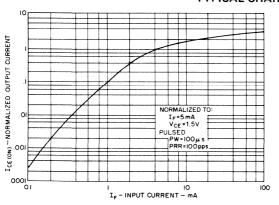
# coupled electrical characteristics (25°C)

			MIN.	TYP.	MAX.	UNITS
CTR	<ul> <li>DC Current Transfer Ratio (I<sub>F</sub> = 5mA, V<sub>CE</sub> = 1.5V)</li> </ul>	H24B1	1000		_	%
		H24B2	400	-	_	%
V <sub>CE</sub> (sa	$_{at)}$ - Saturation Voltage - Collector to Emitter ( $I_F = 5mA$ , $I_C =$		_	0.8	1.0	V
R <sub>IO</sub>	<ul> <li>Isolation Resistance (Input to Output Voltage = 500V<sub>DC</sub>)</li> </ul>	†	100	_	-	GΩ
Cio	<ul> <li>Input to Output Capacitance (Input to Output Voltage = 0</li> </ul>	f = 1MHz	-	0.5	_	pF
ton	- Turn-On Time - $(V_{CE} = 10V, I_C = 10mA, R_L = 100\Omega)$		-	105	_	μs
t <sub>off</sub>	- Turn-Off Time - $(V_{CE} = 10V, I_C = 10mA, R_L = 100\Omega)$		_	60	-	μs
ton	- Turn-On Time - $(V_{CC} = 5V, I_F = 10mA, R_L = 1.0K\Omega)$		_	10	_	μs
t <sub>off</sub>	- Turn-Off Time - $(V_{CC} = 5V, I_F = 10\text{mA}, R_L = 1.0\text{K}\Omega)$		_	700	-	μs

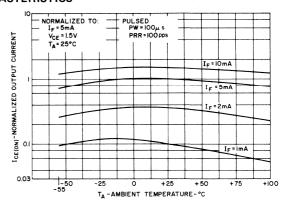
<sup>†</sup>Measured with input diode leads shorted together, and output detector leads shorted together.

<sup>-</sup> Covered under U.L. component recognition program, reference file E51868

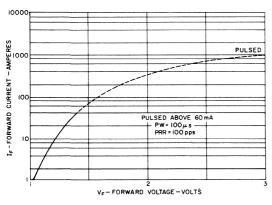
# 13



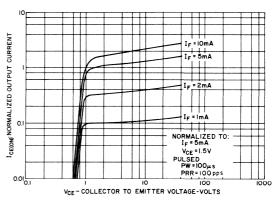
1. OUTPUT CURRENT VS. INPUT CURRENT



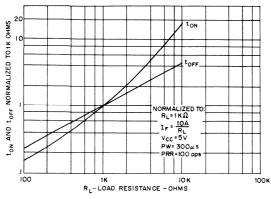
2. OUTPUT CURRENT VS. TEMPERATURE



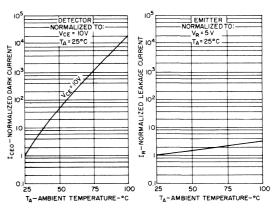
3. INPUT CHARACTERISTICS



4. OUTPUT CHARACTERISTICS



5. SWITCHING SPEED VS. RL



6. LEAKAGE CURRENTS VS. TEMPERATURE

### **BPW36, BPW37**

# Light Detector Planar Silicon Phototransistor

The BPW36 and BPW37 are highly sensitive NPN planar silicon phototransistors. They are housed in a TO-18 style hermetically sealed package with lens cap. These devices are ideal for use in optoelectronic sensing applications where both high sensitivity and fast switching speed are important parameters. Generally only the collector and emitter leads are used; a base lead is provided, however, to control sensitivity and gain of the device.

#### absolute maximum ratings: (25°C unless otherwise specified)

Voltages — Dark Characteristics			
Collector to Emitter Voltage	$V_{CEO}$	45	volts
Collector to Base Voltage	$V_{CBO}$	45	volts
Emitter to Base Voltage	$V_{EBO}$	5	volts
Currents			
Light Current	$I_L$	50	mA
Dissipations			
Power Dissipation $(T_A = 25^{\circ}C)^*$	$\mathbf{P_T}$	300	mW
Power Dissipation $(T_C = 25^{\circ}C)^{**}$	$\mathbf{P_T}$	600	mW
Temperatures			
Junction Temperature	$T_{ m J}$	+150	°C
Storage Temperature	$T_{STG}$	-65 to +150	°C

<sup>\*</sup>Derate 2.4 mW/°C above 25°C ambient

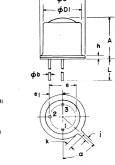
#### electrical characteristics: (25°C unless otherwise specified)

STATIC CHARACTERISTICS	. (23 C unless of	BPW36 MIN. M	) 	BPW37 IIN.
Light Current				
$(V_{CE} = 5V, Ee^{\dagger} = 10mW/cm^2)$	$I_L$	6	:	3 mA
Dark Current				
$(V_{CE} = 10V, Ee = 0)$	$I_{D}$	10	00	n <b>A</b>
Emitter-Base Breakdown Voltage $(I_E = 100\mu A, I_C = 0, Ee = 0)$	$V_{(BR)E}$	во 5		5 V
Collector-Base Breakdown Voltage ( $I_C = 100\mu A, I_E = 0, Ee = 0$ )	$V_{(BR)C}$	BO 45	45	5 <b>V</b>
Collector-Emitter Breakdown Voltage $(I_C = 10 mA, Ee = 0)$	$V_{(BR)C}$	EO 45	45	5 V
Saturation Voltage $(I_C = 10mA, I_B = 1mA)$	V <sub>CE (SA</sub>	T) 0.	4	V
Turn-On Time ( $V_{CE} = 10V$ , $I_C = 2mA$ ,	t <sub>on</sub>	8		μsec
Turn-Off Time ( $R_L = 100\Omega$ )	t <sub>off</sub>	7		μsec

<sup>\*</sup>Ee = Radiation Flux Density. Radiation source is an unfiltered tungsten filament bulb at 2870°K color temperature.

NOTE: A GaAs source of 3.0 mW/cm² is approximately equivalent to a tungsten source, at 2870°K, of 10 mW/cm².





SYMBOL		HES	MILLIN	METERS	NOTE
JIMOOL	MIN.	MAX.	MIN.	MAX.	IVOIL
Α	.225	.255	5.71	6,47	
φь	.016	.021	407	533	
φD	.209	.230	5.31	5.84	
ΦD1	.178	.195	4.52	4.96	
e	.100	NOM	2.54	NOM	2
e <sub>1</sub>	.050	NOM	1.27	NOM	2
h	-	.030	_	.76	
	-036	.046	.92	1.16	
k	.028	.048	.71	1.22	1
L	.500	_	12.7	_	
a	45°	45°	45°	45°	3

NOTES

From centerline tab.

<sup>\*\*</sup>Derate 4.8 mW/°C above 25°C case

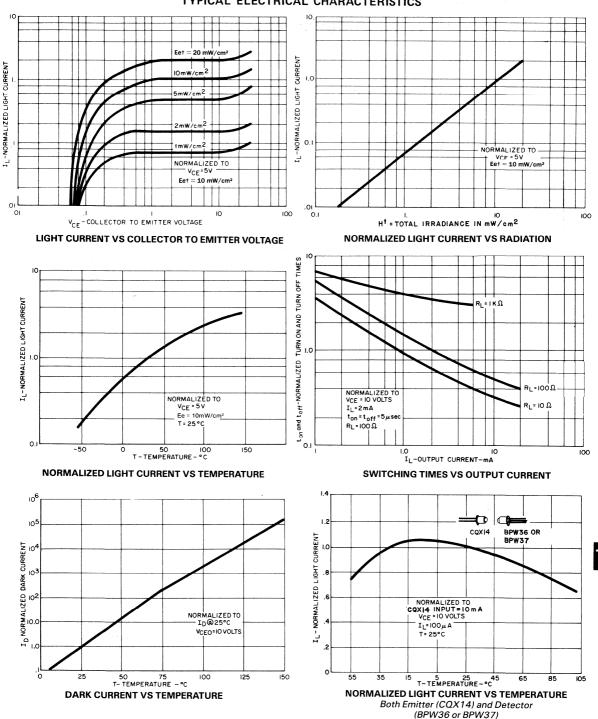
NOTES

1. Measured from maximum diameter of device.

2. Leads having maximum diameter: O21"
(533mm) measured in gauging plane. O54"
+001"-000(137+025-000mm) below
the reference plane of the device shall be
within.007"(778mm) their true position
relative to maximum width tab.

# **BPW36, BPW37**

#### TYPICAL ELECTRICAL CHARACTERISTICS



at Same Temperature

#### **BPW38**

# **Light Detector Planar Silicon Photo-Darlington Amplifier**

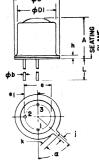
The BPW38 is a supersensitive NPN planar silicon photo-Darlington amplifier. For many applications, only the collector and emitter leads are used; however, a base lead is provided to control sensitivity and the gain of the device. The BPW38 is a TO-18 style hermetically sealed package with lens cap and is designed to be used in optoelectronic sensing applications requiring very high sensitivity.

### absolute maximum ratings: (25°C unless otherwise specified)

<b>VOLTAGES – DARK CHARACTERIS</b>	STICS			
Collector to Emitter Voltage	$V_{CEO}$	25	volts	
Collector to Base Voltage	$V_{CBO}$	25	volts	
Emitter to Base Voltage	$V_{EBO}$	12	volts	
CURRENTS				
Light Current	$I_L$	200	mA	
DISSIPATIONS				
Power Dissipation $(T_A = 25^{\circ}C)^*$	$P_{T}$	300	mW	
Power Dissipation $(T_C = 25^{\circ}C)^{**}$	$P_{T}$	600	mW	
TEMPERATURES				
Junction Temperature	$T_J$	150	°C	
Storage Temperature	$T_{STG}$	-65 to 150	°C	
*Derate 2.4 mW/°C above 25°C ambient.				

#### electrical characteristics: 05°C unless otherwise specified)

electrical characteristics. (25°C	unless otherwise specified)				
STATIC CHARACTERISTICS		MIN.	MAX	•	
LIGHT CURRENT $(V_{CE} = 5V, Ee^{\dagger} = 0.2 \text{ mW/cm}^2)$	$I_{\mathbf{L}}$	3	_	mA	
DARK CURRENT					
$(V_{CE} = 12V, I_B = 0)$	$I_{\mathbf{D}}$	_	100	nΑ	
EMITTER-BASE BREAKDOWN VOLTAGE $(I_E=100\mu A)$	$V_{(BR)EBO}$	12	_	V	
COLLECTOR-BASE BREAKDOWN VOLTAGE ( $I_C = 100 \mu A)$	V <sub>(BR)CBO</sub>	25	_	V	
COLLECTOR-EMITTER BREAKDOWN VOLTAGE (I <sub>C</sub> = 10mA)	V <sub>(BR)CEO</sub>	25		v	
SWITCHING CHARACTERISTICS (see Switching Circuit)	(BK)CEO				
SWITCHING SPEEDS $(V_{CC} = 10V, I_L = 10 \text{ mA}, R_L = 100\Omega)$					
DELAY TIME	td	-	50	μsec	
RISE TIME	tr	_	300	μsec	
STORAGE TIME	$t_{S}$	_	10	μsec	
FALL TIME	tf		250	μsec	



SYMBOL	INC	HES	MILLIN	ETERS	NOTE
3 I MIDUL		MAX.	MIN.	MAA.	14012
A	.225	.255	5.71	6.47	
φь	.016	.021	407	533	
φD	.209	.230	5.31	5.84	
ΦDı	.178	.195	4.52	4.96	
e	.100		2.54	NOM	2
e,	.050	NOM	1.27	NOM	2
h	_	.030	_	.76	
-	.036	.046	.92	1.16	
k	.028	.048	.71	1.22	1 1
	.500	-	12.7	-	
a	45°	45°	45°	45°	3

NOTE: The 2870°K radiation is 25% effective on the photodarlington; i.e., a GaAs source of 0.05 mW/cm<sup>2</sup> is equivalent to this 0.2 mW/cm<sup>2</sup> tungsten source.

<sup>\*\*</sup>Derate 4.8 mW/°C above 25°C case.

NOTES.

1. Measured from maximum diameter of device.

2. Leads having maximum diameter. O21"

(.533 mm) measured in gauging plane.054"

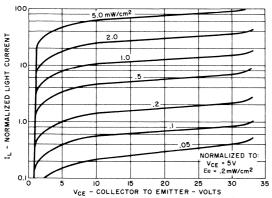
+.00!" -.000(137 +.025 -.000mm) below the reference plane of the device shall be within .007"(.778mm) their true position relative to maximum width tab.

<sup>3.</sup> From centerline tab.

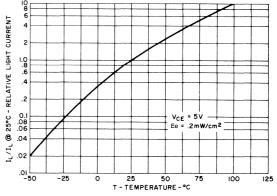
<sup>†</sup>Ee = Radiation Flux Density, Radiation source is an unfiltered tungsten filament bulb at 2870° K color temperature.

# 14

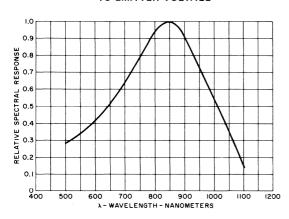
#### TYPICAL ELECTRICAL CHARACTERISTICS



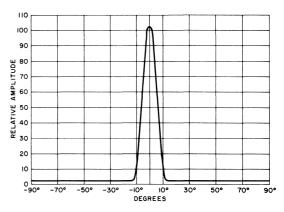
LIGHT CURRENT VS. COLLECTOR
 TO EMITTER VOLTAGE



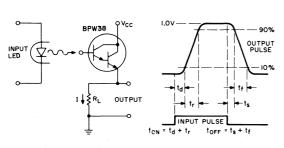
2. RELATIVE LIGHT CURRENT VS.
AMBIENT TEMPERATURE



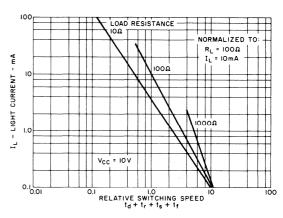
3. SPECTRAL RESPONSE CURVE



4. ANGULAR RESPONSE



5. TEST CIRCUIT AND VOLTAGE WAVEFORMS



6. LIGHT CURRENT VS. RELATIVE SWITCHING SPEED

### **CQX14, CQX15, CQX16, CQX17**

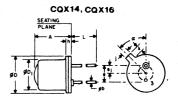
# Infrared Emitter GaAs Infrared Emitting Diode

The CQX14, CQX15, CQX16, CQX17 series are gallium arsenide, light emitting diodes which emit non-coherent, infrared energy with a peak wave length of 940 nanometers. They are ideally suited for use with silicon detectors and are mounted in a TO-18 style hermetically sealed package. The CQX14 and CQX16 have a lens which provides a narrow beam angle. The CQX15 and CQX17 have a flat window for a wide beam angle which is useful with external lensing.

#### absolute maximum ratings: (25°C unless otherwise specified)

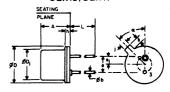
Voltage:			
Reverse Voltage	$V_R$	3	volts
Currents:			
Forward Current Continuous	$I_F$	100	mA
Forward Current (pw 1 µs, 200 Hz)	$ m I_{F}$	10	Α
Dissipations:			
Power Dissipation $(T_A = 25^{\circ}C)^*$	$\mathbf{P_{T}}$	170	mW
Power Dissipation $(T_C = 25^{\circ}C)^{**}$	$P_{T}$	1.3	W
Temperatures:			
Junction Temperature	$T_{J}$	-65°C t	o +150°C
Storage Temperature	$T_{stg}$	-65°C t	o +150°C
Lead Soldering Time	10 seconds at 260°C		
*D 1 26			

<sup>\*</sup>Derate 1.36 mW/°C above 25°C ambient.



SYMBOL		INCHES		MILLIMETERS		
31111000	MIN.	MAX.	MIN.	MAX.	NOTES	
Α		255		6.47		
<b>p</b>	.016	021	.407	.533		
60	.209	230	5.31	5.84	1	
øD₁	.180	.187	4.57	4.77	l	
•	IOONOM		2.54	2		
•1	.05	O NOM.	1.27 NOM.		2	
n		.030		.76		
)	.031	.044	.79	1.1.1		
k	036	.046	,92	1.16	1	
ιl	1.00		25.4	1		
ا م	45*			45*	3	

**CQX15, CQX17** 



SYMBOL	MIN			MILLIMETERS	
A		155		3.93	NOTES
46	.016	.021	.407	-533	
#0	209	.230	5,31	5,84	
øD,	.180	.187	4,57	4.77	
.	. IOONOM.		2.54	2	
	05	ONOM.	1.27	NOM	2
h		.030		.76	
j	.031	.044	.79	1.11	
k I	.036	.046	.79 .92	1.16	1
L	1.00		25.4		
a 1	4	45*		5.	3



- Measured from maximum diameter of device.
- Leads having max. diameter .021" (.533rmm) measured in gaging plane .054" + .001" - .000 (137 + 025 -000mm) below the reference plane of the device shall be within .007" (.778mm) their true position relative to a maximum width tab.
- 3 From centerline tab

electrical characteristics: (25°C unless otherwise specified)

		MIN.	TYP.	MAX.	UNITS
Reverse Leakage Current					
$(V_R = 3V)$	$I_R$			10	$\mu$ A
Forward Voltage					
$(I_F = 100mA)$	$V_{\mathrm{F}}$		1.4	1.7	V

#### optical characteristics: (25°C unless otherwise specified)

Total Power Output (note 1)

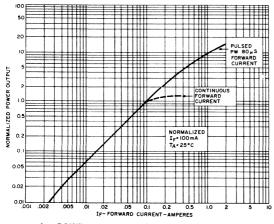
 $(I_F = 100 \text{mA})$ CQX14-CQX15 Po mW CQX16-CQX17 mW Peak Emission Wavelength 940  $(I_F = 100 \text{mA})$ nm Spectral Shift with Temperature .28 nm/°C Spectral Bandwidth 50% nm Rise Time 0-90% of Output 1.0 μs Fall Time 100-10% of Output ШS

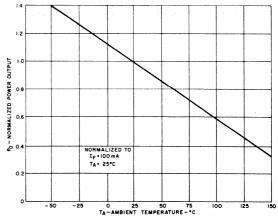
Note 1: Total power output,  $P_{O}$ , is the total power radiated by the device into a solid angle of 2  $\pi$  steradians.

<sup>\*\*</sup>Derate 10.4 mW/°C above 25°C case.

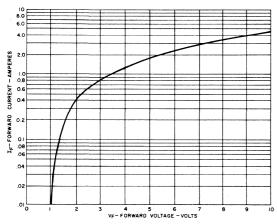




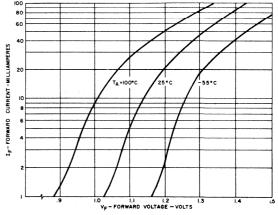




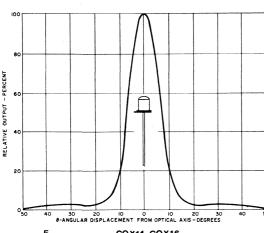
#### 1. POWER OUTPUT VS. INPUT CURRENT



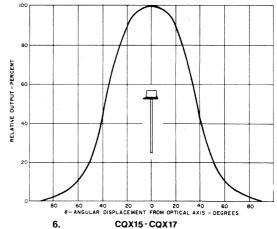
2. POWER OUTPUT VS. TEMPERATURE



#### 3. FORWARD VOLTAGE VS. FORWARD CURRENT



4. FORWARD VOLTAGE VS. FORWARD CURRENT



5. CQX14-CQX16
TYPICAL RADIATION PATTERN

CQX15-CQX17
TYPICAL RADIATION PATTERN

#### CQY80

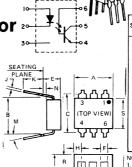
# Optoisolator GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The CQY80 is a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. This device is also available in surface-mount packaging.

#### absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE			
Power Dissipation	*100	milliwatts	
Forward Current (Continuous)	60	milliamps	
Forward Current (Peak) (Pulse width 1 µsec 300 P Ps)	3	ampere	
Reverse Voltage	5	volts	
*Derate 1.33 mW/°C above 2	5°C ambient	t.	

PHOTO-TRANSISTOR		
Power Dissipation	**150	milliwatts
$V_{CEO}$	32	volts
V <sub>CBO</sub>	70	volts
$V_{ECO}$	5	volts
Collector Current (Continuous)	100	milliamps
**Derate 2.0 mW/°C above 2	25°C ambien	ıt.



MIN.				NOTES
WITE.	MAX.	MIN.	MAX.	
8.38	8.89	.330	.350	
7.62	REF.	.300	REF.	1
	8.64	- 1	.340	2
.406	.508	.016	.020	
-	5.08	-	.200	3
1.01	1.78	.040	.070	
2.28	2.80	.090	.110	
- 1	2.16	-	.085	4
	.305		.012	
2.54	-	.100	-	
- "	15"		15	
.381	-	.015	-	
-	9.53	-	.375	
2.92	3.43	.115	.135	
6.10	6.86	.240	.270	
	7.62 -406 -1.01 2.28 - .203 2.54 - .381 -	7.62 REF.  -   8.64   .406   .508   .01   1.78   2.28   2.80   -   2.16   .203   .305   2.54   -   15   .381   -   9.53   2.92   3.43	8.38 8.89 .330 7.62 REF300 - 8.64 -4.06 .508 .016 - 5.08 -1.01 1.78 .040 2.28 2.80 .090 - 2.16 -203 .305 .008 2.54 - 1.100 - 15015 - 9.53 - 292 3.43 1.115	8.38 8.89 .330 .350 7.62 REF300 REF340 4.06 .508 .016 .020 - 5.08200 1.01 1.78 .040 .070 2.28 2.80 .090 .110 - 2.16085 .203 .305 .008 .012 2.54100 - 15 .53375 - 9.53375 - 9.53335

- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.

MILLIMETERS

- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES.

#### TOTAL DEVICE

Storage Temperature -55°C to +150°C

Operating Temperature -55°C to +100°C

Lead Soldering Time (at 260°C) 10 seconds

Surge Isolation Voltage (Input to Output)

 $4000\,\mathrm{V_{RMS}}$ 

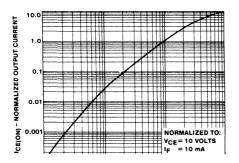
# individual electrical characteristics:(25°C)

1	INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
	Forward Voltage $V_F$ $(I_F = 10 \text{ mA})$	1.1	1.5	volts
	Reverse Current $I_R$ $(V_R = 3 V)$	-	10	microamps
	Capacitance $C_J$ (V = O,f = 1 MHz)	50	_	picofarads

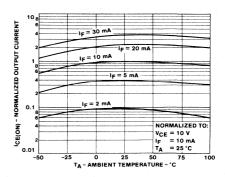
	PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
	Breakdown Voltage - V <sub>(BR)CEO</sub>	32	-	-	volts
١	$(I_C = 10 \text{mA}, I_F = 0)$				
١	Breakdown Voltage $-V_{(BR)CBO}$	70	-	-	volts
1	$(I_C = 100 \mu\text{A}, I_F = 0)$				
1	Breakdown Voltage – V <sub>(BR)ECO</sub>	5	-	-	volts
1	$(I_E = 100 \mu\text{A}, I_F = 0)$		_		
1	Collector Dark Current - I <sub>CEO</sub>	-	5	100	nanoamps
1	$(V_{CE} = 10 \text{ V}, I_{F} = 0)$		_		
1	Capacitance		2	-	picofarads
1	$(V_{CE} = 10 \text{ V}, f = 1 \text{ MHz})$				

# coupled electrical characteristics:(25°C)

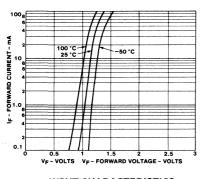
0.1	0.4	%
0.1	104	114
	J 0.7	volts
_	_	gigaohms
_	2	picofarads
2	_	microseconds
	_ _ 2	$\begin{bmatrix} - & - \\ 2 & - \end{bmatrix}$



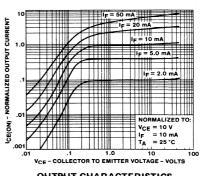
**OUTPUT CURRENT VS. INPUT CURRENT** 



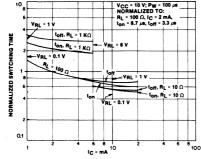
**OUTPUT CURRENT VS. TEMPERATURE** 



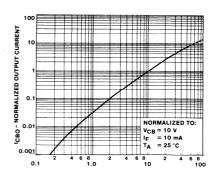
INPUT CHARACTERISTICS



**OUTPUT CHARACTERISTICS** 



**SWITCHING SPEED VS. COLLECTOR CURRENT** (NOT SATURATED)



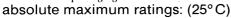
OUTPUT CURRENT (ICBO) VS. INPUT CURRENT

### **CNX35, CNX36**

# **Optoisolator**

# **GaAs Infrared Emitting Diode and NPN Silicon Phototransistor**

The CNX35 and CNX36 are gallium arsenide, infrared emitting diodes coupled with a silicon phototransistor in a dual in-line package. These devices are also available in surface-mount packaging.



INFRARED EMITTING DIODE					
Power Dissipation	*150	milliwatts			
Forward Current (Continuous)	100	milliamps			
Forward Current (Peak) (Pulse width 1 µsec 300 P Ps)	3	ampere			
Reverse Voltage *Derate 1.33mW/°C above 25°C ambient.	3	volts			

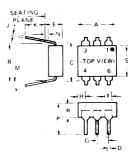
PHOTO-TRANSISTOR					
Power Dissipation	**150	milliwatts			
V <sub>CEO</sub>	30	volts			
V <sub>CBO</sub>	70	volts			
V <sub>ECO</sub>	7	volts			
Collector Current (Continuous)	100	milliamps			
**Derate 2.0 mW/°C above 25°C ambie	nt.	•			

# Individual electrical characteristics (25°C)

INFRARED EMITTI	TYP.	MAX.	UNITS	
Forward Voltage (I <sub>F</sub> = 10 mA)	V <sub>F</sub>	1.1	1.5	volts
Reverse Current (V <sub>R</sub> = 3 V)	$I_R$		10	microamps
Capacitance V <sub>B</sub> = O, f = 1 MHz	$C_{J}$	50		picofarads

TOTAL DEVICE	
Storage Temperature –55°C to 150°C	
Operating Temperature -55 to 100°C	
Lead Soldering Time (at 260°C) 10 seconds	
Surge Isolation Voltage (Input to Output) 5656 V <sub>(peak)</sub> 4000 V <sub>(RMS)</sub>	
Steady-State Isolation Voltage (Input to Output). 5300 $V_{(peak)}$ 3750 $V_{(RMS)}$	





	MILLIMETERS		INCHES		
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Λ	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
C		8.64	1	.340	2
D	.406	.508	0.16	.020	1
E		5.08		.200	3
F	1.01	1.78	.040	.070	1
G	2.28	2.80	.090	.110	i
н		2.16	1	.085	4
J	.203	.305	.008	.012	1
к	2.54		.100		1
M		15*		15*	1
N ·	.381		.015		1
P		9.53		.375	1
R	2.92	3.43	.115	.135	1
s	6.10	6.86	.240	.270	1

NOTES

1. INSTALLED POSITION LEAD CENTERS.
2. OVERALL INSTALLED DIMENSION.
3. THESE MEASUREMENTS ARE MADE FROM THE SEATING

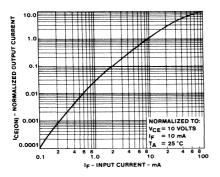
PLANE. 4. FOUR PLACES.

PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - $V_{(BR)CEO}$ ( $I_C = 10 \text{ mA}, I_F = O$ )	30	and the same		volts
Breakdown Voltage - $V_{(BR)CBO}$ ( $I_C = 100 \mu A, I_F = O$ )	70			volts
Breakdown Voltage - $V_{(BR)EBO}$ ( $I_E = 100 \mu A, I_E = O$ )	7		_	volts
Collector Dark Current - I <sub>CEO</sub> (V <sub>CE</sub> = 10 V, I <sub>F</sub> = O)		5	50	nano- amps
Collector-Base Dark Current - $I_{CBO}$ ( $V_{CB} = 10 \text{ V}, I_F = O$ )			20	nano- amps
Capacitance $(V_{CE} = 10 \text{ V}, f = 1 \text{MHz})$		2		pico- farads

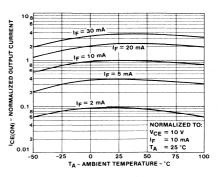
# coupled electrical characteristics: (25°C)

		MIN.	TYP.	MAX.	UNITS
D.C. Current Transfer Ratio - $(I_F = 10 \text{ mA}, V_{CF} = 0.4 \text{ V})$	CNX35 CNX36	40 80		160	% %
$I_{CFT}$ (<70° C, $I_F$ = 2 mA, $V_{CF}$ = 0.4 V)	CNX35, CNX36	150			μΑ
$I_{CF2}$ (<70°C, $V_F = 0.8 \text{ V}$ , $V_{CF} = 15 \text{ V}$ )	CNX35, CNX36	N 1		15	μΑ
Saturation Voltage — Collector Emitter ( $I_F = 10 \text{ mA}$ , $I_C = 4 \text{ mA}$ )			0.1	0.4	volts
Isolation Resistance (Input to Output Voltage = 500 V DC)		100	maga		gigaohms
Input to Output Capacitance (Input to Output Voltage = O, f = 1 MHz	<b>(</b> )		halisani	2	picofarads
Switching Speeds		1 1 1 L	ŀ		N. 7. 1. 1.
Rise/Fall Time ( $V_{CF} = 10 \text{ V}$ , $I_{CE} = 2 \text{ mA}$ , $R_L = 100$ )			2	1 dices	microseconds
Rise/Fall Time ( $V_{CB} = 10 \text{ V}$ , $I_{CB} = 50 \mu\text{A}$ , $R_1 = 100$ )			300		nanoseconds

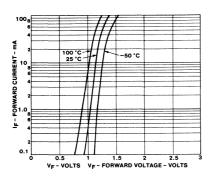
# 14



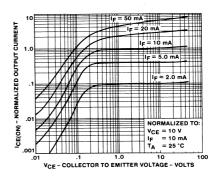
1. OUTPUT CURRENT VS INPUT CURRENT



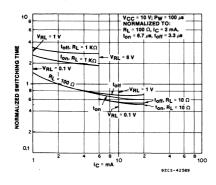
2. OUTPUT CURRENT VS TEMPERATURE



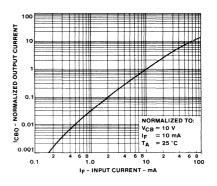
3. INPUT CHARACTERISTICS



4. OUTPUT CHARACTERISTICS



5. SWITCHING SPEED VS COLLECTOR CURRENT (NOT SATURATED)



6. OUTPUT CURRENT (ICBO) VS INPUT CURRENT

#### **CNY17**

# **Optoisolator**

# GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

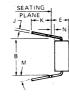
absolute maximum ratings: (25°C) (unless otherwise specified)

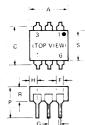
The CNY17 consists of a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. This device is also available in surface-mount packaging.

#### **FEATURES:**

- · Fast switching speeds
- High DC current transfer ratio
- · High isolation resistance
- High isolation voltage
- I/O compatible with integrated circuits







SYMBOL	MILLIN	ETERS	INC	NOTES	
STIVIBUL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	8.38	8.89	.330	.350	
В	7.62 REF.		.300	REF.	1
C		8.64		.340	2
D	:406	.508	.016	.020	1
E		5.08		.200	3
F	1.01	1.78	.040	.070	1
G	2.28	2.80	.090	.110	l
H.		2.16		.085	4
J	.203	.305	.008	.012	l
K	2.54		.100		
M		15		15	l
N	.381		.015		l
Р	1.0	9.53		.375	l

#### NOTES

- 1. INSTALLED POSITION LEAD CENTERS
- 2. OVERALL INSTALLED DIMENSION.
- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES.

INFRARED EMITTING DIODE		
Power Dissipation - T <sub>A</sub>	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width $1\mu$ s, 300 P Ps)		
Reverse Voltage	3	volts
*Derate 1.33 mW/°C at	bove 25°C	

PHOTO-TRANSISTOR		
Power Dissipation – T <sub>A</sub>	**150	milliwatts
$V_{ m CEO}$	70	volts
$V_{CBO}$	70	volts
$V_{ECO}$	7	volts
Collector Current (Continuous	150	milliamps
**Derate 2.0 mW/°C a	above 25°C	

#### TOTAL DEVICE

Storage Temperature -55 to 150°C
Operating Temperature -55 to 100°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output).

5000V<sub>(peak)</sub> 3000V<sub>(RMS)</sub>
Steady-State Isolation Voltage (Input to Output).

4000V<sub>(peak)</sub> 2830V<sub>(RMS)</sub>



VDE approved to 0883/6.80 0110/11.72



# individual electrical characteristics (25°C) (unless otherwise specified)

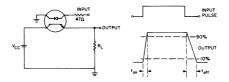
INFRARED EMITTING DIODE	MIN.	MAX.	UNITS
Forward Voltage - V <sub>F</sub> (I <sub>F</sub> = 60 mA)	.8	1.65	volts
Reverse Current $-I_R$ $(V_R = 3V)$		10	microamps
Capacitance $-C_J$ (V = O, f = 1  MHz)		100	picofarads

PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - V <sub>(BR)CEO</sub>	70	-	_	volts
$(I_C = 10mA, I_F = 0)$				
Breakdown Voltage – V <sub>(BR)CBO</sub>	70	-	-	volts
$(I_C = 100\mu A, I_F = O)$ Breakdown Voltage $-V_{(BR)ECO}$	7			volts
$(I_F = 100\mu A, I_F = 0)$	′ .			TORES
Collector Dark Current - ICEO	_	5	50	nanoamps
$(V_{CE} = 10V, I_F = 0)$				
Capacitance – C <sub>CE</sub>	-	2	-	picofarads
$(V_{CE} = 10V, f = 1MHz)$		ļ		
Current Transfer Ratio —h <sub>FE</sub>	100			
$(V_{CE} = 5V, I_C = 100\mu A)$	100			

# coupled electrical characteristics (25°C) (unless otherwise specified)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_E = 10$ mA, $V_{CE} = 5$ V) CNY17 I	40	_	80	%
CNY17 II	63	-	125	%
CNY17 III	100		200	%
CNY17 IV	160	-	320	%
Saturation Voltage – Collector to Emitter (I <sub>F</sub> = 10mA, I <sub>C</sub> = 2.5mA)		_	0.3	volts
Isolation Resistance ( $V_{IO} = 500V_{DC}$ ) (See Note 1)	100			gigaohms
Input to Output Capacitance ( $V_{IO} = O,f = 1 \text{ MHz}$ ) (See Note 1)			2	picofarads
Turn-On Time $-t_{on}$ ( $V_{CC} = 10V$ , $I_{C} = 2mA$ , $R_{L} = 100\Omega$ ) (See Figure 1)	-	5	10	microseconds
Turn-Off Time $-t_{off}$ ( $V_{CC} = 10V$ , $I_C = 2mA$ , $R_L = 100\Omega$ ) (See Figure 1)		5	10	microseconds

Note 1: Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together.

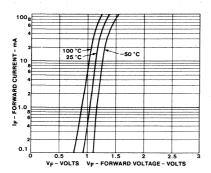


Adjust Amplitude of Input Pulse for Output (I<sub>C</sub>) of 2 mA

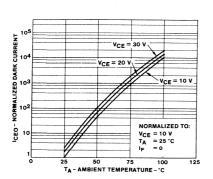
TEST CIRCUIT AND VOLTAGE WAVEFORMS

#### **CNY17**

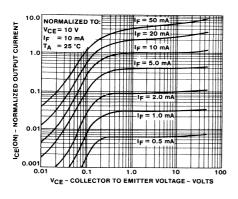
#### TYPICAL CHARACTERISTICS



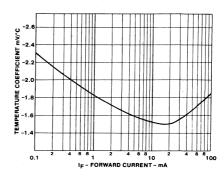
#### 1. INPUT CHARACTERISTICS



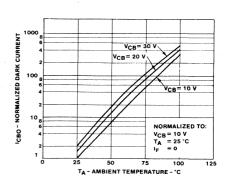
3. DARK ICEO CURRENT VS TEMPERATURE



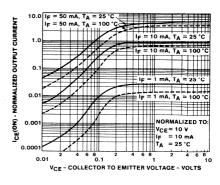
5. OUTPUT CHARACTERISTICS



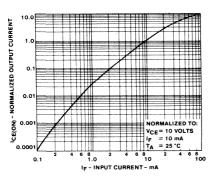
2. FORWARD VOLTAGE TEMPERATURE COEFFICIENT



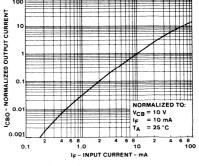
4. ICBO VS TEMPERATURE



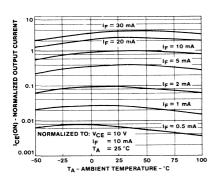
6. OUTPUT CHARACTERISTICS



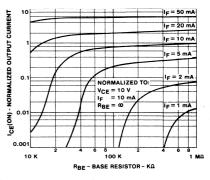
7. OUTPUT CURRENT VS INPUT CURRENT



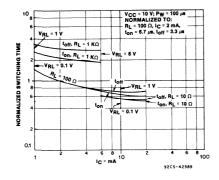
8. OUTPUT CURRENT — COLLECTOR TO BASE VS INPUT CURRENT



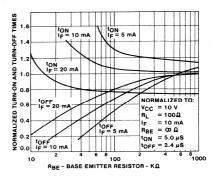
9. OUTPUT CURRENT VS TEMPERATURE



10. OUTPUT CURRENT VS BASE EMITTER RESISTANCE



11. SWITCHING TIMES VS OUTPUT CURRENT



12. SWITCHING TIME VS RBE

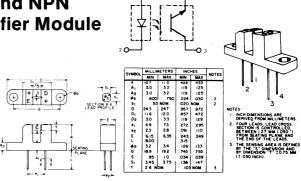
#### CNY28

# Optointerrupter Module GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier Module

The CNY28 is a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a plastic housing. The gap in the housing provides a means of interrupting the signal with tape, cards, shaft encoders, or other opaque material, switching the output transistor from an "ON" into an "OFF" state.

#### **FEATURES:**

- Low cost, plastic module
- Non-contact switching
- Fast switching speeds
- · Solid state reliability
- I/O compatible with integrated circuits



# absolute maximum ratings: (25°C) (unless otherwise specified)

Storage and Operating Temperature -55° to 85°C. Lead Soldering Time (at 260°C) 10 seconds.

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (peak, 100µs, 1% duty cycle)	1	amp
Reverse Voltage	3	volts
*Derate 1.67mW/°C above 25°C	ambient	

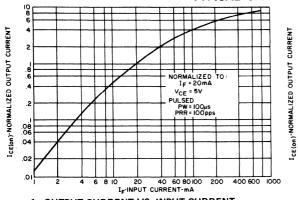
Power Dissipation	**150	milliwatt
Collector Current (Continuous)	100	milliamps
V <sub>CEO</sub>	30	volts
VECO	5	volts

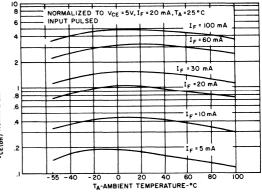
# individual electrical characteristics (25°C)

INFRARED EMITTING	DIODE	TYP.	MAX.	UNITS	PHOTO-TRANSISTOR	MIN.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> = 10 mA)	$V_{\mathrm{F}}$	1.2	1.7	volts	Breakdown Voltage V(BR)CEO (I <sub>C</sub> = 10 mA)	30	-	volts
Reverse Current $(V_R = 2V)$	I <sub>R</sub>	-	10	<i>µ</i> amps	Breakdown Voltage V(BR)ECO (I <sub>E</sub> = 100μA)	5	–	volts
Capacitance (V = O, f = 1 Mhz)	$C_{J}$	150	_	pf	Collector Dark Current $I_{CEO} (V_{CE} = 10V, I_F = O, H=O)$	-	100	nA.

## coupled electrical characteristics (25°C)

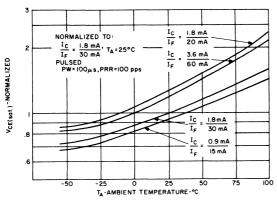
	MIN.	TYP.	MAX.	UNITS
Output Current ( $I_F = 20\text{mA}$ , $V_{CE} = 10\text{V}$ ) Saturation Voltage ( $I_F = 20\text{mA}$ , $I_C = 25\mu\text{A}$ ) Switching Speeds ( $V_{CE} = 5\text{V}$ , $I_F = 30\text{mA}$ , $R_L = 2.5\Omega$ )	200	400 0.2	_ 0.4	μamps volts
On Time $(t_d + t_T)$ Off Time $(t_s + t_f)$	= - ,	5 5		μsec μsec

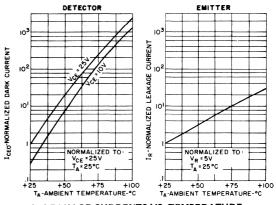




1. OUTPUT CURRENT VS. INPUT CURRENT

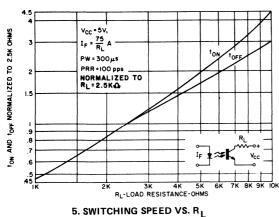
2. OUTPUT CURRENT VS. TEMPERATURE

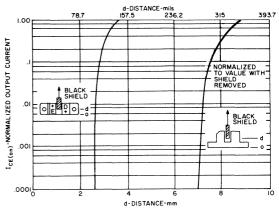




3.  $V_{CE(sat)}$  VS. TEMPERATURE

4. LEAKAGE CURRENTS VS. TEMPERATURE





6. OUTPUT CURRENT VS. DISTANCE

#### **CNY29**

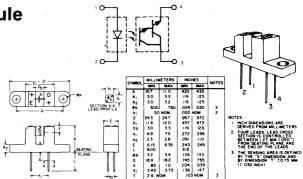
# **Optointerrupter**

GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier Module

The CNY29 is a gallium arsenide, infrared emitting diode coupled with a silicon photo-Darlington in a plastic housing. The gap in the housing provides a means of interrupting the signal with tape, cards, shaft encoders, or other opaque material, switching the output transistor from an "ON" into an "OFF" state.

#### **FEATURES:**

- Low cost, plastic module
- Non-contact switching
- Solid-state reliability
- I/O compatible with integrated circuits



# absolute maximum ratings: (25°C) (unless otherwise specified)

Storage and Operating Temperature -55° to 85°C. Lead Soldering Time (at 260°C) 10 seconds.

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current	1	amp
(peak, $100 \mu$ s, $1\%$ duty cycle)		
Reverse Voltage	3	volts
*Derate 1.67mW/°C above 25°C ambi	ent	

Power Dissipation	**150	milliwatts
Collector Current (Continuous)	100	milliamps
$v_{CEO}$	25	volts
$v_{ECO}$	7	volts

# individual electrical characteristics (25°C)

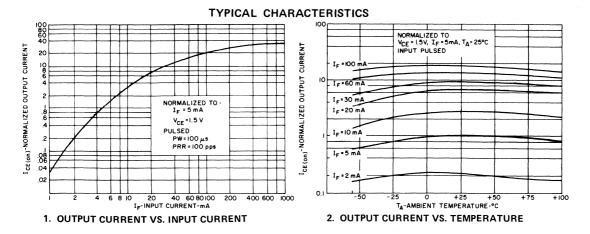
INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage V <sub>F</sub> (I <sub>F</sub> = 10 mA)	1.2	1.7	volts
Reverse Current $I_R$ $(V_R = 2V)$		10	μamps
Capacitance $C_J$ (V = O, f = 1 MHz)	150	-	pf

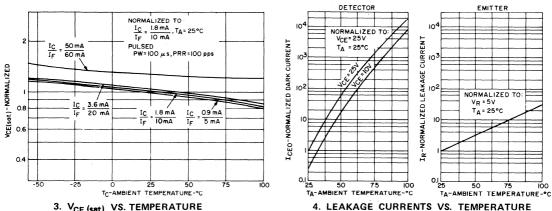
PHOTO-DARLINGTON	MIN.	MAX.	UNITS
Breakdown Voltage V(BR)CEO (IC = 10 mA)	25	-	volts
Breakdown Voltage $V_{(BR)ECO}(I_E = 100\mu a)$	7	, <del>-</del>	volts
Collector Dark Current I <sub>CEO</sub> (V <sub>CE</sub> = 10V, I <sub>F</sub> =O, H=O)		100	nA

# coupled electrical characteristics (25°C)

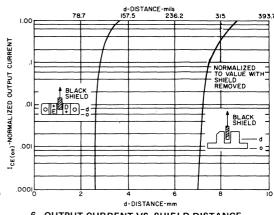
	MIN.	TYP.	MAX.	UNITS
Output Current (I <sub>F</sub> = 20mA, V <sub>CE</sub> = 5V)	2500	_		μamps
Saturation Voltage (I <sub>F</sub> = 20mA, I <sub>C</sub> = 0.5 mA)			1.2	volts
Switching Speeds ( $V_{CE} = 10V$ , $I_C = 2$ mA, $R_L = 100\Omega$ )				
On Time $(t_d + t_i)$		150		μsecs
Off Time $(t_S + t_f)$	-	150	i -	μsecs
		İ		<b>-</b>







3. V<sub>CE (sat)</sub> VS. TEMPERATURE



AND TOFF NORMALIZED PW = 300 µs PRR = 100 pps I<sub>F</sub> = 7.5 AMPS, V<sub>CC</sub> = 5 V NORMALIZED TO R<sub>L</sub> = 750 Ω Š .2 0.1 400 600 800 1000 1500 75
RL-LOAD RESISTANCE-OHMS 5. SWITCHING SPEED VS. R

6. OUTPUT CURRENT VS. SHIELD DISTANCE

# **CNY30, CNY34**

# **Optoisolator**

# GaAs Infrared Emitting Diode and Light Activated SCR

The CNY30 and CNY34 consist of a gallium arsenide, infrared emitting diode coupled with a light activated silicon controlled rectifier in a dual-in-line package. These devices are also available in surface-mount packaging.

## absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation (-55°C to 50°C)	*100	milliwatts
Forward Current (Continuous)	60	milliamps
(-55°C to 50°C)	•	
Forward Current (Peak) (-55°C to 50°C)	) 1	ampere
(100 µs 1% duty cycle)		
Reverse Voltage (-55°C to 50°C)	6	volts
*Derate 2.0mW/°C above 50°C.		

PHOTO-SCR	
Off-State and Reverse Voltage CNY30 200	volts
(-55°C to 100°C) CNY34 400	volts
Peak Reverse Gate Voltage (-55°C to 50°C) 6	volts
Direct On-State Current (-55°C to 50°C) 300	milliamps
Surge (non-rep) On-State Current 10	amps
(-55°C to 50°C)	-
Peak Gate Current (-55°C to 50°C) 10	milliamps
Output Power Dissipation	•
(-55°C to 50°C)** 400	milliwatts
**Derate 8mW/°C above 50°C.	

#### 350 8.89 330 8.38 8.64 2 .406 016 3 200 1.01 .070 .090 110 085 100 15 .381 .015 .375 2.92 135 INSTALLED POSITION LEAD CENTERS 2. OVERALL INSTALLED DIMENSION. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE. 4. FOUR PLACES.

MILLIMETERS

MIN MAX

NOTES

MAX

MIN

#### TOTAL DEVICE

Storage Temperature Range -55°C to 150°C
Operating Temperature Range -55°C to 100°C
Normal Temperature Range (No Derating) -55°C to 80°C
Soldering Temperature (10 seconds) 260°C
Total Device Dissipation (-55°C to 50°C), 450 milliwatts
Linear Derating Factor (above 50°C), 9.0mW/°C
Surge Isolation Voltage (Input to Output).

3535V(peak) 2500V(RMS)
Steady-State Isolation Voltage (Input to Output).

3180V(peak) 2250(RMS)

# individual electrical characteristics (25°C) (unless otherwise specified)

INFRAREDEMITTINGDIC	DDE TYP.	MAX.	UNITS
Forward Voltage V <sub>F</sub>	1.1	1.5	volts
$(I_F = 10mA)$			
	İ		
Reverse Current I <sub>R</sub>	-	10	microamps
$(V_R = 3V)$	•		
	Ì		
	1		
Capacitance C <sub>J</sub>	50	_	picofarads
(V = O, f = 1  MHz)			
-	1		
	1	1	

<del></del>				
PHOTO-SCR		MIN.	MAX.	UNITS
Peak Off-State Voltage-V <sub>DM</sub>	CNY30	200	_	volts
$(R_{GK} = 10K\Omega, T_A = 100^{\circ}C)$	CNY34	400	-	volts
Peak Reverse Voltage-V <sub>RM</sub>	CNY30	200	_ "	volts
$(T_A = 100^{\circ}C)$	CNY34	400	-	volts
On-State Voltage-V <sub>T</sub>			1.3	volts
$(I_T = 300 \text{mA})$				
Off-State Current-ID	CNY30		50	microamps
$(V_D = 200V, T_A = 100^{\circ}C, I_F = 0,$	$R_{GK}=10K$	1		_
Off-State Current-I <sub>D</sub>	CNY34		150	microamps
$(V_D = 400V, T_A = 100^{\circ}C, I_F = C$	$R_{GK}=10K$			
Reverse Current-I <sub>R</sub>	CNY30		50	microamps
$(V_R = 200V, T_A = 100^{\circ}C, I_F = 0)$				-
Reverse Current-I <sub>R</sub>	CNY34		150	microamps
$(V_R = 400V, T_A = 100^{\circ}C, I_F$	= O)			•

# coupled electrical characteristics (25°C)

	MIN.	MAX.	UNITS
Input Current to Trigger $V_{AK} = 50V, R_{GK} = 10K\Omega$ $I_{FT}$	_	20	milliamps
$V_{AK} = 100V$ , $R_{GK} = 27K\Omega$ $I_{FT}$	-	11	milliamps
Isolation Resistance $V_{IO} = 500V_{DC}$	100	_	gigaohms
Turn-On Time – $V_{AK}$ = 50V, $I_F$ = 30mA, $R_{GK}$ = 10K $\Omega$ , $R_L$ = 200 $\Omega$ $t_{on}$		50	microseconds
Coupled dv/dt, Input to Output (See Figure 13)	500	·	volts microsec
Input to Output Capacitance (V <sub>IO</sub> = O,f = 1 MHz)	_	2	picofarads

<sup>(</sup>a) VDE Approved to 0883/6.80 0110b Certificate # 35025

# 14

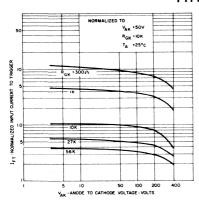


FIGURE 1. INPUT CURRENT TO TRIGGER
VS. ANODE-CATHODE VOLTAGE

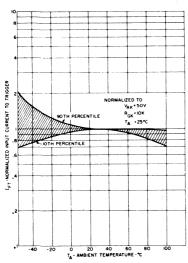


FIGURE 3. INPUT CURRENT TO TRIGGER DISTRIBUTION VS. TEMPERATURE

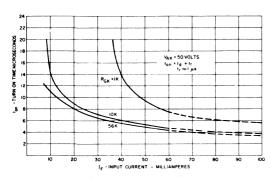


FIGURE 5, TURN-ON TIME VS. INPUT CURRENT

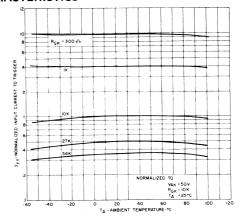


FIGURE 2. INPUT CURRENT TO TRIGGER VS. TEMPERATURE

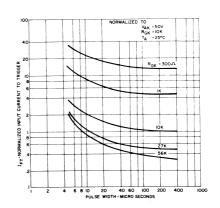


FIGURE 4. INPUT CURRENT TO TRIGGER VS. PULSE WIDTH

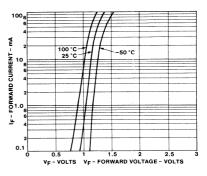


FIGURE 6. INPUT CHARACTERISTICS  $I_F$  VS.  $V_F$ 

#### **CNY30, CNY34**

#### TYPICAL CHARACTERISTICS OF OUTPUT (SCR)

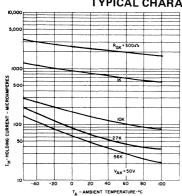


FIGURE 7. HOLDING CURRENT VS. TEMPERATURE

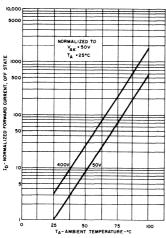


FIGURE 9. OFF-STATE FORWARD CURRENT VS. TEMPERATURE

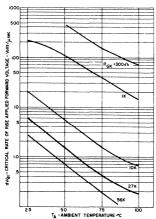


FIGURE 11. dv/dt VS. TEMPERATURE

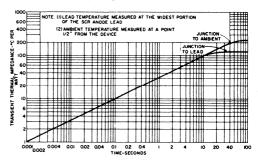


FIGURE 8. MAXIMUM TRANSIENT THERMAL IMPEDANCE

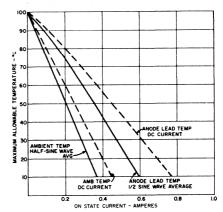


FIGURE 10. ON-STATE CURRENT VS.
MAXIMUM ALLOWABLE TEMPERATURE

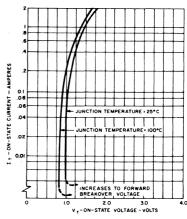
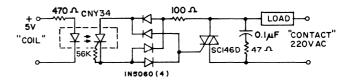


FIGURE 12. ON-STATE CHARACTERISTICS

#### TYPICAL APPLICATIONS

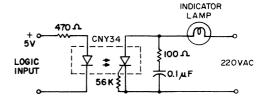
#### 10A, T2L COMPATIBLE, SOLID STATE RELAY

Use of the CNY34 for high sensitivity, 2500V isolation capability, provides this highly reliable solid state relay design. This design is compatible with 74, 74S and 74H series T<sup>2</sup>L logic systems inputs and 220V AC loads up to 10A.



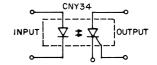
#### 25W LOGIC INDICATOR LAMP DRIVER

The high surge capability and non-reactive input characteristics of the device allow it to directly couple, without buffers, T<sup>2</sup> L and DTL logic to indicator and alarm devices, without danger of introducing noise and logic glitches.

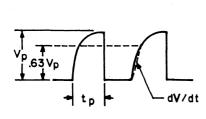


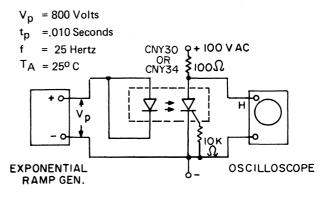
#### 400V SYMMETRICAL TRANSISTOR COUPLER

Use of the high voltage PNP portion of the CNY34 provides a 400V transistor capable of conducting positive and negative signals with current transfer ratios of over 1%. This function is useful in remote instrumentation, high voltage power supplies and test equipment. Care should be taken not to exceed the CNY34 400 mW power dissipation rating when used at high voltages.



# FIGURE 13 COUPLED dv/dt — TEST CIRCUIT





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#### CNY31

# Optoisolator GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier

The CNY31 is a gallium arsenide, infrared emitting diode coupled with a silicon photo-Darlington amplifier in a low-cost plastic package with lead spacing compatible to a dual in-line package.

# absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1 µsec 300 pps)		
Reverse Voltage	3	volts
*Derate 1.67 mW/°C above		

PHOTO-DARLINGTON		
Power Dissipation	**150	milliwatts
$V_{CEO}$	30	volts
$V_{\rm ECO}$	7	volts
Collector Current (Continuous)	100	milliamps
**Derate 2.5 mW/°C above	25°C ambient	

# TOTAL DEVICE

Storage Temperature -55 to 85°C
Operating Temperature -55 to 85°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output).

5650V<sub>(peak)</sub> 4000V<sub>(RMS)</sub>
Steady-State Isolation Voltage (Input to Output).

5300V<sub>(peak)</sub> 3750V<sub>(RMS)</sub>

#### individual electrical characteristics (25°C)

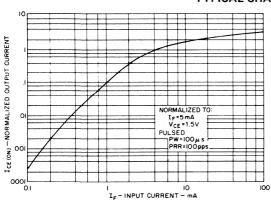
INFRARED EMITTING	G DIODE	TYP.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> = 10mA)	$V_{\mathrm{F}}$	1.1	1.7	volts
Reverse Current (V <sub>R</sub> = 3V)	$I_R$	-	10	microamps
Capacitance (V = O,f = 1 MHz)	$C_J$	50	_	picofarads

PHOTO-DARLINGTON	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - V <sub>(BR)CEO</sub>	30	_	_	volts
$(I_C = 10mA, I_F = 0)$		1		
Breakdown Voltage – V <sub>(BR)ECO</sub>	7	-	-	volts
$(I_E = 100 \mu A, I_F = O)$		_		
Collector Dark Current – I <sub>CEO</sub>	-	5	100	nanoamps
$(V_{CE} = 10V, I_{F} = 0)$				6
Capacitance	-	6	_	picofarads
$(V_{CE} = 10V, f = 1 MHz)$				

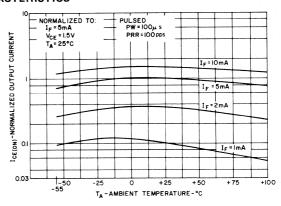
# coupled electrical characteristics (25°C)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_F = 5 \text{ mA}$ , $V_{CE} = 5 \text{ V}$ )	400	_		%
Saturation Voltage – Collector to Emitter ( $I_F = 5 \text{ mA}$ , $I_C = 2 \text{ mA}$ )		0.8	1.4	volts
Isolation Resistance (Input to Output Voltage = 500V <sub>DC</sub> )	100		_	gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1 MHz)		-	2	picofarads
Switching Speeds. Turn-On Time $-(V_{CE} = 10V, I_{C} = 10mA, R_{L} = 100\Omega)$		125	-	microseconds
Turn-Off Time – $(V_{CE} = 10V, I_C = 10mA, R_L = 100\Omega)$	_	100	_	microseconds

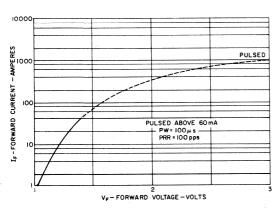
### TYPICAL CHARACTERISTICS



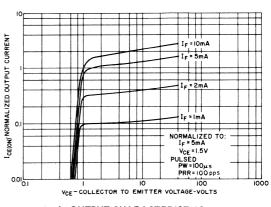
1. OUTPUT CURRENT VS. INPUT CURRENT



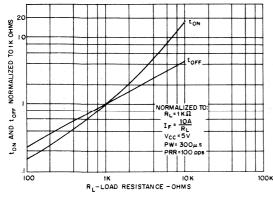
2. OUTPUT CURRENT VS. TEMPERATURE



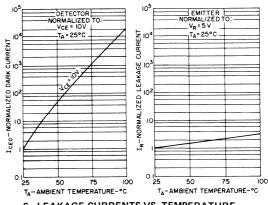
3. INPUT CHARACTERISTICS



4. OUTPUT CHARACTERISTICS



5. SWITCHING SPEED VS. RL



6. LEAKAGE CURRENTS VS. TEMPERATURE

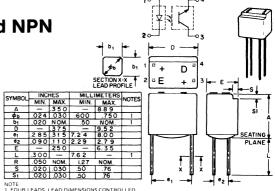
# Optoisolator GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The CNY32 is a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a low-cost plastic package with lead spacing compatible to a dual in-line package.

# absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE				
Power Dissipation	*100	milliwatts		
Forward Current (Continuous)	60	Milliamps		
Forward Current (Peak)	3	ampere		
(Pulse width 1 µsec 300 pps)		_		
Reverse Voltage	3	volts		
*Derate 1.67 mW/° above 25°C ambient.				

**150	milliwatts
30	volts
5	volts
100	milliamps
	30 5



NUTE

1. FOUR LEADS, LEAD DIMENSIONS CONTROLLED
BETWEEN .050" (1.27 MM) FROM THE SEATING
PLANE AND THE END OF THE LEADS.

### TOTAL DEVICE

Storage Temperature -55 to 85°C
Operating Temperature -55 to 85°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output)
5650V<sub>(peak)</sub> 4000V<sub>(RMS)</sub>
Steady-State Isolation Voltage (Input to Output).
5300V<sub>(peak)</sub> 3750V<sub>(RMS)</sub>

# individual electrical characteristics (25°C)

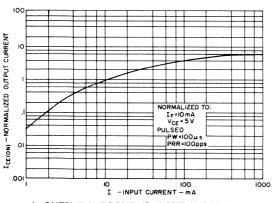
INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage $V_F$ $(I_F = 10mA)$	1.1	1.7	volts
Reverse Current $I_R$ $(V_R = 3V)$	-	10	micoramps
Capacitance $C_J$ (V = O, f = 1  MHz)	50		picofarads

PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - V(BR)CEO	30	_	-	volts
$(I_C = 10mA, I_F = 0)$				
Breakdown Voltage – V <sub>(BR)ECO</sub>	-5	-	-	volts
$(I_E = 100\mu A, I_F = 0)$				
Collector Dark Current – I <sub>CEO</sub>	- 1	5	100	nanoamps
$(V_{CE} = 10V, I_F = 0)$				
Capacitance		3.5	-	picofarads
$(V_{CE} = 10V, f = 1 MHz)$				

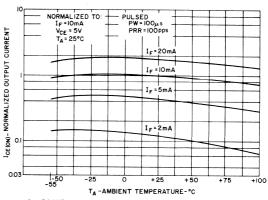
# coupled electrical characteristics (25°C)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_F = 10$ mA, $V_{CE} = 10$ V)	20	_	_	%
Saturation Voltage – Collector to Emitter ( $I_F = 10\text{mA}$ , $I_C = 0.5\text{mA}$ )		0.2	0.4	volts
Isolation Resistance (Input to Output Voltage = 500V <sub>DC</sub> )	100	_		gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1 MHz)	_	_	2	picofarads
Switching Speeds: Turn-On Time $-(V_{CE} = 10V, I_{CE} = 2mA, R_L = 100\Omega)$	_	3		microseconds
Turn-Off Time – $(V_{CE} = 10V, I_{CE} = 2mA, R_L = 100\Omega)$	-	3	_	microseconds

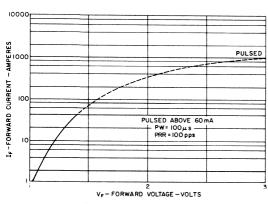
### TYPICAL CHARACTERISTICS



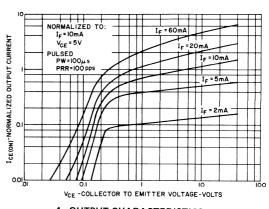
1. OUTPUT CURRENT VS. INPUT CURRENT



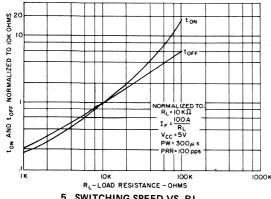
2. OUTPUT CURRENT VS. TEMPERATURE



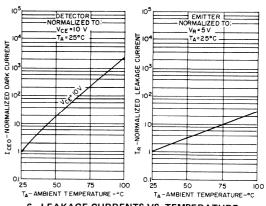
3. INPUT CHARACTERISTICS



4. OUTPUT CHARACTERISTICS



5. SWITCHING SPEED VS. RL



6. LEAKAGE CURRENTS VS. TEMPERATURE

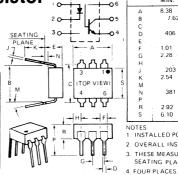
# **Optoisolator**

**GaAs Infrared Emitting Diode and NPN** Silicon High Voltage Phototransistor

The CNY33 is a gallium arsenide, infrared emitting diode coupled with silicon high voltage phototransistors in a dual in-line package. This device is also available in surfacemount packaging.

# absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1 µsec 300 pps)		
Reverse Voltage	6	volts
*Derate 1.33mW/°C above 25°C amb	ient.	



1	SYMBOL.	MILLIM	ETERS	INC	HES	NOTES
	STIVIBUL	MIN.	MAX.	MIN.	MAX.	NOTES
	A	8.38	8.89	.330	.350	
	В	7.62	REF.	.300	REF.	1
	C :		8.64		.340	2
	D	.406	.508	.016	.020	
ł	E		5.08		.200	3
	F	1.01	1.78	.040	.070	
	G	2.28	2.80	.090	.110	
	н		2.16		.085	4
,	J	.203	.305	.008	.012	1
ĺ	К	2.54		100		
3	M		15		15	
	N .	.381		.015	1	
Ł.	Р		9.53		.375	1
	. R	2.92	3.43	.115	.135	
	S	6.10	6.86	.240	.270	

- INSTALLED POSITION LEAD CENTERS
- 2. OVERALL INSTALLED DIMENSION. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE

PHOTO-TRANSISTOR				
Power Dissipation	**300	milliwatts		
$ m V_{CEO}$	300	volts		
$V_{CBO}$	300	volts		
$V_{\mathrm{EBO}}$	7	volts		
Collector Current	100	milliamps		
(Continuous)				
**Derate 4.0mW/°C above 25° ambient.				

### **TOTAL DEVICE**

Storage Temperature -55 to 150°C Operating Temperature -55 to 100°C Lead Soldering Time (at 260°C) 10 seconds. Surge Isolation Voltage (Input to Output).  $3535V_{(peak)}$ 2500V(RMS) Steady-State Isolation Voltage (Input to Output).  $3180V_{(peak)}$ 2250V<sub>(RMS)</sub>

# individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage V <sub>F</sub> (I <sub>F</sub> = 10mA)	1.1	1.5	volts
Reverse Current $I_R$ $(V_R = 6V)$	-	10	microamps
Capacitance C <sub>J</sub> (V = O,f = 1 MHz)	50	_	picofarads

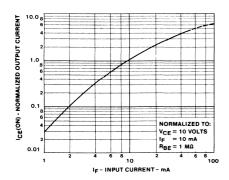
PHOTO-TRANSISTOR	MIN.	MAX.	UNITS
Breakdown Voltage – V <sub>(BR)CEO</sub>	300	-	volts
$(I_C = 1 \text{mA}; I_F = 0)$ Breakdown Voltage $-V_{(BR)CBO}$	300		volts
$(I_C = 100\mu A; I_F = 0)$ Breakdown Voltage $-V_{(BR)EBO}$	7	-	volts
$(I_E = 100\mu A; I_F = 0)$	2 1 1		
Collector Dark Current – $I_{CEO}$ ( $V_{CE}$ =200V; $I_{F}$ =0, $T_{A}$ = 25°C)	-	100	nanoamps
$(V_{CE}=200V; I_F=0; T_A=100^{\circ}C)$	_	250	microamps

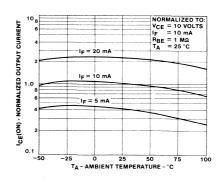
# coupled electrical characteristics (25°C)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_F = 10 \text{mA}$ , $V_{CE} = 10 \text{V}$ )	20	<del>-</del>	-	%
Saturation Voltage – Collector to Emitter (I <sub>F</sub> = 10mA, I <sub>C</sub> = 0.5mA)	_	0.1	0.4	volts
Isolation Resistance ( $V_{IO} = 500V_{DC}$ )	100	_ :	-	gigaohms
Input to Output Capacitance (V <sub>IO</sub> = O,f = 1MHz)		-	2	picofarads
Switching Speeds: Turn-On Time – $(V_{CE} = 10V, I_{CE} = 2mA, R_L = 100\Omega)$	_	5 ,		microseconds
Turn-Off Time – $(V_{CE} = 10V, I_{CE} = 2mA, R_L = 100\Omega)$		5	· ÷ ,.	microseconds

VDE Approved to 0883/6.80 0110b Certificate # 35025

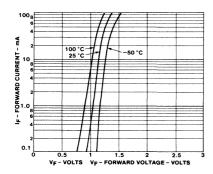
### TYPICAL CHARACTERISTICS

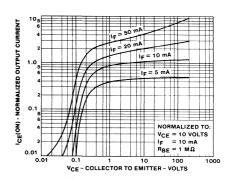




### 1. OUTPUT CURRENT VS INPUT CURRENT

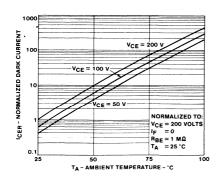
2. OUTPUT CURRENT VS. TEMPERATURE

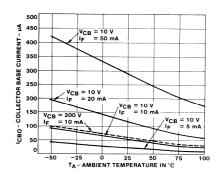




### 3. INPUT CHARACTERISTICS

4. OUTPUT CHARACTERISTICS





5. NORMALIZED DARK CURRENT VS. TEMPERATURE

6. COLLECTOR BASE CURRENT VS. TEMPERATURE

# **Optoisolator**

AC Input GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The CNY35 consists of two gallium arsenide, infrared emitting diodes connected in inverse parallel and coupled with a silicon phototransistor in a dual in-line package. This device is also available in surface-mount packaging.

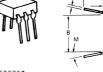
- FEATURES:

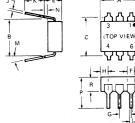
   AC or polarity insensitive inputs
  - · Fast switching speeds
  - · Built-in reverse polarity input protection
  - · High isolation voltage
  - High isolation resistance
  - I/O compatible with integrated circuits

# absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE		
Power Dissipation $-T_A = 25^{\circ}C$	*100	milliwatts
Power Dissipation $-T_A = 25^{\circ}C$	*100	milliwatts
(T <sub>C</sub> indicates collector lead		
temperature 1/32" from case)		
Input Current (RMS)	60	milliamps
Input Current (Peak)	±1	ampere
(Pulse width 1 $\mu$ s, 300 pps)		
*Derate 1.33 mW/°C at	bove 25°C	

PHOTO-TRANSISTOR		To the second
Power Dissipation - T <sub>A</sub> = 25°C Power Dissipation - T <sub>A</sub> = 25°C (T <sub>C</sub> indicates collector lead temperature 1/32" from case)	**300 ***500	milliwatts milliwatts
$V_{CEO}$ $V_{CBO}$ $V_{EBO}$ Collector Current Continuous)  **Derate 4.0 mW/ $^{\circ}$ C at	30 70 5 100	volts volts volts milliamps
***Derate 6.7 mW/°C ab		





SYMBOL	MILLIM	ETERS	INC	HES	NOTES
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
A	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1 1
C	- 1	8.64	-	.340	2
D	.406	.508	.016	.020	
Ë	_	5.08	***	.200	3
F	1.01	1.78	.040	.070	1
G	2.28	2.80	.090	.110	
н		2.16		.085	4
J	.203	.305	.008	.012	İ
ĸ	2.54	_	.100	-	
M	-	15		15	
N	.381	-	.015	-	1
P	- !	9.53		.375	
R	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	

#### NOTES

- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES.

### TOTAL DEVICE

Storage Temperature -55 to 150°C
Operating Temperature -55 to 100°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output)
1500V<sub>(neak)</sub> 1060V<sub>(RMS)</sub>

Steady-State Isolation Voltage (Input to Output) 950V<sub>(peak)</sub> 660V<sub>(RMS)</sub>

# individual electrical characteristics (25°C) (unless otherwise specified)

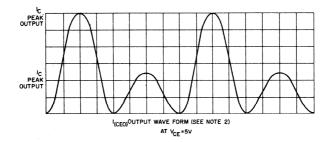
INFRARED EMITTING DIODE	MAX.	UNITS
Input Voltage $-V_F$ $(I_F = \pm 10 \text{mA})$	1.8	volts
Capacitance C <sub>J</sub> (V = O,f = 1 MHz)	100	picofarads

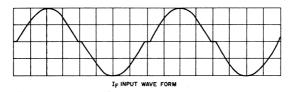
PHOTO-TRANSISTOR	MIN.	MAX.	UNITS
Breakdown Voltage – V <sub>(BR)CEO</sub>	30	_	volts
$(I_C = 10 \text{mA}, I_F = 0)$			
Breakdown Voltage – V <sub>(BR)CBO</sub>	70	-	volts
$(I_C = 100\mu A, I_F = 0)$			
Breakdown Voltage – $V_{(BR)EBO}$	5	_	volts
$(I_E = 100\mu A, I_F = 0)$			1
Collector Dark Current - I <sub>CEO</sub>	_	200	nanoamps
$(V_{CE} = 10V, I_{F} = 0)$			

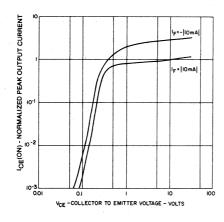
# coupled electrical characteristics (25°C) (unless otherwise specified)

	MIN.	MAX.	UNITS
Current Transfer Ratio ( $V_{CE} = 10V$ , $I_F = \pm 10mA$ )	10		percent
Saturation Voltage — Collector to Emitter (I <sub>CEO</sub> = 0.5 mA, I <sub>F</sub> = ± 10mA)	_	0.4	volts
Isolation Resistance V <sub>IO</sub> = 500V (note 1)	100	-	gigaohms

Note 1: Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together.

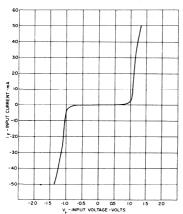




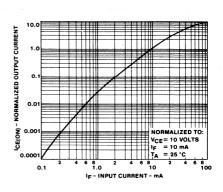


Note 2: These waveforms and curves are exaggerated in amplitude differences to indicate the outputs corresponding to the positive and negative input polarities will not be identical. Typical differences in amplitude is 10% to 20%.

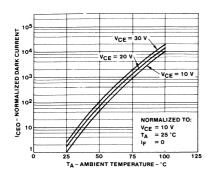
TYPICAL CHARACTERISTICS



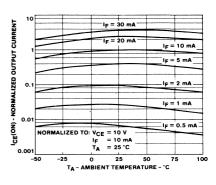
1. INPUT CHARACTERISTICS



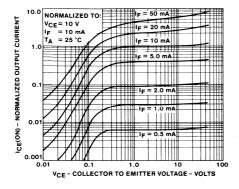
2. OUTPUT CURRENT VS INPUT CURRENT



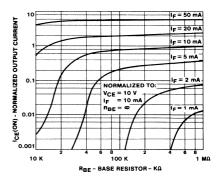
3. DARK  $I_{CEO}$  CURRENT VS TEMPERATURE



4. OUTPUT CURRENT VS TEMPERATURE

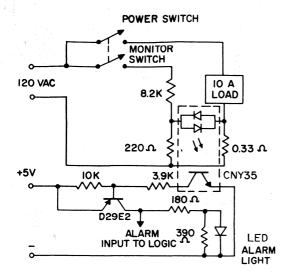


5. OUTPUT CHARACTERISTICS



6. OUTPUT CURRENT VS BASE EMITTER RESISTANCE

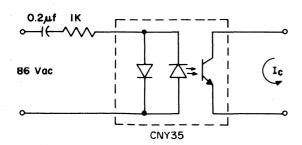
### LOAD MONITOR AND ALARM



In many computer controlled systems where AC power is controlled, load dropout due to filament burnout, fusing, etc. or the opposite situation - load power when uncalled for due to switch failure can cause serious systems or safety problems. This circuit provides a simple AC power monitor which lights an alarm lamp and provides a "1" input to the computer control in either of these situations while maintaining complete electrical isolation between the logic and the power system.

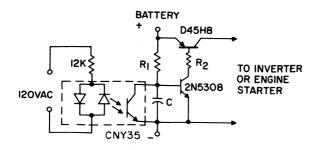
Note that for other than resistive loads, phase angle correction of the monitoring voltage divider is required.

### RING DETECTOR



In many telecommunications applications it is desirable to detect the presence of a ring signal in a system without any direct electrical contact with the system. When the 86 Vac ring signal is applied, the output transistor of the CNY35 is turned on indicating the presence of a ring signal in the isolated telecommunications system.

### **UPS SOLID STATE TURN-ON SWITCH**



Interruption of the 120 VAC power line turns off the CNY35, allowing C to charge and turn on the 2N5308-D45H8 combination which activates the auxiliary power supply. This system features low standby drain, isolation to prevent ground loop problems and the capability of ignoring a fixed number of "dropped cycles" by choice of the value of C.

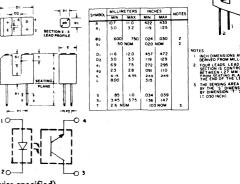
# Optointerrupter Module GaAs Infrared Emitting Diode and NPN

Silicon Phototransistor Module

The CNY36 is a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a plastic housing. The gap in the housing provides a means of interrupting the signal with tape, cards, shaft encoders, or other opaque material, switching the output transistor from an "ON" into an "OFF" state.

### **FEATURES**:

- Low cost, plastic module
- Non-contact switching
- Fast switching speeds
- Solid state reliability
- I/O compatible with integrated circuits



# absolute maximum ratings: (25°C) (unless otherwise specified)

Storage and Operating Temperature -55° to 85°C. Lead Soldering Time (at 260°C) 10 seconds.

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current	1	amp
(peak, 100µs, 1% duty cycle)		•
Reverse Voltage	3	volts
*Derate 1.67mW/°C above 25°C	mbient	

Power Dissipation	**150	milliwatts
Collector Current (Continuous)	100	milliamps
$v_{CEO}$	30	volts
VECO	5	volts

# individual electrical characteristics (25°C)

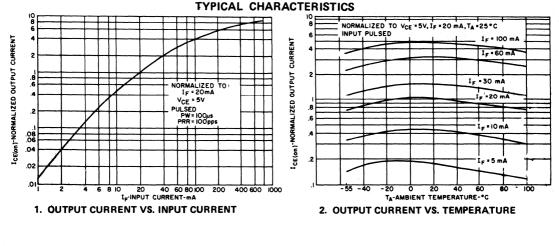
INFRARED EMITTING	DIODE	TYP.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> = 10 mA)	$V_{\rm F}$	1.2	1.7	volts
Reverse Current (V <sub>R</sub> = 2V)	I <sub>R</sub>	-	10	µamps −
Capacitance (V = O, f = 1 Mhz)	$c_{j}$	150	, -	pf

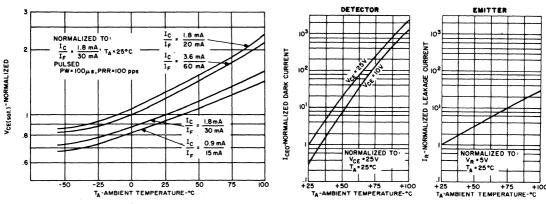
PHOTO-TRANSISTOR	MIN.	MAX.	UNITS
Breakdown Voltage V(BR)CEO (IC = 10 mA)	30	· //.	volts
Breakdown Voltage V <sub>(BR)ECO</sub> (I <sub>E</sub> = 100μA)	5	- '	volts
Collector Dark Current ICEO (VCE = 10V, IF = 0, H=0)		100	nA.

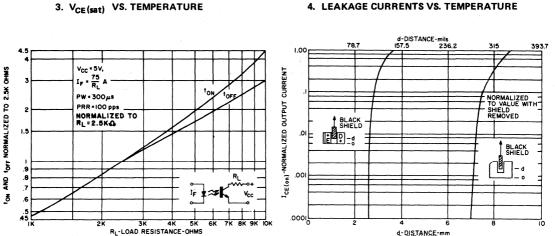
# coupled electrical characteristics (25°C)

	MIN.	TYP.	MAX.	UNITS
Output Current (I <sub>F</sub> = 20mA, $V_{CE}$ = 10V) Saturation Voltage (I <sub>F</sub> = 20mA, $I_{C}$ = 25 $\mu$ A) Switching Speeds ( $V_{CE}$ = 10V, $I_{C}$ = 2mA, $R_{L}$ = 100 $\Omega$ )	200	400 0.2	_ 0.4	µamps volts
On Time $(t_d + t_r)$ Off Time $(t_s + t_f)$		5 5	- -	μsec μsec









5. SWITCHING SPEED VS. R<sub>L</sub> 6. OUTPUT CURRENT VS. DISTANCE

# CNY47, CNY47A

# **Optoisolator**

# GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The CNY47 and CNY47A are gallium arsenide, infrared emitting diodes coupled with a silicon phototransistor in a dual in-line package. These devices are also available in surface-mount packaging.

# absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	30	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1 $\mu$ s 300 pps)		
Reverse Voltage	3	volts
*Derate 1.33mW/°C above 25°C	C ambient	

PHOTO-TRANSISTOR		
Power Dissipation	**150	milliwatts
$V_{ m CEO}$	30	volts
$V_{CBO}$	50	volts
$V_{EBO}$	4	volts
Collector Current (Continuous)	30	milliamps
**Derate 2.0mW/°C above 25°C	C ambient	

# 8 SEATING STATES AND S

# TOTAL DEVICE

3180V(peak)

Storage Temperature -55 to 150°C
Operating Temperature -55 to 100°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output).
3535V(peak)
2500V(RMS)
Steady-State Isolation Voltage (Input to Output).

### individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	ТҮР.	MAX.	UNITS	
Forward Voltage V <sub>F</sub> (I <sub>F</sub> = 10 mA)	1.1	1.5	volts	
Reverse Current I <sub>R</sub> (V <sub>R</sub> = 3 V)	_	100	microamps	
Capacitance C <sub>J</sub> (V = O,f = 1 MHz)	50		picofarads	
I .	1	1	i	ı

<b>,</b>				
PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage- $V_{(BR)CEO}$ ( $I_C = 10mA, I_F = 0$ )	30	-	-	volts
Breakdown Voltage-V <sub>(BR)CBO</sub>	50	-		volts
$(I_C = 100\mu A, I_F = O)$ Breakdown Voltage- $V_{(BR)EBO}$	4	-	_	volts
$(I_E = 100 \mu A, I_F = O)$		5	100	
Collector Dark Current $-I_{CEO}$ ( $V_{CE} = 10V, I_F = O$ )	_	5	100	nanoamps
Collector Dark Current-I <sub>CBO</sub>	-	-	_ 20	nanoamps
(V <sub>CB</sub> = 10V, I <sub>F</sub> = 0) Capacitance	_	2	_	picofarads
$(V_{CE} = 10V, F = 1 MHz)$				

2250(RMS)

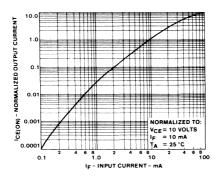
# coupled electrical characteristics (25°C)

		MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_F = 10mA$ , $V_{CE} = .4V$ )	CNY47	20		60	%
	CNY47A	40		. —	%
Saturation Voltage – Collector to Emitter ( $I_F = 10mA$ , $I_C = 2mA$ )	CNY47		0.1	0.4	volts
Isolation Resistance ( $V_{IO} = 500V_{DC}$ ) ( $I_F = 10mA$ , $I_C = 4mA$ )	CNY47A	100	_	0.4	volts gigaohms
Input to Output Capacitance (V <sub>IO</sub> = O,f = 1 MHz)		-		2	picofarads
Switching Speeds:		1			
Rise/Fall Time ( $V_{CE} = 10V$ , $I_{CE} = 2mA$ , $R_L = 100\Omega$ )		_	2		microseconds
Rise/Fall Time ( $V_{CB} = 10V$ , $I_{CB} = 50\mu A$ , $R_L = 100\Omega$ )			300	_	nanoseconds

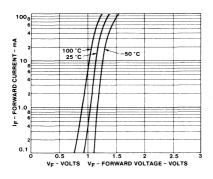
VDE Approved to 0883/6.80 0110b Certificate # 35025

# CNY47, CNY47A

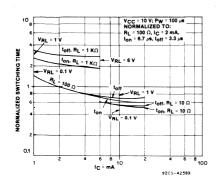
### TYPICAL CHARACTERISTICS



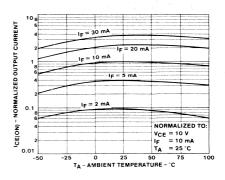
1. OUTPUT CURRENT VS INPUT CURRENT



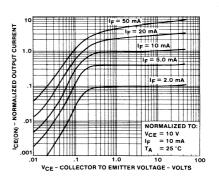
3. INPUT CHARACTERISTICS



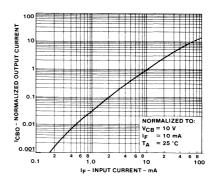
5. SWITCHING SPEED VS COLLECTOR CURRENT (NOT SATURATED)



2. OUTPUT CURRENT VS TEMPERATURE



4. OUTPUT CHARACTERISTICS



6. OUTPUT CURRENT (ICBO) VS INPUT CURRENT

# CNY48 Optoisolator

# GaAs Infrared Emitting Diode and NPN Silicon Photo-Darlington Amplifier

The CNY48 consists of a gallium arsenide, infrared emitting diode coupled with a silicon photo-Darlington amplifier in a dual in-line package. This device is also available in surfacemount packaging.

# absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1 $\mu$ s 300 pps)		
Reverse Voltage	3	volts
*Derate 1.33mW/°C above	25°C ambie	ent.

PHOTO-DARLINGTON		
Power Dissipation	**150	milliwatts
V <sub>CEO</sub>	30	volts
V <sub>CBO</sub>	30	volts
V <sub>EBO</sub>	6	volts
Collector Current (Continuous)	100	milliamps
**Derate 2.0mW/°C above 25	°C ambient.	-

#### MILLIMETERS INCHES NOTES MIN. MAX. MIN 8.89 350 300 REF 7.62 REE 340 8.64 .020 016 5.08 PLANE 0.70 1.78 .090 110 2.28 2.80 085 2.16 008 .012 15 15 .381 .015 .375 115 .135 2 92 3.43 6.86 1. INSTALLED POSITION LEAD CENTERS OVERALL INSTALLED DIMENSION. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE 4. FOUR PLACES

# TOTAL DEVICE Storage Temperature -65 to 150°C Operating Temperature -55 to 100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output). 3535V(peak) 2500V(RMS) Steady-State Isolation Voltage (Input to Output). 3180V(peak) 2250(RMS)

# individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage V <sub>F</sub> (I <sub>F</sub> = 10mA)	1.1	1.3	volts
Reverse Current $I_R$ $(V_R = 3V)$	_	10	microamps
Capacitance C <sub>J</sub> (V = O,f = 1 MHz)	50	_	picofarads

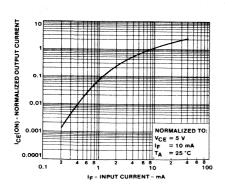
PHOTO-DARLINGTON	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage-V <sub>(BR)CEO</sub>	30	-	-	volts
$(I_C = 10\text{mA}, I_F = 0)$ Breakdown Voltage $-V_{(BR)CBO}$	30	~	_	volts
$(I_C = 100\mu A, I_F = O)$ Breakdown Voltage $-V_{(BR)EBO}$	6	-	_	volts
$(I_F = 100\mu A, I_F = O)$ Collector Dark Current $-I_{CEO}$	_	5	100	nanoamps
$(V_{CE} = 10V, I_F = 0)$ Capacitance	_	6	-	picofarads
$(V_{CE} = 10V, f = 1 \text{ MHz})$				

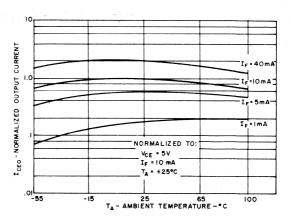
# coupled electrical characteristics (25°C)

		MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_F = 10$ mA, $V_{CE} = 1$ V)		600	-	-	%
Saturation Voltage—Collector to Emitter ( $I_F = 1 \text{mA} I_C = 2 \text{mA}$ )		_	-	.8	volts
$(I_F = 5mA I_C = 10mA)$		_	_	.8	volts
$(I_F = 10 \text{mA}, I_C = 60 \text{mA})$		_	-	1.0	volts
Isolation Resistance ( $V_{IO} = 500V_{DC}$ )		100	- 1	_	gigaohms
Input to Output Capacitance $(V_{IO} = O, f = 1 MHz)$		_	- '	2	picofarads
Switching Speeds: $(V_{CE} = 10V, I_C = 10mA, R_L = 100\Omega)$	On-Time		125	-	microseconds
	Off-Time	_	100		microseconds

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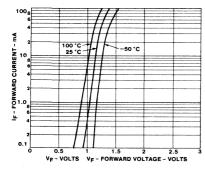
### TYPICAL CHARACTERISTICS

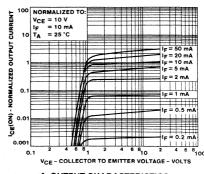




### 1. OUTPUT CURRENT VS INPUT CURRENT

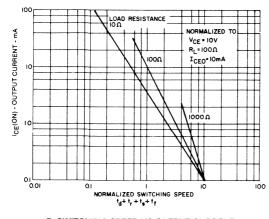


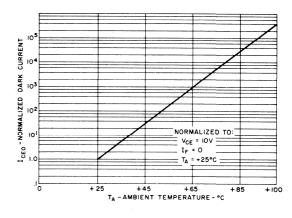




### 3. INPUT CHARACTERISTICS







5. SWITCHING SPEED VS OUTPUT CURRENT

6. NORMALIZED DARK CURRENT VS TEMPERATURE

# **Optoisolator**

**GaAs Infrared Emitting Diode and NPN** 

**Silicon Phototransistor** 





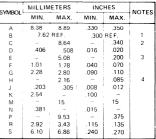
The CNY51 consists of a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. This device is also available in surface-mount packaging.

### **FEATURES:**

- High isolation voltage, 5000V minimum.
- Unique patented glass isolation construction
- High efficiency liquid epitaxial IRED.
- High humidity resistant silicone encapsulation.
- · Fast switching speeds.

absolute maximum ratings: (25°C) (unless otherwise specified)

1	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	Γ
С	(TOP VIEW) S	1
+	<u></u>	ŀ
R P	H  F -  G  F	



DET TITLE	4
PLANE	1
J → H + K →	<del> -</del> E-+
4 1	11
	- N
	11
Ī	1 1
	1 1
B	1 1
	1 1
M	1 1
1 /	1 1
+ +	7

- NOTES:
  1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE
- SEATING PLANE
- 4. FOUR PLACES.

Creepage Distance 8.2 mm min. Air Gap 7.6 mm min.

INFRARED EMITTING DIODE		
Power Dissipation $-T_A = 25^{\circ}C$	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	amperes
(Pulse width 1 $\mu$ sec, 300 pps)		
Reverse Voltage	6	volts
*Derate 1.33mW/°C above 2	25°C.	

**300	milliwatts
70	volts
70	volts
7	volts
100	milliamps
	70 7

### TOTAL DEVICE

Storage Temperature -55 to 150°C. Operating Temperature -55 to 100°C.

Lead Soldering Time (at 260°C) 10 seconds.

Surge Isolation Voltage (Input to Output). See Note 2.

 $5656V_{(peak)}$   $4000V_{(RMS)}$ 

Steady-State Isolation Voltage (Input to Output).

See Note 2. 5000V<sub>(DC)</sub>

 $3000V_{(RMS)}$ 

# individual electrical characteristics (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE	MIN.	MAX.	UNITS
Forward Voltage — V <sub>F</sub> (I <sub>F</sub> = 60mA)	-	1.65	volts
Forward Voltage — V <sub>F</sub> (I <sub>F</sub> = 10mA)	.8	1.5	volts
	.9	1.7	volts
Forward Voltage — $V_F$ $(I_F = 10 \text{mA})$ $T_A = +100^{\circ}\text{C}$	.7	1.4	volts
Reverse Current $-I_R$ $(V_R = 6V)$		10	microamps
Capacitance $-C_J$ (V = O,f = 1 MHz)		100	picofarads

PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage $-V_{(BR)CEO}$ $(I_C = 10 \text{mA}, I_F = O)$	70	-	-	volts
Breakdown Voltage – $V_{BR)CEO}$ ( $I_C = 100\mu A, I_F = O$ )	70		-	volts
Breakdown Voltage — $V_{(BR)CEO}$ ( $I_C = 100\mu A, I_F = O$ )	7		-	volts
Collector Dark Current — I <sub>CEO</sub> (V <sub>CE</sub> = 10V, I <sub>F</sub> = O)	-	5	50	nano- amps
Collector Dark Current — $I_{CEO}$ ( $V_{CE} = 10\dot{V}, I_F = O$ ) $T_A = 100^{\circ} C$	_		500	micro- amps
Capacitance — $C_{CE}$ ( $V_{CE} = 10V, f = 1MHz$ )	_	2	_	pico farads

Na Covered under U.L. component recognition program, reference file E51868

**VDE** Approved to 0883/6.80 0110b Certificate #. 35025

# coupled electrical characteristics (25°C) (unless otherwise specified)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_F = 10 \text{mA}$ , $V_{CE} = 10 \text{V}$ ) CYN51	100	_	_	%
Saturation Voltage – Collector to Emitter ( $I_F = 20mA$ , $I_C = 2mA$ )		_	0.4	volts
Isolation Resistance (Input to Output Voltage = 500V <sub>DC</sub> . See Note 1)	100		_	gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1 MHz. See Note 1)	-	- 1	2.0	picofarads
Turn-On Time $-t_{on}$ ( $V_{CC} = 10V$ , $I_C = 2mA$ , $R_L = 100\Omega$ ). (See Figure 1)		5	10	microseconds
Turn-Off Time – $t_{off}$ ( $V_{CC}$ = 10V, $I_C$ = 2mA, $R_L$ = 100 $\Omega$ ). (See Figure 1)	,	5	10	microseconds

#### NOTE 1

Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together.

#### NOTE 2

### Surge Isolation Voltage

a. Definition:

This rating is used to protect against transient over-voltages generated from switching and lightning-induced surges. Devices shall be capable of withstanding this stress, a minimum of 100 times during its useful life. Ratings shall apply over entire device operating temperature range.

- b. Specification Format:
  - Specification, in terms of peak and/or RMS, 60 Hz voltage, of specified duration (e.g., 5656V<sub>peak</sub>/4000V<sub>RMS</sub> for one minute).
- e Test Conditions

Application of full rated 60 Hz sinusoidal voltage for one minute, with initial application restricted to zero voltage (i.e., zero phase), from a supply capable of sourcing 5mA at rated voltage.

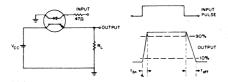
### Steady-State Isolation Voltage

a. Definition:

This rating is used to protect against a steady-state voltage which will appear across the device isolation from an electrical source during its useful life. Ratings shall apply over the entire device operating temperature range for a period of 10 minutes minimum.

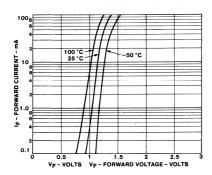
- b. Specification Format:
  - Specified in terms of D.C. and/or RMS 60 Hz sinusoidal waveform.
- c, Test Conditions:

Application of the full rated 60 Hz sinusoidal voltage, with initial application restricted to zero voltage (i.e., zero phase), from a supply capable of sourcing 5mA at rated voltage, for the duration of the test.

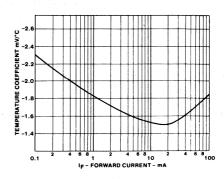


Adjust Amplitude of Input Pulse for Output (I<sub>C</sub>) of 2mA Test Circuit and Voltage Waveforms

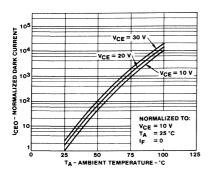
### TYPICAL CHARACTERISTICS



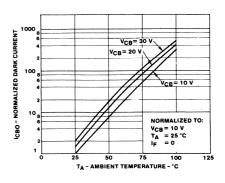
1. INPUT CHARACTERISTICS



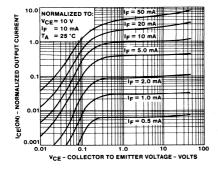
### 2. FORWARD VOLTAGE TEMPERATURE COEFFICIENT



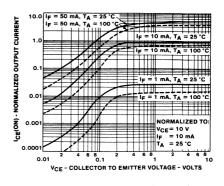
3. DARK I<sub>CEO</sub>CURRENT VS TEMPERATURE



4. I<sub>CBO</sub> VS TEMPERATURE



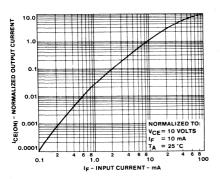
5. OUTPUT CHARACTERISTICS



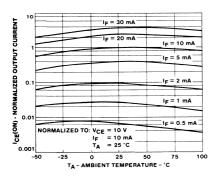
6. OUTPUT CHARACTERISTICS

# 14

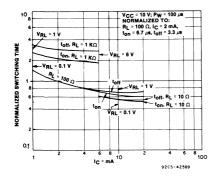
### TYPICAL CHARACTERISTICS



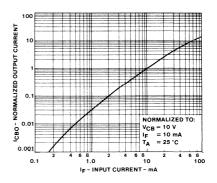
7. OUTPUT CURRENT VS INPUT CURRENT



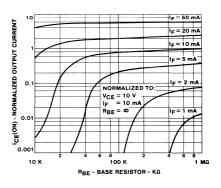
9. OUTPUT CURRENT VS TEMPERATURE



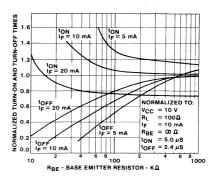
11. SWITCHING SPEED VS COLLECTOR CURRENT (NOT SATURATED)



8. OUTPUT CURRENT — COLLECTOR-TO-BASE VS INPUT CURRENT



10. OUTPUT CURRENT VS BASE EMITTER



12. SWITCHING TIME VS RBE

### GE3009-GE3012

# Optoisolator GaAs Infrared Emitting Diode and Light Activated Triac Driver

The GE3009-GE3012 series consists of a gallium arsenide, infrared emitting diode coupled with a light activated silicon bilateral switch, which functions like a triac, in a dual in-line package. These devices are also available in surface-mount packaging.

These devices are especially designed for triggering power triacs while maintaining dielectric isolation from the trigger control circuit.

# absolute maximum ratings: (25°C)

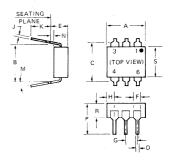
INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	50	milliamps
Forward Current (Peak)	3	amperes
(Pulse width 1 μsec. 300 pps)		
Reverse Voltage	3	volts
*Derate 1.33 mW/°C ab	ove 25°C ambier	nt.

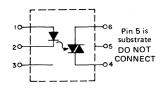
OUTPUT DRIVER		
Off-State Output Terminal Voltage	250	volts
On-State RMS Current	100	milliamps
(Full Cycle Sine Wave, 50 to 60 Hz)		
Peak Nonrepetitive Surge Current	1.2	amperes
(PW = 10 ms, DC = 10%) Total Power Dissipation @ T <sub>A</sub> = 25°C	**300	milliwatts
	3,	min watts
**Derate 4.0 mW/°C above	25°C.	

# TOTAL DEVICE Storage Temperature -55°C to +150°C Operating Temperature -49°C to +100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output) 5656 V<sub>(peak)</sub> 4000 V<sub>(RMS)</sub> Steady-State Isolation Voltage (Input to Output) 5300 V<sub>(peak)</sub> 3750 V<sub>(RMS)</sub>

Su Covered under U.L. component recognition program, reference file E51868







0.000	MILLIM	ETERS	INC	HES	NOTES
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
С	-	8.64		.340	2
D	.406	.508	.016	.020	
Е	-	5.08		.200	3
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
н	_	2.16	400	.085	4
J	.203	.305	.008	.012	
К	2.54		.100	-	
M	-	15	***	15	
N	.381		.015		
Р	-	9.53		.375	
R	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	

### NOTES

- INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES.

# individual electric characteristics (25°C)

EMITTER		SYMBOL	TYP.	MAX.	UNITS
Forward Voltage (I <sub>F</sub> = 10 mA)	(N)	V <sub>F</sub>	1.2	1.5	volts
Reverse Current $(V_R = 3V)$		I <sub>R</sub>	_	100	microamp
Capacitance (V = O, f = 1 MHz)		CJ	50	_	picofarads

DETECTOR See Note 1		SYMBOL	TYP.	MAX.	UNITS
Peak Off-State Current	$V_{DRM} = 250 \text{ V}$	I <sub>DRM</sub>	_	100	nanoamps
Peak On-State Voltage	$I_{TM} = 100 \text{ mA}$	$V_{TM}$	2.5	3.0	volts
Critical Rate-of-Rise of Off-State Voltage	$V_{in}$ = 30 $V_{(RMS)}$ (See Figure 1)	dv/dt	10.0		volts/µsec.
Critical Rate-of-Rise of Commutating Off-State Voltage	$I_{load} = 15 \text{ mA}$ $V_{in} = 30 V_{(RMS)}$ (See Figure 1)	dv/dt <sub>(C)</sub>	0.15		volts/μsec.
Critical Rate-of-Rise of Off-State Voltage	$V_{in}$ = 140 $V_{(RMS)}$ JEDEC conditions	dv/dt	6.0		volts/μsec.

# coupled electrical characteristics (25°C)

		SYMBOL	TYP.	MAX.	UNITS
IRED Trigger Current, Current Required to Latch Output	GE3009	I <sub>FT</sub>		30	milliamps
(Main Terminal Voltage = 3.0V, R <sub>L</sub> = 150 Ω)	GE3010	$I_{FT}$	_	15	milliamps
	GE3011	I <sub>FT</sub>	_	10	milliamps
	GE3012	$I_{FT}$		5	milliamps
Holding Current, Either Direction		I <sub>H</sub>	250	_	microamps

NOTE 1: Ratings apply for either polarity of Pin 6 — referenced to Pin 4.

Voltages must be applied within dv/dt rating.

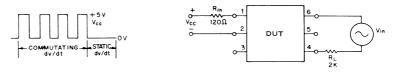


FIGURE 1. dv/dt — TEST CIRCUIT

### GE3020-GE3023

# **Optoisolator GaAs Infrared Emitting Diode and Light Activated Triac Driver**

The GE3020-GE3023 series consists of a gallium arsenide, infrared emitting diode coupled with a light activated silicon bilateral switch, which functions like a triac, in a dual in-line package. These devices are also available in surface-mount packaging.

These devices are especially designed for triggering power triacs while maintaining dielectric isolation from the trigger control circuit.



# absolute maximum ratings: (25°C)

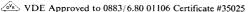
INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	50	milliamps
Forward Current (Peak)	3	amperes
(Pulse width 1 µsec. 300 pps)		_
Reverse Voltage	3	volts
*Derate 1.33 mW/°C ab	ove 25°C ambier	

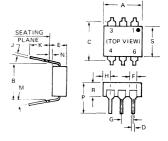
OUTPUT DRIVER		
Off-State Output Terminal Voltage	400	volts
On-State RMS Current	100	milliamps
(Full Cycle Sine Wave, 50 to 60 Hz)		_
Peak Nonrepetitive Surge Current	1.2	amperes
(PW = 10  ms, DC = 10%)		
Total Power Dissipation @ T <sub>A</sub> = 25°C	**300	milliwatts
••Derate 4.0 mW/°C above	25°C.	

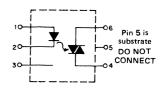
### **TOTAL DEVICE**

Storage Temperature -55°C to +150°C Operating Temperature -40°C to +100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output)  $5656\ V_{(peak)}$ 4000 V(RMS) Steady-State Isolation Voltage (Input to Output)  $5300\ V_{(peak)}$  $3750 \, V_{(RMS)}$ 

Na Covered under U.L. component recognition program, reference file E51868







SYMBOL	MILLIM	ETERS	INC	HES	NOTES
SYMBUL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
С		8.64	_	.340	2
D	.406	.508	.016	.020	
Ε	-	5.08	-	.200	3
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
н	-	2.16		.085	4
J	.203	.305	.008	.012	
к	2.54	_	.100	- '	
M		15		15	
N	.381		.015	-	
P	-	9.53	-	.375	
R	2.92	3.43	.115	.135	
s	6.10	6.86	.240	.270	

- INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES

# individual electric characteristics (25°C)

EMITTER	SYMBOL	TYP.	MAX.	UNITS
Forward Voltage	$V_{\rm F}$	1.2	1.5	volts
$(I_F = 10 \text{ mA})$		-		
Reverse Current	I <sub>R</sub>	_	100	microamp
$(V_R = 3V)$				
Capacitance	C <sub>J</sub>	50	_	picofarad
(V = O, f = 1 MHz)				

DETECTOR See Note 1		SYMBOL	TYP.	MAX.	UNITS
Peak Off-State Current	$V_{DRM} = 400 \text{ V}$	I <sub>DRM</sub>	_	100	nanoamps
Peak On-State Voltage	$I_{TM} = 100 \text{ mA}$	V <sub>TM</sub>	2.5	3.0	volts
Critical Rate-of-Rise of Off-State Voltage	$V_{in}$ = 30 $V_{(RMS)}$ (See Figure 1)	dv/dt	10.0	_	volts/µsec.
Critical Rate-of-Rise of Commutating Off-State Voltage	$I_{load}$ = 15 mA $V_{in}$ = 30 $V_{(RMS)}$ (See Figure 1)	dv/dt <sub>(C)</sub>	0.15	_	volts/µsec.
Critical Rate-of-Rise of Off-State Voltage	V <sub>in</sub> = 120 V <sub>(RMS)</sub> JEDEC conditions	dv/dt	6.0	_	volts/µsec.

# coupled electrical characteristics (25°C)

				MAX.	UNITS
IRED Trigger Current, Current Required to Latch Output	GE3020	I <sub>FT</sub>	_	30	milliamps
(Main Terminal Voltage = 3.0V, $R_L$ = 150 $\Omega$ )	GE3021	I <sub>FT</sub>	_	15	milliamps
	GE3022	I <sub>FT</sub>	-	10	milliamps
	GE3023	I <sub>FT</sub>		5	milliamps
Holding Current, Either Direction		I <sub>H</sub>	250	-	microamps
Holding Current, Either Direction		I <sub>FT</sub>	250	10 5 —	

NOTE 1: Ratings apply for either polarity of Pin 6 — referenced to Pin 4.

Voltages must be applied within dv/dt rating.

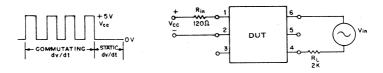


FIGURE 1. dv/dt - TEST CIRCUIT

### **GEPS2001**

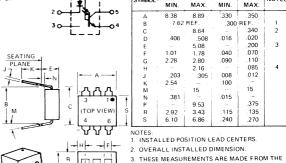
# **Optoisolator**

# GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The GEPS2001 is a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. This device is also available in surface-mount packaging.

# absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1µsec 300 P Ps)		
Reverse Voltage	5	volts
*Derate 1.33mW/°C above 2	5°C ambient	•



	P O O O O O O O O O O O O O O O O O O O
--	---

SEATING PLANE: 4. FOUR PLACES:

MILLIMETERS

INCHES

NOTES

PHOTO-TRANSISTOR		
Power Dissipation	**150	milliwatts
$V_{CEO}$	30	volts
$V_{CBO}$	70	volts
$V_{ECO}$	7	volts
Collector Current (Continuous)	100	milliamps
**Derate 2.0mW/°C above	25°C ambient.	

### TOTAL DEVICE

Storage Temperature -55 to 150°C
Operating Temperature -55 to 100°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output).

3535V(peak)
2500V(RMS)

# individual electrical characteristics (25°C)

1	INFRARED EMI	TTING DIODE	TYP.	MAX.	UNITS
	Forward Voltage (I <sub>F</sub> = 20mA)	$V_{\mathrm{F}}$	1.1	1.4	volts
	Reverse Current (V <sub>R</sub> = 4V)	$I_R$	_	20	microamps
	Capacitance (V = O,f = 1MH	C <sub>J</sub> z)	50	_	picofarads

PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage – V <sub>(BR)CEO</sub>	30	_		volts
$(I_C = 10 \text{mA}, I_F = 0)$				
Breakdown Voltage – V <sub>(BR)CBO</sub>	70	-		volts
$(I_C = 100\mu A, I_F = O)$				-
Breakdown Voltage – V <sub>(BR)ECO</sub>	7	-		volts
$(I_E = 100\mu A, I_F = O)$				
Collector Dark Current - I <sub>CEO</sub>	_	5	100	nanoamps
$(V_{CE} = 10V, I_F = 0)$				
DC Current Gain h <sub>FE</sub>	-	400	-	1
$(V_{CE}=5V, I_{C}=4mA)$				

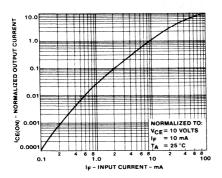
# coupled electrical characteristics (25°C)

	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio $(I_F = 20 \text{mA}, V_{CE} = 5 \text{V})$	30			%
Saturation Voltage – Collector to Emitter (I <sub>F</sub> = 20mA, I <sub>C</sub> = 2mA)		0.1	0.3	volts
Isolation Resistance (Input to Output Voltage = 1000V <sub>DC</sub> )	100	-	-	gigaohms
Input to Output Capacitance (Input to Output Voltage = O,f = 1MHz)		0.8	2	picofarads
Switching Speeds: Rise/Fall Time ( $V_{CE} = 10V$ , $I_{CE} = 2mA$ , $R_L = 100\Omega$ )	-	5	_	microseconds
Rise/Fall Time ( $V_{CB} = 10V$ , $I_{CB} = 50\mu A$ , $R_L = 100\Omega$ )	-	300	-	nanoseconds

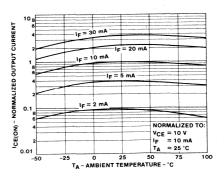
No Covered under U.L. component recognition program, reference file #E51868

### **GEPS2001**

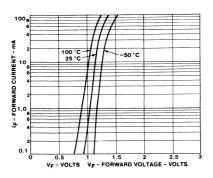
### TYPICAL CHARACTERISTICS



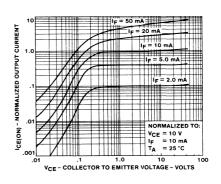
**OUTPUT CURRENT VS. INPUT CURRENT** 



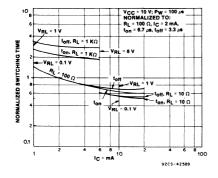
**OUTPUT CURRENT VS. TEMPERATURE** 



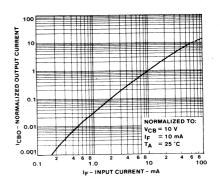
INPUT CHARACTERISTICS



**OUTPUT CHARACTERISTICS** 



SWITCHING SPEED VS COLLECTOR CURRENT (NOT SATURATED)



**OUTPUT CURRENT (ICBO) VS INPUT CURRENT** 

# Optoisolator GaAs Solid-State Lamp and NPN Silicon Phototransistor

The GFH600 consists of a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. This device is also available in surfacemount packaging.

### FEATURES:

- Fast switching speeds
- High DC current transfer ratio
- · High isolation resistance
- · High isolation voltage
- I/O compatible with integrated circuits

# absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE		
Power Dissipation - T <sub>A</sub>	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1µs, 300 P Ps)		
Reverse Voltage	6	volts
*Derate 1.33 mW/°C al	bove 25°C	

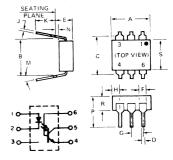
PHOTO-TRANSISTOR		
Power Dissipation - T <sub>A</sub>	**150	milliwatts
$V_{CEO}$	70	volts
$V_{CBO}$	70	volts
$V_{ECO}$	7	volts
Collector Current (Continuous)	150	milliamps
**Derate 2.0 mW/°C a	bove 25°C	-

### **TOTAL DEVICE**

Storage Temperature -55 to 150°C
Operating Temperature -55 to 100°C
Lead Soldering Time (at 260°C) 10 seconds
Surge Isolation Voltage (Input to Output).
4000V<sub>(peak)</sub> 2800V<sub>(RMS)</sub>

**VDE** Approved to 0883/6.80 0110b Certificate # 35025





SYMBOL	MILLIMETERS		INC	INCHES	
	MIN.	MAX.	MIN.	MAX.	NOTES
A	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
С		8.64		.340	2
D	406	.508	.016	.020	
E		5.08		.200	3
F	1.01	1.78	.040	.070	1
G	2.28	2.80	.090	.110	
н		2.16		.085	4
J	.203	.305	.008	.012	1
K	2.54		.100		
M		15		15	
N	.381		.015	İ	
Р		9.53		.375	
R	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	1

### NOTE

- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- 4. FOUR PLACES

# individual electrical characteristics (25°C) (unless otherwise specified)

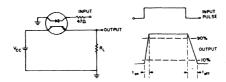
INFRARED EMITTING DIODE	MIN.	MAX.	UNITS
Forward Voltage – V <sub>F</sub> (I <sub>F</sub> = 60 mA)		1.65	volts
Reverse Current $-I_R$ ( $V_R = 3V$ )		10	microamps
Capacitance $-C_J$ (V = O,f = 1 MHz)	_	100	picofarads

PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage - V(BR)CEO	70	-	-	volts
$(I_C = 10 \text{mA}, I_F = 0)$	70			14
Breakdown Voltage – $V_{(BR)CBO}$ ( $I_C = 100\mu A, I_E = 0$ )	70	_	_	volts
Breakdown Voltage – V <sub>(BR)ECO</sub>	7		_	volts
$(I_F = 100\mu A, I_F = 0)$				
Collector Dark Current – I <sub>CEO</sub>	-	2	50	nanoamps
$(V_{CE} = 10V, I_F = 0)$ Capacitance - $C_{CE}$	_	2	_	picofarads
$(V_{CE} = 10V, f = 1 \text{ MHz})$		-		r

# coupled electrical characteristics (25°C) (unless otherwise specified)

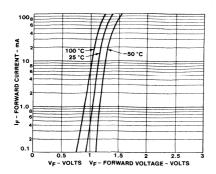
	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio (I <sub>F</sub> = 10mA, V <sub>CF</sub> = 5V)				
GFH600 I	63	_	125	%
GFH600 II	100		200	%
GFH600 III	160	-	320	%
Saturation Voltage – Collector to Emitter ( $I_F = 10mA$ , $I_C = 2.5mA$ )	_	-	0.3	volts
Isolation Resistance ( $V_{IO} = 500V_{DC}$ ) (See Note 1)	100	-	-	gigaohms
Input to Output Capacitance ( $V_{IO} = O,f = 1 \text{ MHz}$ ) (See Note 1)	_	_	2	picofarads
Turn-On Time $-t_{on}$ ( $V_{CC} = 10V$ , $I_C = 2mA$ , $R_L = 100\Omega$ ) (See Figure 1)	-	5	10	microseconds
Turn-Off Time – $t_{off}$ ( $V_{CC}$ = 10V, $I_C$ = 2mA, $R_L$ = 100 $\Omega$ ) (See Figure 1)	-	5	10	microseconds

Note 1: Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the output terminals (transistor) shorted together.

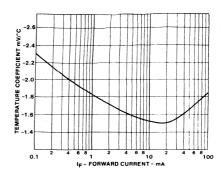


Adjust Amplitude of Input Pulse for Output (I<sub>C</sub>) of 2mA FIGURE 1 - TEST CIRCUIT AND VOLTAGE WAVEFORMS

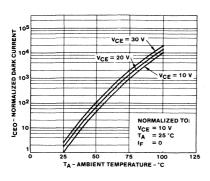
TYPICAL CHARACTERISTICS



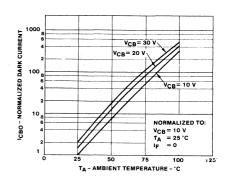
1. INPUT CHARACTERISTICS



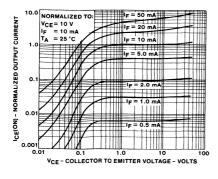
2. FORWARD CURRENT TEMPERATURE COEFFICIENT



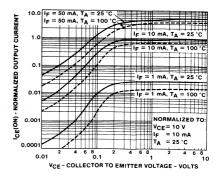
3. DARK ICEO CURRENT VS TEMPERATURE



4. ICBO VS TEMPERATURE

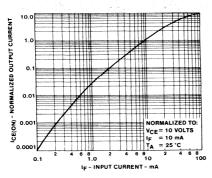


5. OUTPUT CHARACTERISTICS

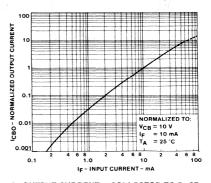


6. OUTPUT CHARACTERISTICS

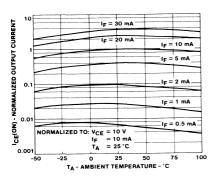
### TYPICAL CHARACTERISTICS



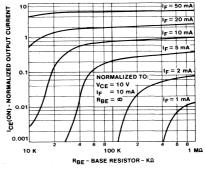
7. OUTPUT CURRENT VS INPUT CURRENT



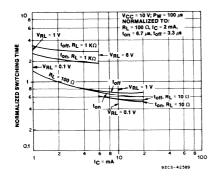
8. OUTPUT CURRENT — COLLECTOR TO BASE VS INPUT CURRENT



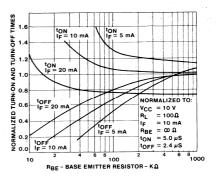
9. OUTPUT CURRENT VS TEMPERATURE



10. OUTPUT CURRENT VS BASE EMITTER RESISTANCE



11. SWITCHING SPEED VS COLLECTOR CURRENT (NOT SATURATED)



12. SWITCHING TIME VS RBE

# **Optoisolator**

# GaAs Solid-State Lamp and NPN Silicon Phototransistor

The GFH601 consists of a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. This device is also available in surfacemount packaging.

### **FEATURES:**

- · Fast switching speeds
- · High DC current transfer ratio
- · High isolation resistance
- · High isolation voltage
- I/O compatible with integrated circuits

# absolute maximum ratings: (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE		
Power Dissipation - T <sub>A</sub>	*100	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1µs, 300 P Ps)		
Reverse Voltage	6	volts
*Derate 1.33 mW/°C at	pove 25°C	

PHOTO-TRANSISTOR		
Power Dissipation - TA	**150	milliwatts
$V_{CEO}$	70	volts
V <sub>CBO</sub>	70	volts
V <sub>ECO</sub>	7	volts
Collector Current (Continuous)	150	milliamps
**Derate 2.0 mW/°C a	bove 25°C	

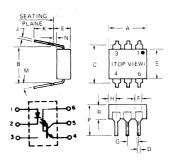
### TOTAL DEVICE

Storage Temperature -55 to 150°C Operating Temperature -55 to 100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output). 5300 V(peak) 3750 V(RMS)



VDE Approved to 0883/6.80 0110b Certificate # 35025 0883/0110/1172 Certificate # 30415 0883/0804/183 Certificate # 30415 0883/0806/8.81 Certificate # 30415





SYMBOL	MILLIM	ETERS	INC	INCHES	
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
A	8.38	8.89	.330	350	
В	7.62	REF.	.300	REF.	1
Č		8.64	-	.340	2
Ď.	.406	.508	016	.020	
Ē		5.08	118	.200	3
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
н		2.16		.085	4
J	,203	.305	.008	.012	i
K	2.54		.100	-	i
M		15		15	1
N	.381		.015	-	
Р		9.53	-	.375	1
R	2.92	3.43	.115	.135	
S	6.10	6.86	.240	.270	1

- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE
- 4. FOUR PLACES.



V<sub>883</sub> V<sub>DE</sub> APPROVED TO: V<sub>DE</sub> 0883/6.80 V<sub>DE</sub> 0110/11.72 V<sub>DE</sub> 0804/1.83 V<sub>DE</sub> 0806/8.81

CERTIFICATE #30415

# individual electrical characteristics (25°C) (unless otherwise specified)

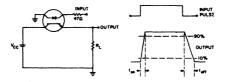
INFRARED EMITTING DIODE	MIN.	MAX.	UNITS
Forward Voltage - V <sub>F</sub> (I <sub>F</sub> = 60 mA)		1.65	volts
Reverse Current $-l_R$ ( $V_R = 6V$ )	-	10	microamps
Capacitance — C <sub>J</sub> (V = O <sub>3</sub> f = 1 MHz)	-	100	picofarads

PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage – $V_{(BR)CEO}$	70	_	-	volts
$(I_C = 10\text{mA}, I_F = 0)$ Breakdown Voltage $-V_{(BR)CBO}$	70	_	_	volts
$(I_C = 100\mu A, I_E = 0)$ Breakdown Voltage $-V_{(BR)ECO}$	7			volts
$(I_F = 100\mu A, I_F = 0)$			_	VOILS
Collector Dark Current – $I_{CEO}$ ( $V_{CE} = 10V, I_{E} = 0$ )	-	2	50	nanoamps
Capacitance - C <sub>CE</sub>	-	2		picofarads
$(V_{CE} = 10V, f = 1 MHz)$				

# coupled electrical characteristics (25°C) (unless otherwise specified)

			MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio (I <sub>F</sub> = 10mA, V <sub>CF</sub> = 5V)	FH601	I	40		80	%
( )	FH601	II	63		125	%
	FH601	III	100	_	200	%
	GFH601	IV	160	_	320	%
Saturation Voltage – Collector to Emitter ( $I_F = 10mA$ , $I_C = 2.5mA$ )			_	_	0.4	volts
Isolation Resistance ( $V_{IO} = 500V_{DC}$ ) (See Note 1)			100	- 1	-	gigaohms
Input to Output Capacitance $(V_{IO} = O, f = 1 \text{ MHz})$ (See Note 1)		1	-	-	2	picofarads
Turn-On Time $-t_{on}$ ( $V_{CC} = 10V$ , $I_C = 2mA$ , $R_L = 100\Omega$ ) (See Figure				5	10	microseconds
Turn-Off Time – $t_{off}$ ( $V_{CC}$ = 10V, $I_C$ = 2mA, $R_L$ = 100 $\Omega$ ) (See Figure	1)		_	5	10	microseconds

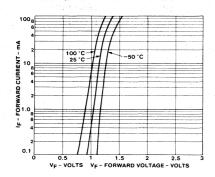
Note 1: Tests of input to output isolation current resistance, and capacitance are performed with the input terminals (diode) shorted together and the autput terminals (transistor) shorted together.



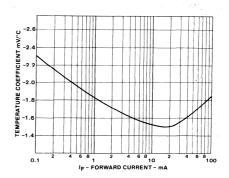
Adjust Amplitude of Input Pulse for Output (I<sub>C</sub>) of 2 mA

FIGURE 1

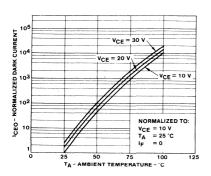
### TYPICAL CHARACTERISTICS



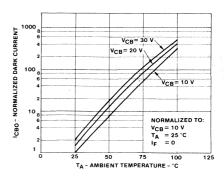
1. INPUT CHARACTERISTICS



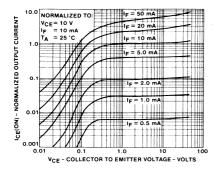
2. FORWARD VOLTAGE TEMPERATURE COEFFICIENT



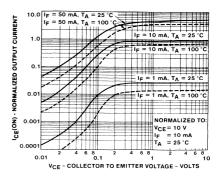
3. DARK ICEO CURRENT VS TEMPERATURE



4. I<sub>CBO</sub> VS TEMPERATURE

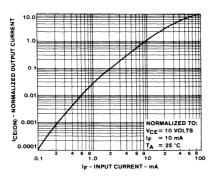


5. OUTPUT CHARACTERISTICS

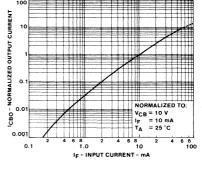


6. OUTPUT CHARACTERISTICS

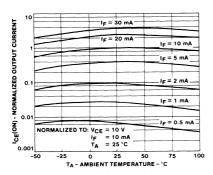
### TYPICAL CHARACTERISTICS



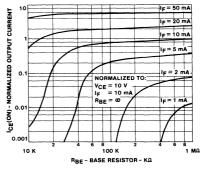
7. OUTPUT CURRENT VS INPUT CURRENT



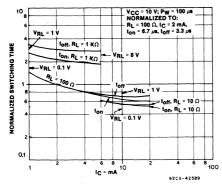
8. OUTPUT CURRENT - COLLECTOR TO BASE VS INPUT CURRENT



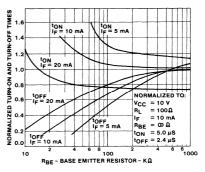
9. OUTPUT CURRENT VS TEMPERATURE



10. OUTPUT CURRENT VS BASE EMITTER RESISTANCE



11. SWITCHING SPEED VS COLLECTOR CURRENT (NOT SATURATED)



12. SWITCHING TIME VS RBE

# MCA230, MCA231, MCA255

# **Optoisolator**

# GaAs Infrared Emitting Diode and NPN Silicon Darlington-Connected Phototransistor

The MCA series consists of a gallium arsenide, infrared emitting diode coupled with a silicon photo-Darlington amplifier in a dual in-line package. These devices are also available in surface-mount packaging.

# absolute maximum ratings: (25°C)

74	
*100	milliwatts
60	milliamps
0.5	amperes
3	amperes
	volts
25°C ambier	ıt.
	0.5 3 3

		51
SEATING PLANE B M M 20 10 10 10 10 10 10 10 10 10 10 10 10 10	R G	NO <sup>-</sup> 1. I 2. (C 3. T S 4. F

SYMBOL	MILLIM	ETERS	INCHES		NOTES
3 TIVILLOL	MIN.	MAX.	MIN.	MAX.	NOTES
- A	8.38	8.89	.330	.350	
В	7.62	REF.	.300	REF.	1
С		8.64		.340	2
D	.406	.508	.016	.020	
Ε .		5.08		.200	3
F	1.01	1.78	.040	.070	
G	2.28	2.80	.090	.110	
H		2.16		.085	. 4
J	.203	.305	.008	.012	
K	2.54		.100		
M	- "	- 15		15	
N	.381	-	.015		ļ
Р	- 1	9.53	- '	.375	1
R	2.92	3.43	.115	.135	İ
S	6.10	6.86	.240	.270	1

1. INSTALLED POSITION LEAD CENTERS

- OVERALL INSTALLED DIMENSION.
   THESE MEASUREMENTS ARE MADE OF
- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE.
- ←D 4. FOUR PLACES.

DARLINGTON CONNECTED PHOTO-TRANSISTOR			
Power Dissipation	**210	milliwatts	
$V_{CEO} = MCA230/MCA231$	30	volts	
- MCA255	55	volts	
$V_{CBO}$ — MCA230/MCA231	30	volts	
— MCA255	55	volts	
$V_{EBO}$	8	volts	
Collector Current (Continuous)  — Forward  Collector Current (Continuous)	150	milliamps	
- Reverse	10	milliamps	
**Derate 2.8mW/°C above 25°C ambient.			

# TOTAL DEVICE

Storage Temperature -55°C to +150°C Operating Temperature -55°C to +100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output)

3550V<sub>(peak)</sub> 2500V<sub>(RMS)</sub> Steady-State Isolation Voltage (Input to Output)

 $3180V_{(peak)}$  2250 $V_{(RMS)}$ 

# individual electrical characteristics: (25°C)

EMITTER	TYP.	MAX.	UNITS
Forward Voltage $V_F$ $(I_F = 20\text{mA})$	1.1	1.5	volts
Reverse Current $I_R$ $(V_R = 3V)$	1-1	10	microamps
Capacitance $C_J$ (V = 0, f = 1MHz)	50		picofarads

MIN.	TYP.	MAX.	UNITS
55	-	_	volts
30	-	<b>—</b>	volts
55	_	_	volts
30	_	<b> </b> —	volts
8	-		volts
		1	
ļ		l	
_	-	100	nanoamp
	55 30 55 30	55 — 30 — 55 — 30 —	55 30 55 30

# coupled electrical characteristics: (25°C)

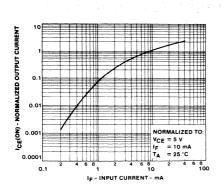
		MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio — $(I_F = 10\text{mA}, V_{CE} = 5\text{V})$	MCA230/MCA255	100		_	%
	MCA231	200		_	%
Saturation Voltage — Collector to Emitter — $(I_F = 50 \text{mA}, I_C = 50 \text{mA})$	MCA230/255	_	_	1.0	volts
$-(I_F = 1mA, I_C = 2mA)$	MCA231		-	1.0	volts
$-(I_F = 5mA, I_C = 10mA)$	MCA231	_		1.0	volts
$-(I_F = 10mA, I_C = 50mA)$	MCA231	1	_	1.2	volts
Isolation Resistance (Input to Output Voltage = $500V_{DC}$ )		100	-	-	gigaohms
Input to Output Capacitance (Input to Output Voltage = $0$ , $f = 1MHz$ )		_	-	2	picofarads
Switching Speeds:					-
On-Time $- (V_{CE} = 5V, R_L = 100\Omega, I_F = 10\text{mA})$		_	5		microseconds
Off-Time — (Pulse width $\leq 300\mu \text{sec}$ , $f \leq 30\text{HZ}$ )		_	100	-	microseconds

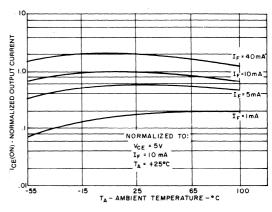
Covered under U.L. component recognition program, reference file E51868

VDE Approved to 0883/6.80 0110b Certificate #35025, except type 4N38A

# MCA230, MCA231, MCA255

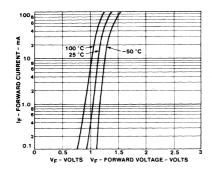
### TYPICAL CHARACTERISTICS

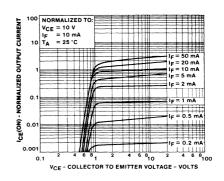




### 1. OUTPUT CURRENT VS. INPUT CURRENT

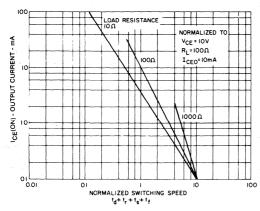
2. OUTPUT CURRENT VS. TEMPERATURE

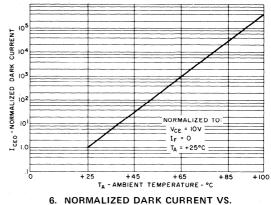




### 3. INPUT CHARACTERISTICS

4. OUTPUT CHARACTERISTICS





5. SWITCHING SPEED VS. OUTPUT CURRENT

6. NORMALIZED DARK CURRENT VS TEMPERATURE

### MCS2, MCS2400

# **Optoisolator**

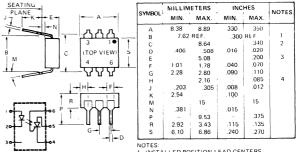
# GaAs Infrared Emitting Diode and Light Activated SCR

The MCS2 and MCS2400 consist of a gallium arsenide. infrared emitting diode coupled with a light activated silicon controlled rectifier in a dual in-line package. These devices are also available in surface-mount packaging.

# absolute maximum ratings

INFRARED EMITTING DIODE		2.0
Power Dissipation	*100	milliwatts
Forward Current (Continous)	60	milliamps
Forward Current (Peak)	1	ampere
(100μsec 1% duty cycle)		
Reverse Voltage	3	volts
*Derate 1.33mW/°C above	25°C ambient.	

PHOTO-SCR			
Off-State and Reverse Voltage	MCS2	200	volts
	MCS2400	400	volts
Peak Reverse Gate Voltage		6	volts
Direct On-State Current		300	milliamps
Surge (non-rep) On-State Curre	nt	10	amps
Peak Gate Current		10	milliamps
Output Power Dissipation		**400	milliwatts
**Derate 5.3mW/°C	above 25°C a	mbient.	



- 1. INSTALLED POSITION LEAD CENTERS.
- 2. OVERALL INSTALLED DIMENSION.
- 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE. 4. FOUR PLACES.

### **TOTAL DEVICE**

Storage Temperature Range — 55°C to 150°C Operating Temperature Range —  $55^{\circ}$ C to  $100^{\circ}$ C Soldering Temperature (1/16" from case, 10 seconds) 260°C Total Device Dissipation 450 milliwatts Linear Derating Factor (above 25°C) 6.0mW/°C Surge Isolation Voltage (Input to Output). 3535V<sub>(peak)</sub>

2500 V(RMS) Steady-State Isolation Voltage (Input to Output).  $3180V_{(peak)}$ 2250V(RMS)

# individual electrical characteristics (25°C) (unless otherwise specified)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage V <sub>F</sub> (I <sub>F</sub> = 20mA)	1.1	1.5	V
Reverse Current $I_R$ $(V_R = 3V)$	. <del></del>	10	μΑ
Capacitance $C_J$ (V = 0, f = 1MHz)	50	OFFicial	pF

PHOTO-SCR		MIN.	MAX.	UNITS
Peak Off-State Voltage — V <sub>DM</sub>	MCS2	200		V
$R_{GK} = 10K\Omega$ , $T_A = 100^{\circ}C$ , $I_D = 150\mu A$ )	MCS2400	400	-	V
Peak Reverse Voltage — V <sub>RM</sub>	MCS2	200	l –	V
$(T_A = 100 ^{\circ}\text{C}, I_R = 150 \mu\text{A})$	MCS2400	400	_	V
On-State Voltage — V <sub>T</sub>		-	1.3	V
$(I_T = 100 \text{mA})$			l	
Off-State Current — I <sub>D</sub>	MCS2	_	2	μA
$(V_D = 200V, I_F = 0, R_{GK} = 27K)$		l		
Off-State Current — I <sub>D</sub>	MCS2400		2	μΑ
$(V_D = 400V, I_F = 0, R_{GK} = 27K)$				
Reverse Current — I <sub>R</sub>	MCS2	-	2	μΑ
$(V_R = 200V, I_F = 0)$				
Reverse Current — I <sub>R</sub>	MCS2400		2	μΑ
$(V_R = 400V, I_F = 0)$				
Holding Current — I <sub>H</sub>		10	500	μΑ
$(V_{FX} = 50V, R_{GK} = 27K\Omega)$		l		

# coupled electrical characteristics (25°C)

	MIN.	MAX.	UNITS
Input Current to Trigger			
$V_{AK} = 100V, R_{GK} = 27K\Omega$ $I_{FT}$	.5	14	milliamps
Isolation Resistance (Input to Output) $V_{io} = 500V_{DC}$ $r_{io}$	100		gigaohms
Turn-On Time – $V_{AK} = 50V$ , $I_F = 30mA$ , $R_{GK} = 10K\Omega$ , $R_L = 200\Omega$		50	microseconds
Coupled dv/dt, Input to Output	500		volts/microsec.
Input to Output Capacitance (Input to Output Voltage = 0, f = 1MHz)	-	2	picofarads

Covered under U.L. component recognition program, reference file E51868 VDE Approved to 0883/6.80 0110b Certificate #35025, except type 4N28

### 15

### TYPICAL CHARACTERISTICS

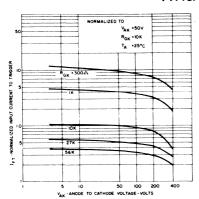


FIGURE 1. INPUT CURRENT TO TRIGGER VS. ANODE-CATHODE VOLTAGE

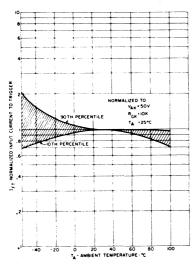


FIGURE 3. INPUT CURRENT TO TRIGGER DISTRIBUTION VS. TEMPERATURE

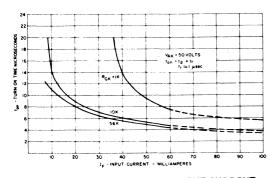


FIGURE 5. TURN-ON TIME VS. INPUT CURRENT

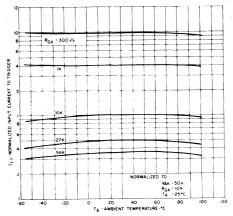


FIGURE 2. INPUT CURRENT TO TRIGGER VS. TEMPERATURE

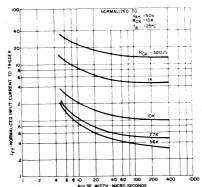


FIGURE 4. INPUT CURRENT TO TRIGGER
VS. PULSE WIDTH

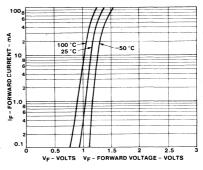


FIGURE 6. INPUT CHARACTERISTICS

IF VS. VF

### MCS21, MCS2401

### **Optoisolator**

### GaAs Infrared Emitting Diode and Light Activated SCR

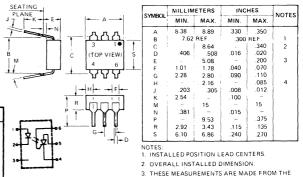
The MCS21 and MCS2401 consist of a gallium arsenide, infrared emitting diode coupled with a light activated silicon controlled rectifier in a dual in-line package. These devices are also available in surface-mount packaging.

■ Covered under U.L. component recognition program, reference file E51868

### absolute maximum ratings

INFRARED EMITTING DIODE		
Power Dissipation	*100	milliwatts
Forward Current (Continous)	60	milliamps
Forward Current (Peak)	1	ampere
(100 μsec 1 % duty cycle)		-
Reverse Voltage	3	volts
*Derate 1 33mW/°C above 25°C	'ambient	

PHOTO-SCR			
Off-State and Reverse Voltage	MCS21	200	volts
_	MCS2401	400	volts
Peak Reverse Gate Voltage		6	volts
Direct On-State Current		300	milliamps
Surge (non-rep) On-State Curre	ent	10	amps
Peak Gate Current		10	milliamps
Output Power Dissipation		**400	milliwatts
**Derate 5.3mW/°C	above 25°C a		



### TOTAL DEVICE

Storage Temperature Range — 55°C to 150°C
Operating Temperature Range — 55°C to 100°C
Soldering Temperature (1/16" from case, 10 seconds) 260°C
Total Device Dissipation 450 milliwatts
Linear Derating Factor (above 25°C) 6.0mW/°C
Surge Isolation Voltage (Input to Output).

4000 V<sub>(peak)</sub> 3000 V<sub>(RMS)</sub>
Steady-State Isolation Voltage (Input to Output).

3500 V<sub>(peak)</sub> 2500V<sub>(RMS)</sub>

SEATING PLANE. 4. FOUR PLACES

### individual electrical characteristics (25°C) (unless otherwise specified)

1	INFRARED EMITTING DIODE	TYP.	MAX.	UNITS	
	Forward Voltage V <sub>F</sub> (I <sub>F</sub> = 20mA)	1.1	1.5	V	
	Reverse Current I <sub>R</sub> (V <sub>R</sub> = 3V)		10	μΑ	
	Capacitance $C_j$ (V = 0, f = 1MHz)	50	_	pF	

PHOTO-SCR		MIN.	MAX.	UNITS
Peak Off-State Voltage — V <sub>DM</sub>	MCS21	200	_	V
$R_{GK} = 10K\Omega$ , $T_A = 100$ °C, $I_D = 150\mu A$ )	MCS2401	400	-	V
Peak Reverse Voltage — V <sub>RM</sub>	MCS21	200	-	V
$(T_A = 100 ^{\circ}\text{C}, I_R = 150 \mu\text{A})$	MCS2401	400		V
On-State Voltage — V <sub>T</sub>		_	1.3	V
$(I_T = 100 \text{mA})$				
Off-State Current — ID	MCS21		2	μA
$(V_D = 200V, I_F = 0, R_{GK} = 27K)$				
Off-State Current — ID	MCS2401	_	2	μΑ
$(V_D = 400V, I_F = 0, R_{GK} = 27K)$			1	
Reverse Current — I <sub>R</sub>	MCS21	_	2	μΑ
$(V_R = 200V, I_F = 0)$				
Reverse Current — I <sub>R</sub>	MCS2401		2	μA
$(V_R = 400V, I_F = 0)$			l	
Holding Current — I <sub>H</sub>		10	500	μΑ
$(V_{FX} = 50V, R_{GK} = 27K\Omega)$				

### coupled electrical characteristics (25°C)

	MIN.	MAX.	UNITS
Input Current to Trigger $V_{AK}$ =50V, $R_{GK}$ =10K $\Omega$		20	milliamps
$V_{AK} = 100V, R_{GK} = 27K\Omega$ $I_{FT}$	.5	11.	milliamps
Isolation Resistance (Input to Output) $V_{io} = 500V_{DC}$ $r_{io}$	100	-	gigaohms
Turn-On Time - $V_{AK} = 50V$ , $I_F = 30mA$ , $R_{GK} = 10K\Omega$ , $R_L = 200\Omega$		50	microseconds
Coupled dv/dt, Input to Output	500	_	volts/microsec.
Input to Output Capacitance (Input to Output Voltage = 0, f = 1MHz)	_	2	picofarads

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### TYPICAL CHARACTERISTICS

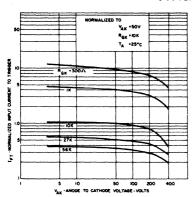


FIGURE 1. INPUT CURRENT TO TRIGGER VS. ANODE-CATHODE VOLTAGE

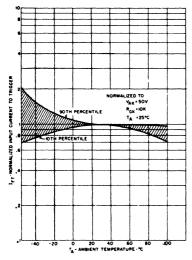


FIGURE 3. INPUT CURRENT TO TRIGGER DISTRIBUTION VS. TEMPERATURE

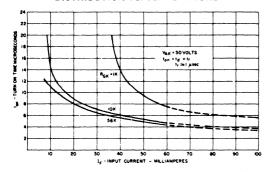


FIGURE 5. TURN-ON TIME VS. INPUT CURRENT

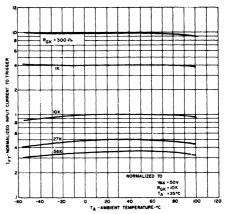


FIGURE 2. INPUT CURRENT TO TRIGGER VS. TEMPERATURE

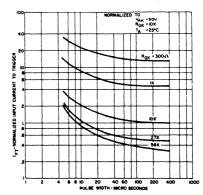


FIGURE 4. INPUT CURRENT TO TRIGGER
VS. PULSE WIDTH

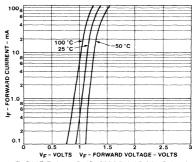


FIGURE 6. INPUT CHARACTERISTICS I<sub>F</sub> VS. V<sub>F</sub>

15

### MCT2, MCT2E, MCT26

### **Optoisolator**

### **GaAs Infrared Emitting Diode and NPN Silicon Phototransistor**



NOTES

3

The MCT2, MCT2E and MCT26 are gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. These devices are also available in surface-mount packaging.

### absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*200	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1µsec 300 P Ps)		-
Reverse Voltage	3	volts
*Derate 2.6mW/°C above 25°	C ambient.	

PHOTO-TRANSISTOR		
Power Dissipation	**200	milliwatts
$V_{ m CEO}$	30	volts
$V_{CBO}$	70	volts
$V_{ECO}$	7	volts
Collector Current (Continuous)	100	milliamps
**Derate 2.6mW/°C above 2	25°C ambient.	

#### MILLIMETERS MIN. MAX. 8.38 8 89 .350 300 340 .016 .020 508 1.01 040 070 .085 381 .015 .375 6.10 240 1. INSTALLED POSITION LEAD CENTERS 2. OVERALL INSTALLED DIMENSION.

- THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE
  - 4. FOUR PLACES

### TOTAL DEVICE

Storage Temperature -55 to 150°C Operating Temperature -55 to 100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output).

> $3500V_{(peak)}$ 2500V<sub>(RMS)</sub>

### individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage V <sub>F</sub> (I <sub>F</sub> = 10mA)	1.1	1.5	volts
Reverse Current $I_R$ $(V_R = 3V)$	-	10	microamps
Capacitance C <sub>J</sub> (V = O,f = 1MHz)	50	-	picofarads

MIN.	TYP.	MAX.	UNITS
30			volts
70		-	volts
		•	
7	-		volts
-	5	50	nanoamps
	İ	1	
-	2	-	picofarads
	30 70	30	30 70 7

### coupled electrical characteristics (25°C)

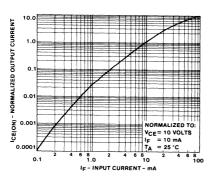
		MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_f = 10 \text{mA}$ , $V_{CE} = 10 \text{V}$ )	MCT2 — MCT2E	20		_	%
	MCT26	6	_	_	%
Saturation Voltage — Collector to Emitter	¥ ,				
$(I_F = 16mA, I_C = 2.0mA)$	MCT2 - MCT2E	-	0.1	0.4	volts
Saturation Voltage — Collector to Emitter ( $I_F = 60 \text{mA}$ , $I_C = 1$	.6mA) MCT26	-		0.5	volts
Isolation Resistance (Input to Output Voltage = $500V_{DC}$ )		100	_	-:-	gigaohms
Input to Output Capacitance (Input to Output Voltage = 0, f =	1MHz)	-	_	2	picofarads
Switching Speeds: Rise/Fall Time ( $V_{CE} = 10V$ , $I_{CE} = 2mA$ , R	$L = 100\Omega$ )	_	5	-	microseconds
Rise/Fall Time ( $V_{CB} = 10V$ , $I_{CB} = 50\mu A$ , F	$L_{\rm L} = 100\Omega$ )		3		microseconds

No Covered under U.L. component recognition program, reference file E51868

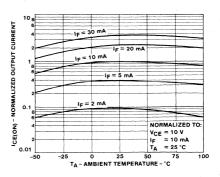


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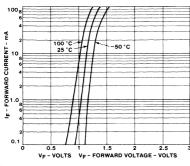
### TYPICAL CHARACTERISTICS



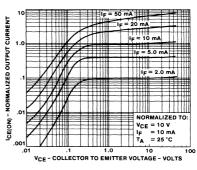
**OUTPUT CURRENT VS INPUT CURRENT** 



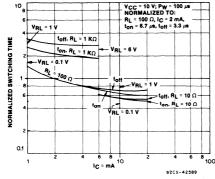
**OUTPUT CURRENT VS TEMPERATURE** 



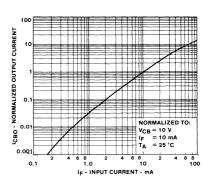
INPUT CHARACTERISTICS



**OUTPUT CHARACTERISTICS** 



SWITCHING SPEED VS. COLLECTOR CURRENT (NOT SATURATED)



OUTPUT CURRENT (ICBO) VS INPUT CURRENT

15

### **MCT210**

### **Optoisolator**

GaAs Infrared Emitting Diode and NPN Silicon Phototransistor

The MCT210 is a gallium arsenide, infrared emitting diode coupled with a silicon phototransistor in a dual in-line package. This device is also available in surface-mount packaging.

Na Covered under U.L. component recognition program, reference file E51868

### absolute maximum ratings: (25°C)

INFRARED EMITTING DIODE		
Power Dissipation	*200	milliwatts
Forward Current (Continuous)	60	milliamps
Forward Current (Peak)	3	ampere
(Pulse width 1 μsec 300 P Ps)		
Reverse Voltage	3	volts
*Derate 2.6mW/°C above 3	25°C ambient.	•

PHOTO-TRANSISTOR		
Power Dissipation	**200	milliwatts
$V_{CEO}$	30	volts
$V_{CBO}$	70	volts
$V_{ECO}$	7	volts
Collector Current (Continuous)	100	milliamps
**Derate 2.6mW/°C above 25	5°C ambient.	•

#### MILLIMETERS INCHES SYMBOL NOTES MIN. MAX MAX MIN 8.89 330 .350 7.62 REF 8.64 2 406 .016 3 5.08 .200 1.78 2.28 .090 110 2.16 വാ 012 15 .015 9.53 375 115 3 43 135 NOTES 1. INSTALLED POSITION LEAD CENTERS OVERALL INSTALLED DIMENSION. 3. THESE MEASUREMENTS ARE MADE FROM THE SEATING PLANE 4 FOUR PLACES

### TOTAL DEVICE

Storage Temperature -55 to 150°C Operating Temperature -55 to 100°C Lead Soldering Time (at 260°C) 10 seconds Surge Isolation Voltage (Input to Output).

 $\begin{array}{ccc} 3535V_{(peak)} & 2500V_{(RMS)} \\ Steady-State I solation Voltage \ (Input to Output). \\ & 3180V_{(peak)} & 2250V_{(RMS)} \end{array}$ 

### individual electrical characteristics (25°C)

INFRARED EMITTING DIODE	TYP.	MAX.	UNITS
Forward Voltage $V_F$ $(I_F = 40 \text{mA})$	1.1	1.5	volts
Reverse Current $I_R$ $(V_r = 6V)$	-	10	microamps
Capacitance C <sub>J</sub> (V = O,f = 1 MHz)	50	_	picofarads

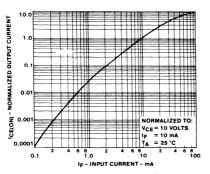
PHOTO-TRANSISTOR	MIN.	TYP.	MAX.	UNITS
Breakdown Voltage-V <sub>(BR)CEO</sub>	30	_	-	volts
(I <sub>C</sub> = 10mA, I <sub>F</sub> = 0)	70		_ '	volts
Breakdown Voltage- $V_{(BR)CBO}$ ( $I_C = 100\mu A, I_F = O$ )	,,,			VOILS
Breakdown Voltage- $V_{(BR)ECO}$ ( $I_E = 100\mu A, I_F = O$ )	،6	-	-	volts
$(I_E = 100\mu A, I_F = 0)$ Collector Dark Current- $I_{CEO}$	_	. 5	50	nanoamps
$(V_{CE} = 10V, I_F = O)$		2		mino Como do
Capacitance $(V_{CE} = 10V, f = 1MHz)$	_	2	_	picofarads

### coupled electrical characteristics (25°C)

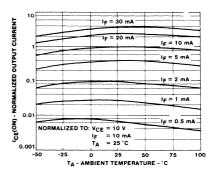
	MIN.	TYP.	MAX.	UNITS
DC Current Transfer Ratio ( $I_F = 3.2 \text{mA}$ to $32 \text{mA}$ , $V_{CE} = 0.4 \text{V}$ )	50	_	_	%
$(I_F = 10\text{mA}, V_{CE} = 5\text{V})$	150	l –		%
Saturation Voltage — Collector to Emitter ( $I_F = 32\text{mA}$ , $I_C = 16\text{mA}$ )	-	0.1	0.4	volts
Isolation Resistance (Input to Output Voltage = 500V <sub>DC</sub> )	100			gigaohms
Input to Output Capacitance (Input to Output Voltage = 0, f = 1MHz)			2	picofarads
Switching Speeds: Rise/Fall Time ( $V_{CE} = 10V$ , $I_{CE} = 2mA$ , $R_L = 100\Omega$ )	_	5	_	microseconds
Rise/Fall Time ( $V_{CB} = 10V$ , $I_{CB} = 50\mu A$ , $R_L = 100\Omega$ )	-	300	_	nanoseconds

VDE Approved to 0883/6.80 0110b Certificate # 35025

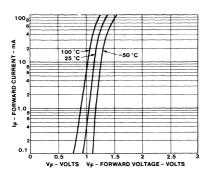
### TYPICAL CHARACTERISTICS



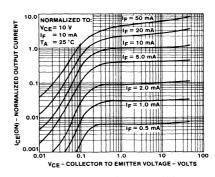
**OUTPUT CURRENT VS INPUT CURRENT** 



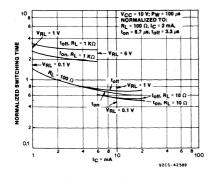
**OUTPUT CURRENT VS TEMPERATURE** 



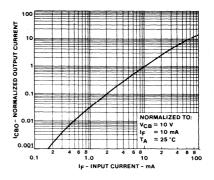
INPUT CHARACTERISTICS



V<sub>CE</sub>- COLLECTOR TO EMITTER VOLTAGE - VOLTS
OUTPUT CHARACTERISTICS



SWITCHING SPEED VS. COLLECTOR CURRENT (NOT SATURATED)



OUTPUT CURRENT (ICBO) VS INPUT CURRENT

15

。 [1] · 阿勒尔克·维纳克·克德克克·伊斯克

# **Application Notes**

Noise-Immune Optoisolator Improves	
Circuit Performance at Low Cost	404
Common-Drain Power-MOSFET Gate-Drive	
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# Noise-Immune Optoisolator Improves Circuit Performance at Low Cost

by W. H. Sahm

#### Introduction

Immunity from common-mode noise and elimination of unwanted signals by isolation are two problems faced by circuit designers in achieving desired circuit performance. Traditional design methods of rejecting common-mode noise, including optoisolation, have proved costly and complex, and normally even limit performance. But now the H11N, a Schmitt-trigger optoisolator, offers a low-cost, flexible solution to ground loop and noise problems common in logic and power-control systems. The H11N performs logic isolation at frequencies 8 to 10 times greater than other Schmitt-trigger devices. It comes in a low-cost six-pin DIP package and surpasses competitive optoelectronic devices in its compatiblity with power supplies, which can range from 4V to 15V. Potential uses fro the high-speed H11Ninclude data-bus/LAN isolation, square-wave shaping, line receivers, and voltage-level shifting for power MOSFET gate drive in switching power supplies.

#### **General Considerations**

Immunity from common-mode noise and elimination of unwanted signals by isolation are two problems circuit designers face in achieving desired circuit performance.

One example of common-mode noise is the 60-Hz signal induced on a pair of signal-acquisition wires by nearby power lines. Voltage transients on the line caused by reactive load switching, lightning, and static discharge add to the problem. Another example is the half-bridge power-switch configuration, in which the control circuits of the top power switch rise and fall hundreds of volts, with relation to signal ground, in sub-microsecond times. In each case, resultant noise can overwhelm the common-mode rejection capability of the signal-acquisition circuitry and reduce performance.

Traditional methods of eliminating these unwanted signals, or at least attenuating them to a reasonable level, have included isolation amplifiers, transformer coupling, fiberoptic signal transmission and optoisolators. Some of these methods prove costly and complex, however, and most also limit performance. The isolation amplifier, for example, requires a floating, isolated power supply for input bias, has limited bandwidth, and is expensive. Transformer coupling is less costly, but trades off isolation and bandwidth and cannot transmit dc. Fiber-optic transmission provides the ultimate in isolation and bandwidth capability, but is also costly and, to date, hard to deal with in a manufacturing environment. The optoisolator — a miniature fiber-optic system in a single package — has shown great promise in approaching the potential performance of fiber optics, but until recently has not been able to provide both wide bandwidth and high common-mode rejection at low signal levels for a reasonable price.

All this has changed, however, with the introduction of the Schmitt-trigger-output optoisolators in the H11N series.

#### The H11N

The H11N, shown in Fig. 1, comes with a high-speed IRED (infrared emitting diode) coupled to a custom-designed optical input, Schmitt-trigger integrated circuit. It is designed to prove logic isolation at frequencies 8 to 10 times greater than those associated with other Schmitt-trigger devices. The H11N is manufactured in a standard six-pin DIP package with glass dielectric isolation. It has

typical rise and fall times of 10 ns with propagation delays of 150 ns typically and 330 ns maximum, providing sensitivity and noise immunity.

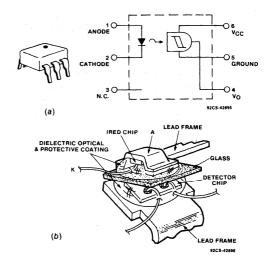


Fig. 1 - (a) Package and functional diagram, (b) internal construction.

The output Schmitt-trigger monolithic IC has an open collector output rated at 50 mA that sinks 20 mA to less than 0.5V, and operates from 4 to 15V. The circuit requires little power-supply current, typically drawing 5 mA at 5V for the output IC, while requiring only about 2 mA IRED drive to switch the output on. The output integrated circuit design incorporates a regulated power supply for low-level handling and Schmitt-trigger hysterisis (typically 20 percent) for switching. These properties of the H11N eliminate the possibility of oscillation at any combination of bias or temperature throughout the operating range. The IC also incorporates temperature compensation for changes in IRED efficiency, and parameters are specified over the entire 0 to 70°C temperature range. Fig. 2 shows a schematic and timing waveforms for the H11N.

The excellent common-mode noise rejection of the H11N is assured by a combination of IC circuit design and glass dielectric construction. The widely-spaced, high-illumination package construction lowers gain requirements, while the "upside-down" photodiode provides its own shield. When measured (using the industry standard of a 50V pulse between input and output), a dv/dt exceeding 10,000 V/ $\mu$ s normally is required to cause an upset of the output state. The H11N has a 3000 V/ $\mu$ s capability to handle pulses of 250V and higher, illustrating high-voltage performance.

This variation of rejection capability with voltage is the result of the combined effect of detector response time and common-mode pulse transition time. The transient-generated "noise triggering" of the IC is caused by currents

Fig. 2 - H11N schematic diagram and timing waveforms.

capacitively coupled into the detector, which are proportional to common-mode dv/dt. The detector has a propagation delay that is only slightly affected by the magnitude of current. The rise time of the low-amplitude transients is shorter than the response time of the detector, so no response will be noted.

As transient amplitude increases, the detector responds at lower dv/dt values until a limiting value of dv/dt is reached that is independent of the transient amplitude for a given bias condition. For the H11N series, the common-mode transient immunity is roughly constant for transients of 250V and up. A survey of other optoisolator specifications

shows that only devices with internal Faraday shields provide this same data, and that assessment of their true capability can be done with voltage amplitudes of 400V H11N common-mode rejection performance is therefore equivalent to or better than most other isolation devices with expensive Faraday shields. Fig. 3 illustrates H11N common-mode transient immunity.

Careful circuit layout also is crucial to maintaining good common-mode transient immunity. The small size of the H11N six-pin DIP package minimizes problems of parasitic capacitance in wiring layouts that induce transient-generated voltages into signal lines.

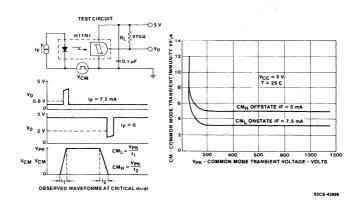


Fig. 3 - H11N common-noise transient immunity.

### **Circuit Performance**

What does all this mean in terms of circuit performance? Consider a twisted-pair data line that carries information between an "island of automation" on the factory floor and a central controller, Fig. 4. As the #22 twisted-pair data line runs in the vicinity of, and often parallel to, power lines, high-amplitude common-mode signals are induced into the data line. In addition, individual data lines often originate or terminate in close proximity to the power switches that both generate switching transients and carry high currents that cause "ground loop" common-mode signals.

System wiring costs can be minimized by sending relatively high-rate serial data on low-cost twisted-pair lines in a half-duplex arrangement. Better noise immunity can be obtained with shielded pairs, coaxial cable and, ultimately, fiber optics, at a progressively higher cost. In such cases where substantial distance runs are required (as in factory automation), wiring costs can be the largest single hardware investment in the information-distribution system. Substantial savings can be obtained, however, through the use of low-cost cabling if the cabling is combined with optically isolated termination to avoid degrading noise performance.

#### Optoisolator As Line Receiver

The normal method of optical line isolation involves the use of the optoisolator as a line receiver. In this configuration, the two-terminal input of the IRED interfaces easily with the two-terminal line. Data-transmission rates are maintained to

the limit of the system and isolation is the full responsibility of the optoisolator.

Often, the limiting factor in this type of data link is the optoisolator's common-mode rejection capability. Transients can be coupled into the transmission system electromagnetically, electrostatically, or through conduction. The worst transients are caused by high-power switching (high dv/dt, high amplitude), induced lightning strikes (moderate dv/dt, ultra-high amplitude), noise coupled in from digital systems, or switching power supplies (ultra high dv/dt, low amplitude). When fast optoisolators became available, it was thought they would solve the common-mode noise problems that plagued line receivers. Although optoisolation helped, the degree of improvement was limited, and many designers became disillusioned with the system due to the trade-offs necessary for suitable data-bus isolation.

Those early optoisolators, like the 6N137, were constructed with fast, low-efficiency, infra-red diodes and compensated for low light emission by using very thin isolation spacing and high-gain detector circuity. This combination provided poor common-mode noise immunity, and circuits would commonly be upset by the transient voltages from relays, switch-mode power supplies and similar sources. The H11N, however, uses a higher-efficiency IRED, 0.2-mm glass isolation, feedback gain control, integrated photodiode shielding, and Schmitt-trigger circuitry that significantly improves common-mode noise immunity. It can typically withstand more than 10,000 V/ $\mu$ s, which even exceeds the capability of many power-MOSFET switching circuits. Fig. 5 shows a simple, isolated line-receiver diagram that illustrates common-mode noise.

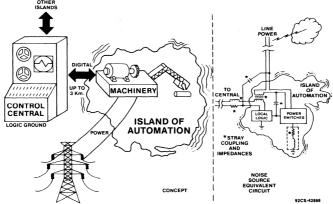


Fig. 4 - Typical factory automation-control system.

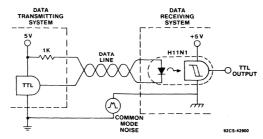


Fig. 5 - Simple isolated line receiver illustrating commonmode noise.

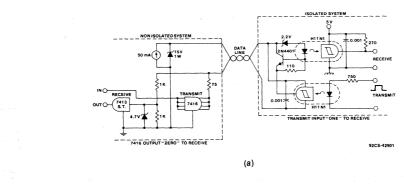
### Normally, datacom links require isolated transceivers, not just receivers, as most remote stations need to send information back to the control center. Fig. 6 illustrates how the H11N, in a two-wire, half-duplex, current-loop transceiver circuit, provides such an optically isolated, noiseimmune, two-way communication link. The moderate supplycurrent requirements of the H11N, combined with its wide supply-voltage tolerance and high-current output capability, allow the output to be biased from the loop current. These features eliminate the need for either a separate isolated supply at the isolated terminal or for a third bias-supply wire in the date link. The receiver H11N1 input IRED is biased from the transmitter output through a 5-mA current source that maintains -4V across itself. This voltage guarantees the transmitter H11N1 adequate supply voltage and stabilizes the receiver input current over a wide variety of line conditions. It also permits "party-line" operation of two isolated transceivers per loop. Link speed is limited by the H11N transmitter bypass capacitor, which raises the longer propagation delay time (tpl) from 150 ns to about 600 ns. For long-line applications, this is not a severe limitation, as

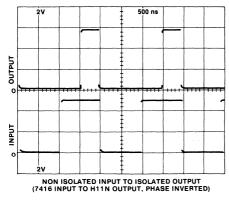
the transmission-line properties also limit data rate.

#### **MOSFET Drivers**

Another example of circuits noted for common-mode noise problems are power-MOSFET drivers, especially in series strings and the half-bridge configuration. The half-bridge, also known as the totem pole, is used to produce an ac output from a dc input and is commonly found in motor-speed-control and switching-power-supply applications.

The basic half-bridge circuit is illustrated in Fig. 7. Power MOSFETs are preferred in this circuit type because of their fast and efficient switching, and their ruggedness and ease of control. A major issue in the operation of the power-MOSFET half-bridge is the gate drive of the top device. The source (i.e., reference terminal) on this top device is attached to the drain of the lower device, and will rise and fall at the same rate as the load voltage. The power MOSFET has the capability of switching 500V in less than 50 ns (i.e., 10,000  $V/\mu s$ ), and therefore puts stress on the common-mode capability of the device that carries control information from ground to the top of the MOSFET. In most circuit applications, the MOSFET drive circuit and parasitic wiring impedences do not allow switching over full voltage ratings under a couple of hundred nanoseconds, although this is still in the 2000 to 3000 V/µs dv/dt range. Fast switching is





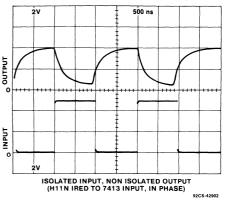


Fig. 6 - (a) Current-loop data-line isolated transceiver, (b) typical

(b)

performance waveforms for a 3450-foot, #18 pair.

16

desirable in these applications as it tends to reduce switching loss in the MOSFET, thereby increasing efficiency, lowering junction temperature, and increasing reliability under most conditions. These same considerations pertain to the series connection of power MOSFETs, Fig. 8. Such arrangements have identical schematics and differ only in the phasing of the gate signal.

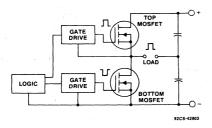


Fig. 7 - Half-bridge power-MOSFET circuit.

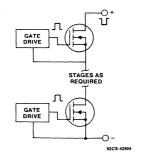


Fig. 8 - Series-connected power MOSFET.

#### **Gate-Control Circuits**

Many gate-control circuits have been proposed for the top power-MOSFET driver. These include level-shift circuits

using bipolar or MOSFET devices, transformer isolation, piezoelectric isolation, or optical isolation. None of these circuits has yet become a universal choice due to the often conflicting constraints of circuit simplicity and cost, automatic assembly compatibility, power dissipation, switching speed, duty cycle, crossover timing reliability, and commonmode noise immunity.

Although the H11N is not a panacea for noise immunity problems, it does offer excellent isolation, low power consumption, and fast, efficient switching. It also is compatible with a variety of simple circuit configurations, optimizing drive-circuit performance. In Figs. 9 and 10, each circuit uses a bootstrap "flying capacitor" to power both the gate of the MOSFET and the H11N Schmitt-trigger IC. The capacitor size is determined by the maximum conduction time of the power MOSFET. The MOS input characteristics of the Insulated Gate Transistor (IGT) allow identical circuitry to be used with the high-voltage switch.

In the Fig. 9 circuit, the capacitor, recharging, and gate bias are supplied by a simple resistor network. This network also regulates the H11N and gate-bias voltage. The disadvantage of this configuration is that both duty cycle and MOSFET turn-on times are limited by RC time constants. The use of simple signal transistors to amplify charging currents (for the bootstrap capacitor and the MOSFET gate capacitance) overcomes these limitations, however, and yields a high-performance circuit. A zener limits the bias-capacitor voltage so that it does not require several RC time constants to fully charge. Both circuits are extremely noise-immune if the physical placement of the wiring minimizes the parasitic coupling of signals between the logic circuitry and the isolated gate-bias circuit.

### **Effective Solution**

Dielectric isolation is an extremely effective method of eliminating common-mode noise signals in high-speed switching circuits. Optoisolators can now offer speed and voltage compatibility with both logic and power circuitry and can provide high common-mode transient immunity. The high-performance H11N Schmitt-trigger-output optoisolator combines these characteristics with modest power consumption at a reasonable cost, making it a very flexible solution to noise problems common to all logic and power-control systems.

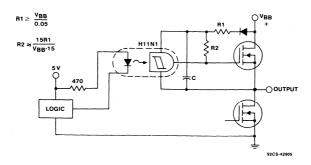


Fig. 9 - Simple, isolated, power-MOSFET driver.

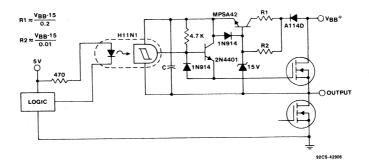


Fig. 10 - High-performance, isolated, power-MOSFET driver.

# Common-Drain Power-MOSFET Gate-Drive Solutions Using the H11N/L Optoisolators

by W. H. Sahm

#### Introduction

Power-MOSFET devices in the half-bridge configuration, Fig. 1, are becoming popular for both switching-power-supplies and PWM (pulse-width-modulated) motor controls. These circuits include a common-drain stage on which the gate and source-terminal potentials, i.e., the control-terminal potentials, rise and fall hundreds of volts in tens of nanoseconds. The magnitude and rate of change of this common-mode voltage places severe constraints on the gate-drive circuitry and represents a challenge to the circuit designer.

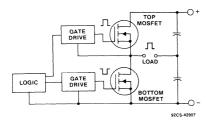


Fig. 1 - Half-bridge power-MOSFET circuit.

This Note investigates several methods of gate control for these common-drain MOSFET devices. These methods include bootstrap techniques with level shifting accomplished through the use of transistors, optoisolators, and high-voltage ICs. The conclusions are applicable to the power MOSFET, the MOS-IGT, and hybrid MOS-bipolar power switches.

### **General Considerations**

Fast-switching efficient power MOSFETs are widely used for PWM power-control applications. The common-drainconnected n-channel power MOSFET is often utilized in switching-power-supplies, motor and solenoid control, and in series-connected high-voltage switches. Although it would appear advantageous to utilize common-source p-channel devices in these sockets to simplify gate-drive circuitry, the penalty caused by the use of p-channel devices is too severe in all but the lower-circuit lower-voltage application areas. This situation will remain until III-V enhancementmode devices become widely available at low cost (if they ever prove viable), because silicon p-channel devices will always require much more silicon area to provide the same ratings. This large die area imposes an economic penalty in device cost, a performance penalty in the increased capacitance associated with the larger die area, and the complete lack of device availability in the higher current and/or voltage ratings. These facts assure a long life for the common-drain power-MOSFET configuration. Note also that a good MOSFET gate-drive design could allow replacement of a preamp bipolar with a MOSFET in the drive of a bipolar common-collector high-power output, which could amost eliminate the need for a floating current source.

The complexity of driving the gate of this common-drain power MOSFET derives from two fundamental facts: the lack of a fixed reference point for the gate signal and the need for a gate voltage with a value higher than the positive supply rail being controlled. Although these factors are also present in bipolar-transistor common-collector stages, the fast switching and the magnitude of the gate signal in power-MOS devices places more stringent requirements on the circuit design. To minimize power dissipation in the conducting state, the gate-source voltage should be greater than 10V but less than 20V, assuring minimum on-state resistance without danger of damage to the fragile gate oxide. To minimize power dissipation during switching, the gate voltage should have fast rise and fall times when driving the highly capacitive gate. Although this explanation is simple and elementary, it is not trivial when examined from a practical viewpoint. Mass-produced circuits are constrained to be very compatible with automated assembly, to be very consistent in performance over the tolerance limits of the standard components used, to perform reliably in an application for long time periods and, if failure occurs, to fail in a manner that will not create a safety hazard.

This combination of performance, manufacturability, reliability, and safety impact the design of the gate-drive circuit, which must meet cost and design-schedule goals. The performance issues that will determine the gate-drive circuit configuration include adequate speed and drive capability, total system-power dissipation, and common-mode transient immunity. The manufacturability issues include standard components, tolerance sensitivity, automatic assembly, size, adaptability, cost, and quantity used. Reliability and safety are impacted by power dissipation, parts count, isolation, noise-transient overvoltage susceptability, ease and speed of shutdown, fault-sensing compatibility, and failure consequences. Although this is not an all-inclusive list, it serves as a starting point to evaluate a gate-drive configuration for a common-drain power MOS.

The simplest gate-drive circuits directly transfer energy to the gate from the control-circuitry low-voltage supply at logic ground. Although photovoltaic and piezoelectric elements are sometimes used, they provide too little output current to be compatible with fast charging and discharging of the MOSFET gate capacitance. Pulse transformers can supply large currents, although they can be difficult to obtain with risetime capability compatible with the power MOSFET. Other possible difficulties with pulse transformers include input-to-output capacitance, automatic-insertion compatibility, and the feedback of signals from the power stages to the control circuitry. Specialty transformers can be designed to overcome these disadvantages, although economic viability may suffer. Dielectric isolation in these energy-transfer devices eliminates the possibility of highvoltage power being present on the low-voltage control circuits in a fault condition.

The most common gate-drive circuits utilize a source of stored energy referenced to the source of the commondrain stage. Although this source can be a floating power

supply powered through a transformer, or piezoelectric or photovoltaic element, it will usually be a capacitor that is charged directly from either the low-voltage control supply (flying capacitor) or the positive power rail (bootstrap) during periods when the common-drain stage is blocking. The bootstrap circuit capacitor may be recharged during long conduction periods of the common-drain MOSFET by using load current. Channel resistance is momentarily allowed to rise until drain-source voltage reaches the approximately 15V required to recharge. To provide this recharge or "refresh" of a flying-capacitor circuit, the common-drain stage must fully turn off and block full supply voltage. The charge on this capacitor is a supply for the gate of the common-drain power MOSFET and its control circuitry. The control circuitry can be as simple as a resistor and high-voltage level-shift transistor, but usually consists of several devices to provide gain, fast switching, noise suppression, voltage stability, and other desired functions. Simple optoisolators are often used to provide the controlsignal path from the low-voltage circuitry, although speed can be marginal in many cases. Until recently the more complex optoisolators would provide speed, but were limited in common-mode rejection and in voltage capability. The high-voltage integrated circuit (HVIC) has also become available recently, providing both the level shift of the control signal and the signal processing for the commondrain MOSFET gate drive. It also can be designed to provide over-current protection, automatic refresh, and coordination of conduction times of the common-drain and commonsource stages. Devices available to date can operate up to 500V and above 20 kHz. These HVICs are normally designed as application-specific devices for specific system applications.

### **Optoisolator Characteristics**

Recently, high-speed optoisolators, with excellent commonmode rejection and wide supply-voltage compatibility, have become available. The simplest and least costly of these devices are six-pin dual-in-line plastic-packaged infrared diode-input Schmitt-trigger-output configurations. Two basic derivations are commonly available, one being optimized for fast switching and one for low power consumption. These derivations are convenient for the power-MOSFET-circuit designer, as a basic "universal" circuit can be designed, and only the optoisolator changed for a choice of either longer duty cycles (>10 ms) at moderate speeds ( $\leq$ 200 kHz @ 150 ns t<sub>r</sub>, t<sub>r</sub>), or a shorter duty cycle operating to more than 2 MHz with 15-ns transitions. Duty cycles are limited by the Schmitt-trigger power-supply current draining the source capacitor and can be increased with larger storage capacitance, but at the cost of increased refresh time or more complex refresh circuitry. DC operation requires a refresh scheme or a small power supply, as mentioned above. Overall, these optoisolators appear to offer great advantages in driving common-drain power MOSFETs and similar devices, such as IGT, MOS-gated thyristor, etc.

#### **Test Circuit**

To check the apparent advantages of the optoisolator approach, a circuit was built that employed the H11L (slow) and H11N (fast) optoisolated Schmitt triggers. A plug-in prototype board was used to construct the circuit of Fig. 2. The circuit makes use of an IRF630 power-MOSFET switch and replaces the lower FET with a 45-ohm power-resistor source load. A  $1-\mu F$ aluminum electrolytic capacitor was used as the bootstrap supply, with a variable dc power source for VBB. The VBB supply was kept below 75V to keep the circuit within the IRF630 ratings during the turn-off spike. No heatsinks or special wiring precautions were used. Although only the H11N1 is actually specified for common-mode rejection at 2000 V/µs minimum, the lower-cost H11L1 uses similar shielding in the IC chip, and identical packaging. These similar features of the H11L1 and N1 lead to the expectation of a similar ability to function under high dy/dt.

Tests of the circuit confirmed the expected performance for both optoisolators in the circuit. The H11L was driven from 5V pulses with a 2K resistor, and drives the IRF630 at about 300 kHz with a 12% duty cycle. Turn-on and turn-off times of the IRF630 were about 60 ns, which yielded more than 2000-V/ $\mu$ s dv/dt during the 175V turn-off spike. These waveforms are illustrated in Fig. 3. The H11N1 was then substituted for the H11L, and the value of the infrared diodelimiting resistor was reduced to 680 ohms. Operation at 1 MHz was confirmed. Higher-frequency operation was obtainable through heatsinking of the IRF630 and the use of a higher-rated load resistor. The waveform presented in Fig. 4 illustrates this operation, and about the same dv/dt as the H11L provided.

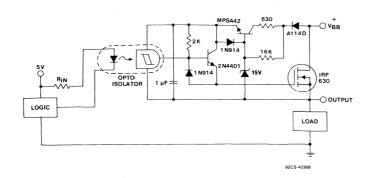
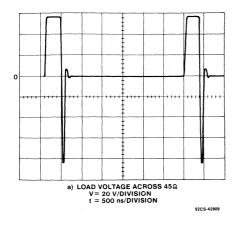
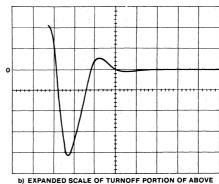


Fig. 2 - Optically isolated power-MOSFET-driver test circuit.





b) EXPANDED SCALE OF TURNOFF PORTION OF ABOVE WAVEFORM
V= 20 V/DIVISION
t = 50 ns/DIVISION
92CS-42910

92CS-42911

92CS-42910

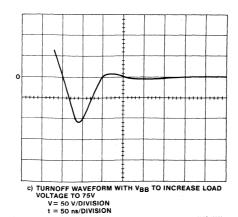


Fig. 3 - Waveforms taken with an H11L in the test circuit.

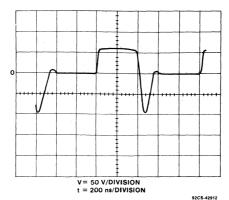
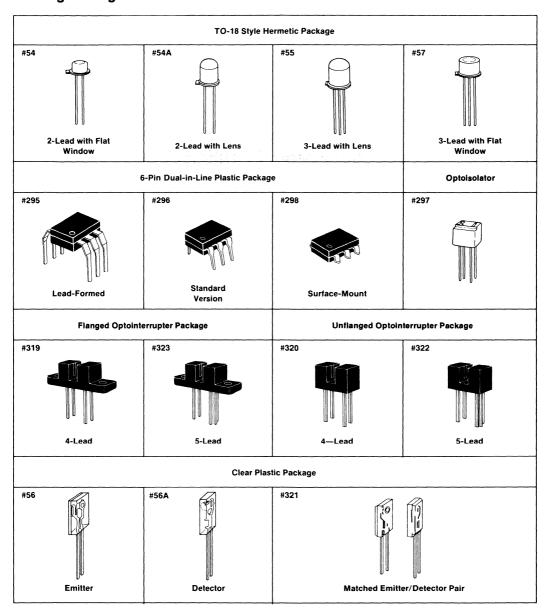


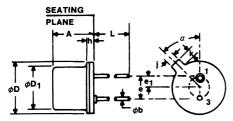
Fig. 4 - Waveforms taken with an H11N in the test circuit.

Dimensional	Outlines	4	11	4

### **Package Designations**



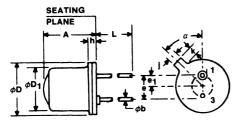
Package Designation #54 TO-18 Style Hermetic Package 2-Lead with Flat Window



### NOTES:

- 1. Measured from maximum diameter of device.
- Leads having max. diameter .021" (.533mm) measured in gaging plane .054" + .001" - .000 (137 + 025 - 000mm) below the reference plane of the device shall be within .007" (.778mm) their true position relative to a maximum width tab.
- 3. From centerline tab.

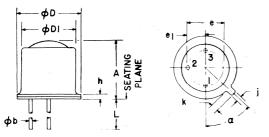
### Package Designation #54A TO-18 Style Hermetic Package 2-Lead with Lens



### NOTES:

- 1. Measured from maximum diameter of device.
- Leads having max. diameter .021" (.533mm) measured in gaging plane .054" + .001" .000 (137 + 025 000mm) below the reference plane of the device shall be within .007" (.778mm) their true position relative to a maximum width
- 3. From centerline tab.

### Package Designation #55 TO-18 Style Hermetic Package 3-Lead with Lens



#### NOTES

- 1. Measured from maximum diameter of device.
- 2. Leads having max. diameter .021" (.533mm) measured in gaging plane .054" + .001" .000 (137 + .025 000mm) below the reference plane of the device shall be within .007"

0744001	INCHES		MILLIN	IETERS	NOTES
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α		.155	_	3.93	
φЬ	.016	.021	.407	.533	
$\phi$ D	.209	.230	5.31	5.84	
$\phi D_1$	.180	.188	4.57	4.77	
e	.100 NOM.		2.54 NOM.		2
e <sub>1</sub>	.050	.050 NOM.		NOM.	2
h	_	.030	_	1.76	
j	.031	.044	.79	1.11	
k	.036	.046	.92	1.16	-1
L	1.00	-	25.4	_	
α	45°		45°		3

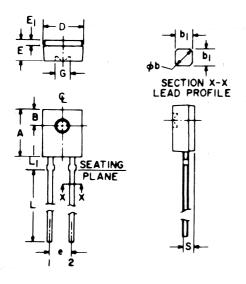
	INCHES		MILLIN	METERS	NOTES
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	_	.255	_	6.47	
φb	.016	.021	.407	.533	
φD	.209	.230	5.31	5.84	
$\phi D_1$	.180	.188	4.57	4.77	
e	.100	.100 NOM.		2.54 NOM.	
e <sub>1</sub>	.050	.050 NOM.		NOM.	2
h	_	.030		.76	
j	.031	.044	.79	1.11	1
k	.036	.046	.92	1.16	1 1
L	1.00	-	25.4	-	
α	4	5°	4	5°	3

					T
SYMBOL	INCHES		MILLIM	NOTES	
31111001	MIN.	MAX.	MIN.	MAX.	1.0120
Α	.225	.255	3.71	6.47	
φb	.016	.021	.407	.533	. [
$\phi$ D	.209	.230	5.31	5.84	
$\phi D_1$	.178	.195	4.52	4.96	
е	.100 l	NOM.	2.54	NOM.	2
e,	.050 NOM.		1.27	NOM.	2
h		.030		.76	
j	.036	.046	.92	1.16	
k	.028	.048	.71	1.22	1
L	.500		12.7	_	
α	45°	45°	45°	45°	3

(.778mm) their true position relative to a maximum width tab.

3. From centerline tab.

Package Designation #56 Clear Plastic Package Emitter

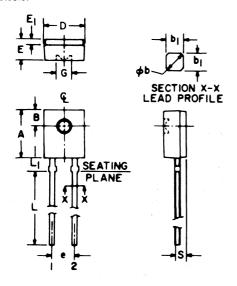


SYMBOL	INCHES		MILLIN	IETERS	
STWIBOL	MIN.	MAX.	MIN.	MAX.	NOTES
A	.220	.228	5.59	5.80	
В	.070	NOM.	1.78	NOM.	2
φb	.024	.030	.60	.75	1
b,	.020	NOM.	.51	NOM.	1
D	.175	.185	4.45	4.70	
E	.095	.105	2.41	2.67	
E,	.023	.027	.58	.69	
e	.095	.105	2.41	2.67	3
G	.078	NOM.	1.98	NOM.	
L	.500	_	12.7	_	
L <sub>1</sub>	.055	.065	1.40	1.65	
S	.033	.037	.83	.94	3

### NOTES:

- Two leads. Lead cross section dimensions uncontrolled within 1.27mm (.050") of seating plane.
- 2. Centerline of active element located within .25mm (.010") of true position.
- 3. As measured at the seating plane.
- 4. Inch dimensions derived from millimeters.

### Package Designation #56A Clear Plastic Package Detector

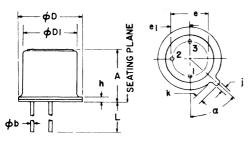


SYMBOL	INC	HES	MILLIN		
STMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
A	.220	.228	5.59	5.80	
В	.070	NOM.	1.78	NOM.	2
φb	.024	.030	.60	.75	1
b <sub>1</sub>	.020	NOM.	.51	NOM.	1
D	.175	.185	4.45	4.70	
E	.095	.105	2.41	2.67	
E,	.023	.027	.58	.69	15.75
e	.095	.105	2.41	2.67	3
G	.078	NOM.	1.98	NOM.	İ
L	.500	_	12.7		
L,	.055	.065	1.40	1.65	1
s	.033	.037	.83	.94	3

#### NOTES:

- Two leads. Lead cross section dimensions uncontrolled within 1.27mm (.050") of seating plane.
- Centerline of active element located within .25mm (.010") of true position.
- 3. As measured at the seating plane.
- 4. Inch dimensions derived from millimeters.

Package Designation #57 TO-18 Style Hermetic Package 3-Lead with Flat Window

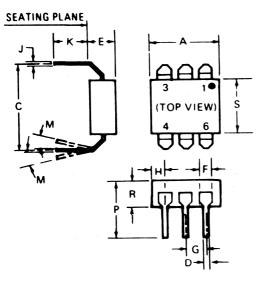


### NOTES:

- 1. Measured from maximum diameter of device.
- Leads having max. diameter .021" (.533mm) measured in gaging plane .054" + .001" - .000 (137 + .025 - 000mm) below the reference plane of the device shall be within .007" (.778mm) their true position relative to a maximum width tab.
- 3. From centerline tab.

SYMBOL	INCHES		MILLIN	MILLIMETERS		
	MIN.	MAX.	MIN.	MAX.	NOTES	
A	_	.210	_	5.34	1	
φb	.016	.021	.406	.534		
$\phi$ D	.209	.230	5.30	5.85		
$\phi D_1$	.178	.195	4.52	4.96		
e	.100 NOM.		2.54	NOM.	2	
e,	.050 NOM.		1.27	NOM.	2	
h	_	.030	-	.76		
j	.036	.046	.91	1.17		
k	.028	.048	.71	1.22	1	
L	.500	_	12.7	_		
α	45°	45°	45°	45°	3	

Package Designation #295 6-Pin Dual-in-Line Plastic Package Lead-Formed

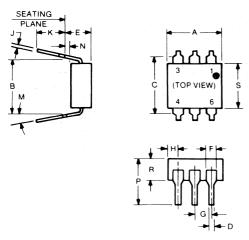


SYMBOL	INCHES		MILLIN	METERS	
SIMBUL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	.330	.350	8.38	8.89	
С	.400	REF.	10.16	ŖEF.	
D	.016	.020	.406	.508	
E		.170	_	4.32	
F	.040	.070	1.01	1.78	
G	.090	.110	2.28	2.80	
н	_	.085		2.16	1
J	.008	.012	.203	.305	
к	.100	-	2.54	_	
м	_	10°	_	10°	
Р	.244 REF.		6.20 F	REF.	
R	.115	.135	2.92	3.43	
s	.240	.270	6.10	6.86	

### NOTES:

1. Dimension applies four places.

Package Designation #296 6-Pin Dual-in-Line Plastic Package Standard Version

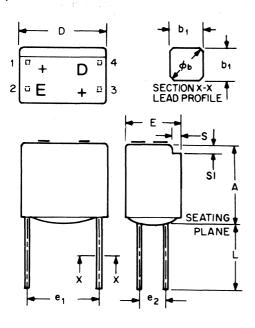


SYMBOL	IN	CHES	MILLIM	ETERS	NOTES
SIMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	0.330	0.350	8.38	8.89	1
В	0.3	00 REF.	7.620	REF.	1
С		0.340	_	8.64	2
D	0.016	0.020	0.406	0.508	
E	_	0.200	_	5.08	3
F	0.040	0.070	1.01	1.78	
G	0.090	0.110	2.28	2.80	1
н	_	0.085	-	2.16	4
J	0.008	0.012	0.203	0.305	
K	0.100		2.54	_	
M	_	15°	_	15°	1
N.	0.015	_	0.381	-	
P	_	0.375	_	9.53	
R	0.115	0.135	2.92	3.43	
S	0.240	0.270	6.10	6.86	

### NOTES:

- 1. Installed position lead centers.
- 2. Overall installed dimension.
- 3. These measurements are made from the seating plane.
- 4. Four places.

### Package Designation #297 Optoisolator

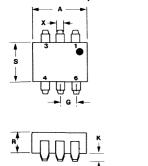


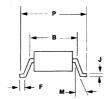
SYMBOL	INCHES		MILLIMETERS		
STMBUL	MIN.	MAX.	MIN.	MAX.	NOTES
A	_	.350		8.89	
φb	.024	.030	.600	.750	1
b <sub>1</sub>	.020 1	NOM.	.50 N	IOM.	1
D		.375		9.52	
<b>e</b> 1	.285	.315	7.24	8.00	1
<b>e</b> <sub>2</sub>	.090	.110	2.29	2.79	
E	_	.250		6.35	1
L	.300	-	7.62	_	1
R	.050 NOM.		1.27 (	NOM.	
S	.020	.030	.50	.76	ļ.
S <sub>1</sub>	.020	.030	.50	.76	

### NOTES:

1. Four leads. Lead dimensions controlled between .050" (1.27mm) from the seating plane and the end of the leads.

Package Designation #298 6-Pin Dual-in-Line Plastic Package Surface-Mount Optoisolator





SMB (Standard) Surface-Mount Package

SYMBOL	INCHES		MILLIM	MILLIMETERS	
	MIN.	MAX.	MIN.	MAX.	NOTES
Α	0.330	0.350	8.38	8.89	
В	0.33	OREF.	8.380	REF.	
F	0.020	0.040	0.508	1.02	2
G	0.090	0.110	2.28	2.80	
J*	0.008	0.022	0.203	0.559	
K	0.0040	0.0098	0.102	0.249	
M		15°	_	15°	
P	0.375	0.395	9.53	10.03	
R	0.115	0.135	2.92	3.43	
s	0.240	0.270	6.10	6.86	
X*	0.015	0.030	0.381	0.762	
Coplan-					
arity	0	0.002	0	0.051	.1 .

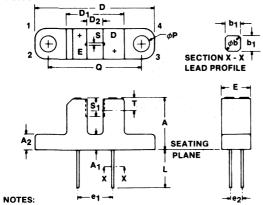
NOTES:

92CS-42862

 Coplanarity is the distance from a plane, defined by the end of the three longest legs to the end of the shortest leg.

\*Solder dip.

Package Designation #319
Flanged Optointerrupter Package
4 Lead



1. Inch dimensions are derived from millimeters.

2. Four leads. Lead cross section is controlled between 1.27mm (.050") from seating plane and the end of the leads.

Surface-mount packaging for the entire 6-pin DIP opto-isolator line!

Add the "SMA" or "SMB" suffix to any 6-pin optoisolator part number when ordering.

SMA (Low-Profile) Surface-Mount Package

SYMBOL	INCHES		MILLIM	MILLIMETERS	
	MIN.	MAX.	MIN.	MAX.	NOTES
Α	0.330	0.350	8.38	8.89	1
В	0.33	O REF.	8.380	REF.	
F	0.020	0.040	0.508	1.02	
G	0.090	0.110	2.28	2.80	
J*	0.008	0.022	0.203	0.559	Ì
K	0.0005	0.0040	0.013	0.102	
м	_	15°	_	15°	
P	0.373	0.393	9.47	9.98	
R	0.115	0.135	2.92	3.43	
s	0.240	0.270	6.10	6.86	1
X*	0.030	0.050	0.762	1.27	1
Coplan-					1
arity	0	0.002	0	0.051	1

NOTES:

92CS-42861

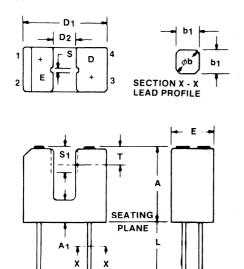
 Coplanarity is the distance from a plane, defined by the end of the three longest legs to the end of the shortest leg.

\*Solder dip.

0744001	INC	HES	MILLIN		
SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	.422	.433	10.7	11.0	
<b>A</b> 1	.119	.125	3.0	3.2	
A <sub>2</sub>	.119	.125	3.0	3.2	
φb	.024	.030	.600	.750	2
b <sub>1</sub>	.020	NOM.	.50 1	NOM.	2
D	.957	.972	24.3	24.7	
D,	.457	.472	11.0	12.0	-
D <sub>2</sub>	.119	.129	3.0	3.3	
e <sub>1</sub>	.272	.295	6.9	7.5	
e <sub>2</sub>	.091	.110	2.3	2.8	
E	.243	.249	.615	6.35	
L	.315	_	6.00	_	
φP	.126	.133	3.2	3.4	
Q	.745	.755	18.9	19.2	
s	.034	.039	.85	1.0	
S <sub>1</sub>	.136	.147	3.45	3.75	
Т	.103	NOM.	2.6 !	NOM.	3

3. The sensing area is defined by the "S" dimension and by dimension "T"  $\pm$  0.75mm ( $\pm.030$  inch).

Package Designation #320
Unflanged OptoInterrupter Package
4 Lead

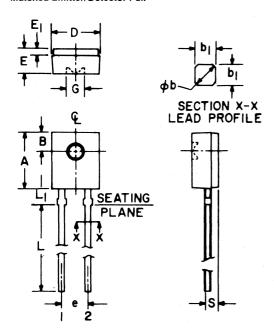


SYMBOL	INC	HES	MILLIN	NOTES	
STWIDUL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	.422	.433	10.7	11.0	
Α,	.119	.125	3.0	3.2	
φb	.024	.030	.600	.750	2
<b>b</b> 1	.020	.020 NOM50 NOM.		2	
D <sub>1</sub>	.457	.472	11.6	12.0	
D <sub>2</sub>	.119	.129	3.0	3.3	
e1	.272	.295	6.9	7.5	
<b>e</b> <sub>2</sub>	.091	.110	2.3	2.8	
E	.243	.249	6.15	6.35	
L	.315	_	8.00	-	
S	.034	.039	.85	1.0	
S <sub>1</sub>	.136	.147	3.45	3.75	1
т	.103	NOM.	2.6 1	NOM.	3

### NOTES:

- 1. Inch dimensions are derived from millimeters.
- Four leads. Lead cross section is controlled between 1.27mm (.050") from seating plane and the end of the leads.
- 3. The sensing area is defined by the "S" dimension and by dimension "T"  $\pm$  0.75mm ( $\pm$ .030 inch).

Package Designation #321
Clear Plastic Package
Matched Emitter/Detector Pair



SYMBOL	INC	HES	MILLIN	MILLIMETERS	
SIMBUL	MIN.	MAX.	MIN.	MAX.	NOTES
A	.220	.228	5.59	5.80	
В	.070	NOM.	1.78	NOM.	2
φb	.024	.030	.60	.75	1
b,	.020 NOM.		.51 NOM.		1
D	.175	.185	4.45	4.70	1
E	.095	.105	2.41	2.67	
E1	.023	.027	.58	.69	
e	.095	.105	2.41	2.67	3
G	.078 1	NOM.	1.98 NOM.		
L	.500	_	12.7	_	1
L,	.055	.065	1.40	1.65	
s	.033	.037	.83	.94	3

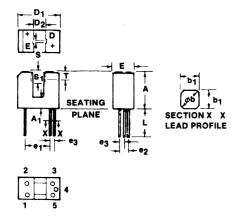
### NOTES:

- Two leads. Lead cross section dimensions uncontrolled within 1.27mm (.050") of seating plane.
- 2. Centerline of active element located within .25mm (.010") of true position.
- 3. As measured at the seating plane.
- 4. Inch dimensions derived from millimeters.

MILLIMETERS

### **Dimensional Outlines**

### Package Designation #322 Unflanged Optointerrupter Package 5 Lead



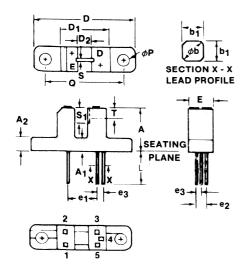
NO	ΓES

- 1. Inch dimensions are derived from millimeters.
- Five leads. Lead cross section is controlled between 1.27mm (.050") from seating plane and the end of the leads.
- 3. The sensing area is defined by the "S" dimension and by dimension "T"  $\pm$ 0.75mm ( $\pm$  .030 inch).

SYMBOL	MIN.	MAX.	MIN.	MAX.	NOTES
Α	.422	.433	10.7	11.0	
Αı	.119	.125	3.0	3.2	
φb	.024	.030	.600	.750	2
b <sub>1</sub>	.020 1	NOM.	.50	NOM.	2
D,	.457	.472	11.6	12.0	
$\mathbf{D}_2$	.119	_	3.0	_	
e <sub>1</sub>	.272	.295	6.9	7.5	
<b>e</b> <sub>2</sub>	.091	.110	2.3	2.8	
<b>e</b> <sub>3</sub>	.045	.055	1.14	1.4	
E	.243	.249	6.15	6.35	
L	.315	_	8.00	_	
s	.034	.039	.85	1.0	
S <sub>1</sub>	.155 N	OM.	3.94 N	OM.	
т	.103 NOM.		2.6 N	OM.	3

INCHES

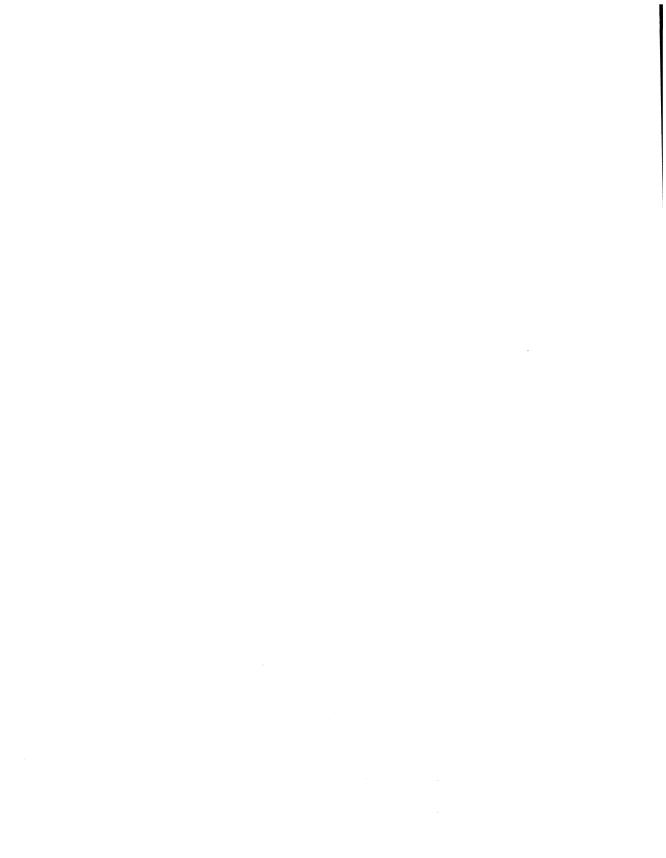
## Package Designation #323 Flanged Optointerrupter Package 5 Lead



SYMBOL	INC	HES	MILLIN	METERS	1
STMBUL	MIN.	MAX.	MIN.	MAX.	NOTES
A	.422	.433	10.7	11.0	
Α,	.119	.125	3.0	3.2	
A <sub>2</sub>	.119	.125	3.0	3.2	
φb	.024	.030	.600	.750	2
b <sub>1</sub>	.020 1	NOM.	.50 1	ŅОМ.	2
D	.957	.972	24.3	24.7	
D <sub>1</sub>	.457	.472	11.6	12.0	
D <sub>2</sub>	.119	_	3.0	-	
e <sub>1</sub>	.272	.295	6.9	7.5	
<b>e</b> <sub>2</sub>	.091	.110	2.3	2.8	
<b>e</b> <sub>3</sub>	.045	.055	1.14	1.40	
E	.243	.249	6.15	6.35	
L	.315	_	8.00	_	
φp	.126	.133	3.2	3.4	
Q	.745	.755	18.9	19.2	
S	.034	.039	.85	1.0	
S <sub>1</sub>	.155 1	NOM.	3.94	NOM.	
Т	.103 1	NOM.	2.6 N	IOM.	3

### NOTES

- 1. Inch dimensions are derived from millimeters.
- 2. Five leads. Lead cross section is controlled between 1.27mm (.050") from seating plane and the end of the leads.
- 3. The sensing area is defined by the "S" dimension and by dimension "T"  $\pm 0.75 mm$  ( $\pm$  .030 inch).



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